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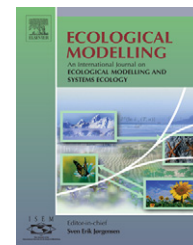


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The solar transformity of petroleum fuels

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ABSTRACT

Petroleum fuels are the primary energy basis for transportation and industry. They are almost always an important input to the economic and social activities of humanity. Emergy analyses require accurate estimates with specified uncertainty for the transformities of major energy and material inputs to economic and environmental systems. In this study, the oil refining processes in Italy and the United States were examined to estimate the transformity and specific emergy of petroleum derivatives. Based on our assumptions that petroleum derivatives are splits of a complex hydrocarbon mixture and that the emergy is split based on the fraction of energy in a product, we estimated that the transformity of petroleum derivatives is $65,826 \text{ sej/J} \pm 1.4\%$ relative to the $9.26\text{E}+24 \text{ sej/year}$ planetary baseline. Estimates of the specific emergies of the various liquid fuels from Italian and U.S. refineries are within 2% of one another and the relationship of particular values varies with the refinery design. Our average transformity is only 1.7% larger than the current estimate for petroleum fuels determined by back calculation, confirming the accuracy of this transformity in existing emergy analyses. The model uncertainty between using energy or mass to determine how emergy is split was less than 2% in the estimate of both the transformity and specific emergy of liquid fuels, but larger for solid and gaseous products. This study is a contribution to strengthen the emergy methodology, providing data that can be useful in the analysis of many human activities.

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1. Introduction

Solar Emergy (from now on simply emergy) is a concept developed by H.T. Odum in the early 1980s to account for the basic energy requirements in obtaining a product. It has been defined as “the available solar energy used up directly and indirectly to make a service or product” (Odum, 1996). The reason why the energy has to be of one particular type (solar) is the totally different ability in performing actual physical work from a joule of different types of energy. Solar energy is then the fundamental unit since it is the basis of all other types of emergy in the biosphere.

Emergy expresses all the energy in space and time going into a product. This quantity and the “intensive” quantity, transformity (defined as the solar energy required, in direct and indirect ways, to obtain a joule of product) are the basis of emergy evaluation. Transformity reflects the pathway of energy transformations in the universe, designing an energy hierarchy. Transformities indicate position of each form of energy of the universe in this universal energy hierarchy (Brown et al., 2004).

Since the definitions of emergy and transformity are based more on a logic of “memorization”, than of conservation, an algebra of emergy has been introduced. In particular the

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difference between the categories of splits and co-products (or by-products) can be expressed as (Brown and Herendeen, 1997):

- By-products from a process have the total emergy assigned to each pathway;
- When a pathway splits, the emergy is assigned to each 'leg' of the split based on its percentage of the total energy flow on the pathway.

Determining the emergy contributed by petroleum fuels is an important factor in almost every emergy evaluation that considers human-dominated systems. The direct use of petroleum fuels may be of variable magnitude, depending on the type of system examined, but its indirect uses support almost every aspect of our industrial-based civilization. In 1995, the use of fossil fuels and minerals accounted for about 2/3 of the emergy basis for the earth (Brown and Ulgiati, 1999). However, in an emergy evaluation of the State of West Virginia Campbell et al. (2005) showed that the petroleum used directly represents 5.3% of the total emergy used and 7.3% of the imported emergy. In agricultural production systems petroleum fuel is an important direct input, accounting for between 10% and 19% of direct emergy inputs for wine (Pizzigallo et al., 2008), 6.7% for grain corn, 7.5% for milk, and 15.6% for green beans (Brandt-Williams, 2002). Petroleum can be especially important in industrial systems where fuel accounted for 71% of the emergy required for the production of caustic soda, 48% for diatomite, and 26% for 20% sulphuric acid (Odum et al., 2000). In general, emergy evaluations are sensitive to the quantities and transformities of fuels used to support systems and carry out processes, e.g., fuel type is a fundamental variable in the calculation of the transformity of electricity (Odum, 1996; Brown and Ulgiati, 2002). For this reason, it is important that these values be calculated as precisely as possible.

The transformity of oil was originally derived starting from an average value for the transformity of electricity determined to be $1.73\text{E}+5$ sej/J (Odum, 1996).¹ From this number an approximate transformity was derived for coal of $4.3\text{E}+4$ sej/J assuming 4 coal J/J electric power. An additional transformity for coal was determined by analyzing its geological process of formation and found to be $3.4\text{E}+4$ sej/J resulting in an average estimate of $3.9\text{E}+4$ sej/J for coal. Rounding this average number to 40,000 sej/J and multiplying by 1.65 J coal/J motor fuel (Slessler, 1978) gives an estimate of 66,000 sej/J for fuels derived from oil (Odum, 1996). Cook (1976) found that 19% of crude oil was used in transport and refining giving a ratio of 1.23 between crude oil and refined products. Odum (1996) estimated the transformity of crude oil to be 54,000 sej/J based on this ratio. Recently, Bastianoni et al. (2005) derived the values of the transformities and emergies per mass of oil and natural gas directly (see Table 1) through an analysis of their geological production process, confirming the results of the

earlier work by Odum using an independent approach. Now that these values have been verified by several methods, it is fundamental for further development of accurate emergy evaluations, to establish the transformities and emergies per mass of the various fuels derived from oil, through a direct analysis of the refining process.

1.1. Split or co-product?

The main factor that influences the value of the transformities of oil-based fuels is the choice between making the various petroleum derivatives splits or co-products in an evaluation of the production process. Emergy is a concept based on the 2nd law of thermodynamics and thus it follows the history of available energy (exergy) use required to create a product or service. In such an accounting, splits and co-products are handled differently, where the sum of the emergy of all co-products can exceed the emergy input. This problem is dealt with by the fourth emergy algebra rule, that states that "Emergy cannot be counted twice within a system: . . . by-products, when reunited, cannot be added to equal a sum greater than the source emergy from which they were derived" (Brown and Herendeen, 1997).

Being based on "memorization", rather than on conservation logic, emergy evaluation emphasizes knowing the difference between a split and a co-product. In particular, co-products are "product items showing different physico-chemical characteristics, but which can only be produced jointly" (Sciubba and Ulgiati, 2005). Splits instead are "originating flows showing the same physico-chemical characteristics" (Sciubba and Ulgiati, 2005).

Petroleum is a complex mixture of hydrocarbons, which is separated into many products in the refining process. There are several problems that can arise in accounting for the emergy delivered by inputs of this type, especially when two or more of them are used in the same production process. If we consider all the oil-derived fuels as a split, in the case of a system supported by several fuels, we can simply add all the emergies of the fuels (since under this assumption they can be considered of independent origin) to obtain the emergy input to the production process. Alternatively, if we consider them as co-products, then only the product with the highest contribution of emergy should be used to determine the emergy input to a fuel-using process. We also considered the hypothesis that petroleum fuels are in a "grey-zone" between a split and a co-product. In this case the best way to estimate the transformities of oil derivatives would be from production processes that have been adjusted for the maximum yield of a particular derivative. In this approach, a problem arises in determining how to sum the emergy contributions to determine the total emergy required by a fuel-using process when more than one fuel from the same source is used: all the contributions should be added and then the "intersection" of the emergies (i.e. the part of the emergy that is in common between one fuel and another) should be subtracted. This calculation could be quite difficult to handle. This paper aims to clarify the production of petroleum derivatives in the refining process and to produce reliable transformities and specific emergies (emergy per unit mass) of the various fuels to be used in other emergy evaluations.

¹ The numbers given in this paragraph are referenced to the $9.44\text{E}+24$ sej/year baseline (Odum, 1996). To convert them to the $9.26\text{E}+24$ sej/year baseline (Campbell, 2000) used in this paper multiply by 0.9809332.

Table 1 – Comparison between the newly calculated transformities (in sej/J) of oil and methane as in Bastianoni et al. (2005) and the previous ones estimated in Odum (1996).

Data in sej/J	Transformity (Bastianoni et al., 2005)	Previous transformity (Odum, 1996) ^a	Average transformity (used in this paper)
Methane	4.00E+4	4.71E+4	4.35E+4
Oil	5.54E+4	5.30E+4	5.42E+4

New transformities and the previous ones are relative to the $9.26\text{E}+24$ sej/year baseline (Campbell, 2000).

^a The range of estimates for the transformity of natural gas was extrapolated from Odum (1996) based on the assumption that gas is 20% more efficient than coal in boilers (Cook, 1976), and two determinations of the transformity of coal (Odum, 1996), one from the sedimentary cycle ($3.4\text{E}+4$ sej/J) and a second from energy quality of coal relative to electricity ($4.3\text{E}+4$ sej/J). The average transformity of coal is 3.9 sej/J coal, but Odum often rounded it to 4.0 sej/J coal. Multiplying 4.0 sej/J coal by 1.2 gives 4.8 sej/J natural gas, which is 4.71 sej/J when converted to the $9.26\text{E}+24$ sej/year baseline.

2. Materials and methods

2.1. Main characteristics of a refinery

To solve the split/co-product/grey-zone problem we decided to focus on how a refinery actually works. The results of an enquiry at the Falconara refinery in Italy can be summarized in the following points:

- Each refinery is constructed according to the characteristics of the crude oil available; this means that each plant operates within a precise range of oils and there is little flexibility in the sources that can be used.
- Each refinery is designed for a specific mix of products according to present and future market analyses. Development plans are made based on a 10–15-year forecast of the expected patterns of consumption, which means that each plant produces certain products and managers cannot change their proportions unless they invest in new components for the plant.
- Before the plant is built, almost any oil derivative could be produced from a certain quantity of crude oil with the same maximum yield (almost 100%); only the cost of obtaining that quantity of the oil derivative from crude oil would be different. Choices are made in order to maximize economic benefit considering the desired mix of products.

2.2. The Falconara plant

Data on the refining process at the Falconara refinery were obtained from the plant records and averaged for the 2001–2004 period (API, 2005). The Falconara plant receives around $3.6\text{E}+6$ t of petroleum every year and about 80% of it is transformed into liquid fuels (in particular around 46% is diesel, 18% is gasoline and the rest is composed of fuel oil and LPG), 6–7% to gases and the remainder into solids such as asphalt, bitumen, sulphur, etc. Part of the solid material is used to produce electricity that is not used in the refinery. The crude oil mainly arrives from the Middle East in various proportions of lighter and heavier crude. The transformity of crude oil used in this paper (see Table 1) is the average between the one obtained by Odum (1996) and the direct calculation performed by Bastianoni et al. (2005). The same holds for natural gas.

The plant costs to process crude oil were estimated to be 22 €/t and plant maintenance costs were 20 €/t. The lifetime of the plant was estimated to be 20 years. Methane was the only external input necessary for the refining process, and the major part of the gaseous residues were internally utilized in refining the oil; and therefore, not explicitly computed in the emergy evaluation. The only gaseous output considered in the process was LPG.

Nine different categories of oil derivatives were produced: gasoline (aviation and auto), jet fuel kerosene, other kerosene, gas/diesel oil, residual fuel oil, LPG, bitumen, refinery gas (for internal use), lubricants, and other oil products. To account for the emergy necessary for transport and all the other services needed to transfer the crude oil from the wells to the refinery, we considered the average cost for oil on the world market from 1946 to 2006 equal to \$26.16 (Williams, 2007). This value was converted into 21.8€ by means of an euro to dollar ratio of 1.2439, that was the average exchange rate in 2004 (source: Bank of Italy: <http://uif.bancaditalia.it/UICFEWebroot/index.jsp?whichArea=Cambi&lingua=en>). The cost of oil was multiplied by the emergy to money ratio that was estimated as $1.07\text{E}+12$ sej/\$ for the U.S. economy in 2000 (Campbell et al., 2005) and this ratio was also used as a proxy of the ratio for OECD countries. It is practically identical to the world average emergy to money ratio $1.08\text{E}+12$ sej/\$ (Brown and Ulgiati, 1999), when converted to the 9.26 baseline. However, the cost of equipment and maintenance for the plant was multiplied by the local emergy to money ratio of the Ancona province in 2000, where Falconara is located (calculated from data in Marchettini et al., 2007), and updated to the € value in 2004: $1.43\text{E}+12$ sej/€.

2.3. The oil refinery system in the United States of America

In addition to the study of the Falconara Refinery, we performed an analysis of the petroleum refining industry in the United States in the periods 1993–2004, focusing particularly on data from 2004 for the evaluation of the energy and material inputs to refining because data on refinery products, energy, and materials used in the refining process were available for that year from the U.S. Energy Information Administration (EIA). The structure of monetary costs was not available for the nation as a whole, but it was found for five San Francisco Bay refineries in Quinn (2001). Petroleum derivative produc-

tion at these five refineries was evaluated from 1996 to 1998 and the results were used to estimate the emergy of goods and services used for refining in the U.S. industry as a whole.

Data on the U.S. refining industry was obtained from EIA (2007) Energy Information Administration web site (http://tonto.eia.doe.gov/dnav/pet/pet.pnp_top.asp). Data on the weekly inputs in barrels from 1993 to 2004 were summed to obtain the annual utilization of crude oil and additives in the U.S. refining industry: the average annual input of crude oil was 5.35 billion barrels. The volumes of outputs were calculated from the percentage yield of products in 16 categories plus a processing gain in volume. There were 10 categories of liquids (liquefied petroleum gas – LPG – motor gasoline, aviation gasoline, kerosene–jet fuel, kerosene, distillates, residual fuel oil, naphtha chemical feedstock, other chemical feedstock and naphtha special), four solids (lubes, waxes, petroleum coke, and asphalt), one gas (still gas), plus one miscellaneous category. The small amount of miscellaneous material was assumed to be solids. The mass of output products was determined by applying an average weight per barrel to the volume data. These factors were also obtained from EIA (2005) (www.eia.doe.gov/emeu/iea/tablec1.html). The weighted average barrels per metric ton (t) was determined for all the products and applied to the crude oil and additive volume input to estimate the weight of crude oil used. In particular in the years 1993–2004 the U.S. refining industry produced 46.3% gasoline, 22.8% distillates (mainly diesel) and around 10% kerosene and jet fuels.

The inputs of energy and materials to the refining process including the feedback of refined products were given in EIA (2004) Petroleum Supply Annual 2004 Volume 1 http://www.eia.doe.gov/oil_gas/petroleum/data_publications/petroleum_supply_annual/psa_volume1/psa_volume1.html.

Also in this case, the transformity of crude oil and of natural gas are according to Table 1, while for the transformity of coal we used 39,200 sej/J (Campbell et al., 2005). The emergy of services in the crude oil extracted and transported to the U.S. was estimated from the average cost for oil on the world market from 1946 to 2006, which was used to convert the dollar value of the oil to an estimate of the emergy of human service required to extract and transport it to the refinery. The emergy of human services used in the refining process in the United States was estimated from an analysis of five refineries in the San Francisco Bay area (Quinn, 2001). The emergy of labor was estimated separately using employment data and subtracted from the total input of all goods and services to avoid double counting. This evaluation of the San Francisco Bay area refineries used data on the material inputs to production from the 2004 analysis of the entire U.S. Refining industry, which were applied to the Bay area refineries assuming that the requirement for material inputs per t of gasoline produced was the same as for the nation in 2004.

3. Results and discussion

3.1. Solution of split/co-product dilemma

Crude oil is a complex mixture of mainly hydrocarbons that comes out of the ground in many different forms. Based on the

demand for petroleum products that exists in a given region and the availability of the various kinds of crude oil (sweet, sour, light, heavy) refineries are constructed to take and refine crude oil within a certain range of properties, e.g., specific gravity, sulphur content, boiling point of the constituents, etc. From the description of the interaction of crude oil input with the refinery system given above, we have seen that the range of proportions among the possible products is in principle very wide. Only after the plant is established are the proportions of the output products constrained by the refinery characteristics. Even after the refinery is built, it can be converted to process a different kind of crude oil by refitting it, even though the cost can be high.

In the refining process petroleum derivatives behave like splits, because the input is a complex mixture of hydrocarbons and the output is a separation of this mixture into fractions of different density. In principle all of the hydrocarbons, thus derived, can be used for the same purpose, i.e., they are combustible, however the best use for some of the solid products may be for other purposes, i.e., lubrication, constructing impervious surfaces, etc. The fact that some petroleum derivatives are best used for different purposes introduces the possibility that they may be legitimately considered as co-products. However, in nature the hydrocarbons in petroleum can be converted into various proportions of the various constituents of the mixture depending on the conditions of heat pressure, and confinement experienced by the material. Under high enough conditions of heat and pressure deep within the earth all petroleum is converted to natural gas (Tissot and Welte, 1978) illustrating that its essential nature is that of a single material. Therefore we conclude that the weight-of-evidence given above indicates that the density separation of crude oil into oil-based fuels is more similar to a split than it is to a co-product.

Now we have to choose between a pure split and the “grey-zone” hypotheses presented above, which introduces elements of the co-product algebra into the calculation. The former is much easier to use, while the latter is perhaps more precise, since the possibility of producing each different fuel in the refining process is not exactly 100%. The choice can be made in favour of the pure split hypothesis only if the error in this assumption is reasonably low. Since the cost of treatment is the main factor allowing flexibility in the established production process, the question becomes, “Is it reasonable to assume that this cost does not influence the results too much?” We performed an emergy evaluation of the Falconara plant in Italy (Table 2) to help answer this question. The diagram of the plant is given in Fig. 1, where all the inputs to the process are visualized. The monetary value of oil was included to consider all the costs due to extraction, transportation, etc. These calculations showed that all the emergy investments (equipment, maintenance and methane) to run the refinery processes amount to around 4% of the total emergy required to produce the products. Thus, the emergy investment in processing is small (not the economic one!) compared to the emergy of the products and we can consider the products of the refining process as splits without introducing an unacceptable uncertainty into the calculation.

Table 2 – Energy evaluation of fuels in Falconara API refinery (Italy), referred to 1 t of crude oil in input.

Note	Category and item	Raw data	Units	Emergy/unit (sej/unit)	Emergy (sej)
1	Oil	1	t	2.27E+15	2.27E+15
2	Methane (internal consumptions)	1.04E+09	J	4.35E+04	4.53E+13
3	Maintenance	20.0	€	1.43E+12	2.86E+13
4	Equipment + rest of the refinery	22.5	€	1.43E+12	3.22E+13
5	Acquisition cost (26.16\$/barrel)	153.5	€	1.37E+12	2.10E+14
6	Fuels	3.89E+10	J	66,490	2.59E+15

The fuels produced are considered as a split in energy. Transformities are according to the 9.26E+24 sej/year baseline. Previous transformity of a generic petroleum derived fuel was 64,742 sej/J (which is equal to 66,000 sej/J, when referred to the 9.44E+24 sej/year baseline). Note 1: Total quantity of oil treated in 1 year: 3,643,093 t, but the analysis is referred to 1 t of crude oil in input. Note 2: Methane (for refinery processes): 3.80E+15 J (assuming 1.04E+09 J/t). Note 3: Maintenance: 20.0 €/t. Note 4: Equipment and other costs: 22.5 €/t. Note 5: Acquisition cost: 2.62E+01 \$/barrel, equal to 153.5 €/t (1 € = 1.2439 US\$ in 2004; 1 t = 7.3 barrels). Note 6: Total fuels, excluding gases for internal use, produced by Falconara Plant (average 2001–2004): gasoline, 2.87E+16 J; diesel, 7.23E+16 J; residual fuel oil, 1.49E+16 J; LPG, 6.10E+15 J; Bitumen, 1.97E+16 J; total fuels, 1.42E+17 J; fuels per t of oil in input, 1.42 E+17 J/3.63E+6 t = 3.89E+10 J/t.

3.2. Split in mass or in energy?

Now that we have given evidence that oil derived fuels reasonably can be considered splits, we must determine if the split should be made in terms of energy or mass. The former (an energy-based split) is supported by the fact that energy must be conserved and that, while all fuels would have the same transformity, the emergy per mass of the lower quality outputs (lower heat content) would be lower. A split based on energy may also be justified by considering the production process for crude oil. If we assume that crude oil constituents with greater enthalpy require more transformations of energy in geological

processing, they should have higher transformities (or emergy per mass, as in this case).

In support of the latter hypothesis (a mass split) is the fact that oil refining is a process based on distillation (density separation) of a complex mixture. Nonetheless there are two main drawbacks to the mass split:

- (1) We would obtain different transformities for the different fuels by dividing the common emergy per mass of the generic fuel by the energy content per unit mass of each fuel. However, we would obtain higher transformities for lower quality fuel outputs, i.e., fuels with lower calorific

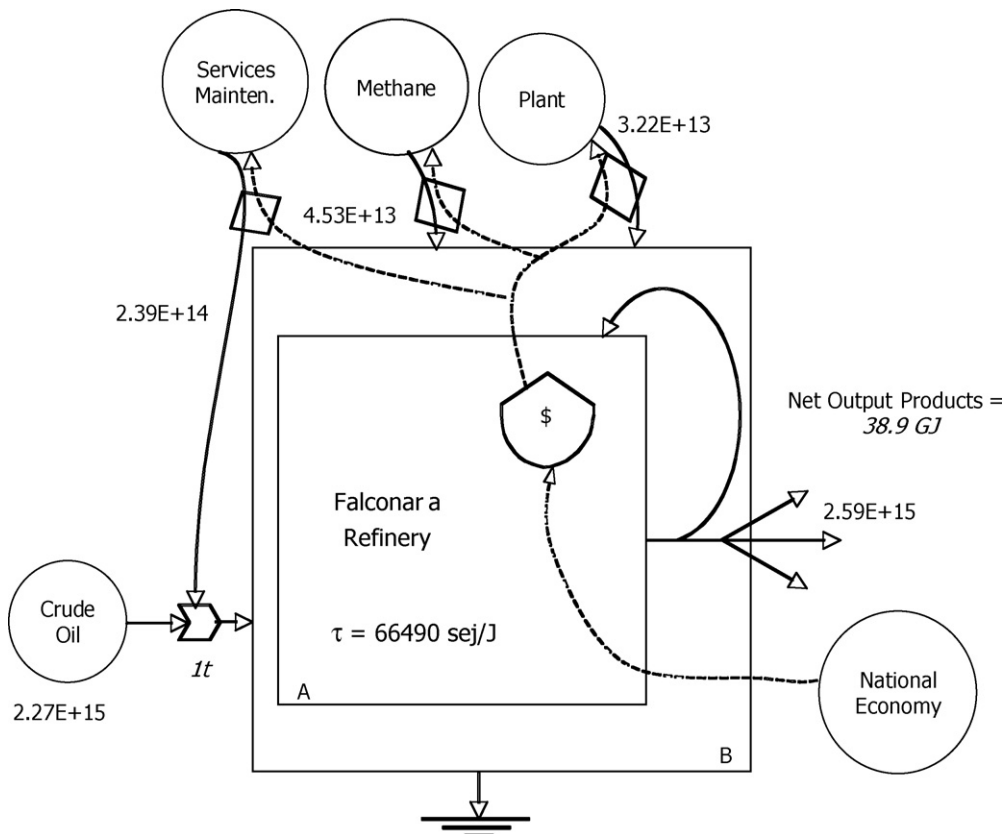


Fig. 1 – An energy diagram of the Falconara refinery system (emergies of the inputs – in sej – are in bold). The analysis was performed using boundary B. Tau, τ , represents the transformity of the generic oil derivative.

Table 3 – Emery analysis of the U.S. refining industry in 2004.

Note	Category and item	Raw data	Units per year	Emery/unit ^a (sej/unit)	Emery (sej/year)
Inputs					
1	Crude oil & additives	3.47E+19	J	54,200	1.88E+24
2	Service in crude oil	1.54E+11	\$	1.07E+12	1.64E+23
3	Natural gas	7.42E+17	J	43,500	3.23E+22
4	Electricity	1.31E+14	J	170,400	2.23E+22
5	Coal	1.00E+15	J	39,200	3.92E+19
6	Steam	2.93E+10	g	1.30E+09	3.80E+19
7	Goods and services ^b				3.50E+22
Internal feedbacks					
8	LPG	1.45E+16	J		
8	Distillate	4.70E+15	J		
8	Residual fuel oil	1.33E+16	J		
8	Petroleum coke	5.35E+17	J		
8	Refinery gases	1.05E+18	J		
Outputs					
9	Fuels (net output)	3.27E+19	J	65,256	2.13E+24

Note 1: Weekly crude oil and additive inputs in 1000 barrels (EIA web site accessed 2/2007) were converted to t and then to energy in J assuming that crude oil and the additives were similar in weight and calorific value. Conversion factors were 7.33 barrels per t of crude oil and 43,370 J/g. The transformity of crude oil is the average of the values obtained by Bastianoni et al. (2005) and Odum (1996). Note 2: In 2004 oil sold for an average price of \$34.16 per barrel. However, we chose to use the long-term average price from 1949 to 2006 because we believe it to be a better indicator of the goods and services required for extraction and transportation. The emery to dollar ratio for the U.S. in 2000, 1.07E+12 sej/\$, was used to convert the dollars paid for the oil to emery assuming that U.S. average value of human service was appropriate to estimate the emery needed to extract and transport the oil to the refineries. Note 3: Natural gas use in the U.S. refining industry was 6.75E+11 cu.ft in 2004 (Table 37 in EIA, 2004). We used an average energy content of 1.1E6 J/cu.ft and 43,500 sej/J (the average of Bastianoni et al. (2005) and Odum (1996)) was used to convert cubic feet of natural gas to emery. Note 4: The U.S. refining industry used 3.64E+10 kWh of electricity in 2004. We converted this value to J and applied the transformity 170,400 sej/J (Campbell et al., 2005). Note 5: The U.S. refining industry used 3.40E+10 g of coal in 2004. We assumed an average energy content of 29,400 J/g and a transformity of 39,200 sej/J (Campbell et al., 2005). Note 6: The specific emery of steam was determined from an emery analysis of a combined cycle natural gas power plant (Raugei et al., 2005). A rough value for industrial steam was obtained as follows: Exergy of the fuel 3.80E+16 J, grams of steam delivered 1.27E+12 g, transformity of natural gas, 43,500 sej/J; the specific emery of steam to run the turbines is then 1.65E+21 sej/1.27E+12 g steam or 1.3E+9 sej/g. Note 7: The dollar value of goods and services purchased was estimated from the goods and services required per t of gasoline produced at 5 San Francisco Bay Refineries from 1996 to 1998. The U.S. emery to dollar ratio for 1997, 1.20E+12 sej/\$, was used to estimate the emery of the goods and services required to refine a t of gasoline. Note 8: Fuel use data from Table 37 in EIA/Petroleum Supply Annual 2004, Volume 1. This data includes all fuel use and all non-processing losses of crude oil and petroleum products including spills, fires, contamination, etc. Note 9: This includes 3.23E+8 t of gasoline, for the production of which the system is optimized.

^a Emery per unit values are relative to the 9.26E+24 sej/year planetary baseline (Campbell, 2000).

^b Extrapolated from the emery of goods and services, labor and investments needed per t of gasoline in San Francisco refineries (see Table 4).

value, which is a result that would be inconsistent with theory, if the products are different.

- (2) Under certain circumstances it might be possible to violate the energy conservation principle (1st law of thermodynamics), since we could (in principle) “choose” to obtain only the highest calorific value products (e.g. gas) and therefore create energy with respect to the average barrel of oil used as input (i.e. a set of products with a total energy content higher than the energy content of a barrel of crude oil).

Therefore, we assigned emery in the split of crude oil constituents in refining on an energy basis. If done in this manner the transformity of the constituents will be the same, and the difference in specific emergies reflects the relative effectiveness of their action in use.

3.3. Calculation of transformities and specific emergies

The results of our analyses are presented in the following order:

- (i) The Falconara calculations and results, i.e., transformity of the generic fuel.
- (ii) Analysis of the U.S. refining industry (average 1993–2004),
- (iii) Estimation of the average energy and material inputs to the U.S. refining industry from 1993 to 2004 based on a complete analysis using 2004 data and estimation of services in the U.S. refining industry from 1993 to 2004 using data from 5 refineries in the San Francisco Bay area.
- (iv) Results of U.S. 1993–2004 refining industry (transformity of generic fuel).
- (v) Comparison of U.S 1993–2004 results with Falconara results and calculation of the average of transformity and specific emergies (emery per mass).
 - (i) The total emery supporting the process of refining 1 t of oil in the Falconara plant is 2.59E+15 sej (Table 2), around 95% of which is directly or indirectly due to the crude oil input (including extraction and transportation costs). The energy content of the mix of outputs is 3.89E+10 J/t of input. The common transformity for the fuels obtained in the Falconara plant is therefore 66,490 sej/J (Table 2).

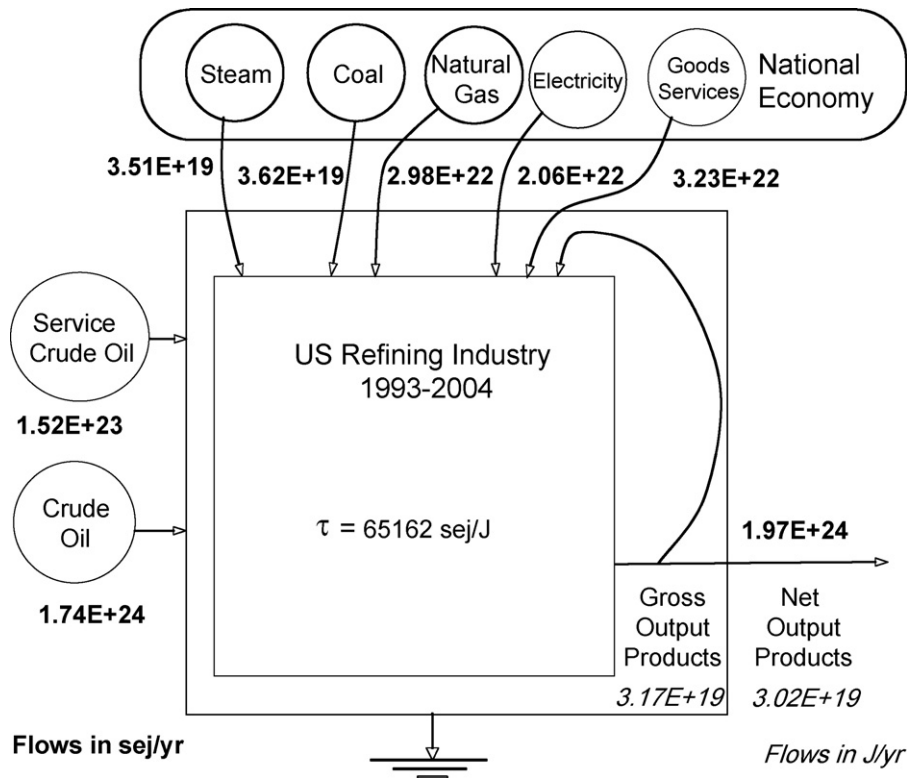


Fig. 2 – Energy diagram of the U.S. refining industry (1993–2004). Emergies are in bold; energies in italic. Tau, τ , represents the transformity of the generic oil derivative.

- (ii) An Emergy evaluation for the U.S. refining industry from 1993 to 2004 is represented in Fig. 2, in which all the inputs and their emergy content are shown. Since the whole set of data for the periods 1993–2004 was not available, estimates of the material and energy inputs required for refining crude oil in the U.S. industry were taken from detailed data for 2004 (Table 3), while an estimate of goods and services used by the U.S. refining industry was extrapolated from an analysis of 5 refineries in the San Francisco Bay area (see Table 4, data from Quinn, 2001).
- (iii) Data from the five refineries in San Francisco area (1996–1998) demonstrated that the cost of refining oil in the United States was a small part (around 2%) of the emergy contained in the products (inputs 7–9 in Table 4). From Table 4 we deduced an emergy input from goods & services, investment and human labor per t of gasoline (the output for which the plant is optimized, 1.87E7 t/year) of 1.08E+14 sej/t of gasoline. This result led to the estimate of the emergy of goods & services, investment and human labor for U.S. refining industry in 2004 (input 7 in Table 3). The values of the transformity in these two cases are calculated but not used in this paper. They can be used in particular cases since they are site specific (San Francisco Bay area, with a transformity of 64,527 sej/J of generic fuel) or referred to 1 year (U.S. 2004, with a transformity of 65,256 sej/J of generic fuel).
- (iv) The material and energy inputs other than crude oil for the U.S. refining industry (1994–2004) were extrapolated from the analysis of 2004 (Table 3), considering the ratios of each input to crude oil (in 2004) and multiplying them by the average amount of crude oil in 1993–2004. Material and energy inputs represent 2.56% of the total emergy, while 1.64% of the emergy inputs are from investments, services and labor, corroborating the results of the analysis of Falconara. In contrast, 7.7% of the emergy required is supplied by the services of extracting and transporting the oil to the refinery and the remainder (around 88%) resides in the crude oil itself (Fig. 2).
- The total average emergy driving the U.S refining industry in the periods 1993–2004 is 1.97E+24 sej/year. In the same period the net output of the system was 3.02E+19J/year that implies an average transformity for petroleum derivatives equal to 65,162 sej/J.
- (v) The transformity of the generic fuel for the U.S. refining industry (1993–2004) is around 2% lower than the estimate for fuels produced at Falconara (66,490 sej/J). This difference is practically negligible and leads to an average transformity of 65,826 sej/J, with a standard error of 1.4%. This value is only 1.7% higher than the transformity obtained by Odum (64,742 sej/J according to 9.26E+24 sej/year baseline) by means of considerations on

Table 4 – Emery analysis of five San Francisco Bay Refineries (1996–1998).

Note	Category and item	Raw data	Units per year	Emery/unit ^a (sej/unit)	Emery (sej/year)
Material inputs					
1	Crude oil & additives	1.59E+18	J	54,200	8.63E+22
2	Natural gas	4.26E+16	J	43,500	1.85E+21
3	Electricity	7.51E+12	J	170,400	1.28E+21
4	Coal	5.73E+13	J	39,200	2.25E+18
5	Steam	1.68E+09	g	1.30E+09	2.18E+18
Service inputs					
6	Service in crude oil	4.61E+09	\$	1.20E+12	5.53E+21
7	Goods and services	8.21E+08	\$	1.2E+12	9.86E+20
8	Labor	1.43E+13	J	4.80E+07	6.60E+20
9	Investment	3.00E+08	\$	1.2E+12	3.60E+20
Internal feedbacks					
10	LPG	8.33E+14	J		
10	Distillate	2.70E+14	J		
10	Residual fuel oil	7.65E+14	J		
10	Petroleum coke & gases	8.81E+16	J		
Outputs					
11	Fuels (net output)	1.50E+18	J	64,527	9.70E+22

Note 1: Crude oil and additive use by 5 major San Francisco Bay area refineries in 1998 reported as 294,001 thousand barrels (Quinn, 2001). The weight of crude oil was determined from the weighted average of the products and its energy using 43,370J/g and 7.33 barrels per t. Note 2: Natural gas used per t of gasoline produced in the U.S. refining industry in 2004 (2087.63 cu.ft/t) was used to estimate Bay area refinery gas use. We used an average energy content of 1.1E+6J/cu.ft and 43,500 sej/J (average of Bastianoni et al., 2005; Odum, 1996) to convert cubic feet of natural gas to emery. Note 3: Electricity use per t of gasoline produced in the U.S. refining industry in 2004 (4.05E+8J/t) was used to estimate electricity used by the Bay area refineries. See Table 3 corresponding note. Note 4: Coal use per t of gasoline produced in the U.S. refining industry in 2004 (105.1 g/t) was used to estimate Bay area refinery use. See Table 3 corresponding note. Note 5: Steam use per t of gasoline produced in the U.S. refining industry in 2004 (90.6 g/t) was used to estimate Bay area refinery use. See Table 3 corresponding note. Note 6: A value for crude oil and additives was reported by Quinn (2001) for 1996–1998. We used the average value for these 3 years. The emery to dollar ratio for the U.S in 1997 (Campbell et al. (2005) was used to convert the dollars paid for the oil to an estimate of the emery used in extraction and transportation. Note 7: The monetary value of goods and services purchased was reported by Quinn (2001) as 1.1 billion dollars. We reduced this cost by the value of labor to avoid double counting. Note 8: The joules of labor required per year were calculated based on 2500 kcal/day for human labor and a 6-day work week with 2 weeks of paid vacation. The transformity of labor was taken as an average between college and high school (Odum, 1996; Campbell et al., 2005). Note 9: Quinn (2001) gives an average of \$300,000 per year in investment. Note 10: Use of internal feedbacks in San Francisco Bay area refineries was estimated on the basis of the amount of feedbacks needed per t of gasoline produced in the U.S. refining industry in 2004. Note 11: This includes 1.85E+7 t of gasoline, for the production of which the plants are optimized.

^a Emery per unit values are expressed relative to the 9.26E+24 sej/year planetary baseline (Campbell, 2000).

the different efficiencies of coal and oil in electricity production (see Odum, 1996).

In order to obtain the (different) values of the emery per mass of the different fuels we used the IPCC (2006) classification and data of calorific values (Table 5). High enthalpy refinery gases have the highest specific emery value (average 3.26E+9 sej/g), while low calorific value products (e.g. bitumen and lubricants) have an average emery per mass of 2.634E+9 sej/g; the most commonly used fuels, gasoline and diesel, have average emery per mass 2.92E+9 and 2.83E+9 sej/g, respectively (Table 5).

3.4. Evaluation of the uncertainty of the energy versus mass split models using 2004 data from the U.S. refining industry

Now that the final results are given, we introduce a section in which we investigate the effects of the choices we made on the results. For example, to better understand the role of model uncertainty, we provide a white box representation (in which splits feeding back in the production process are explic-

itly accounted for), using an energy versus a mass split in the evaluation of transformities and specific emergies for the U.S. refining industry in 2004 (Fig. 3a and b). Table 3 shows the calculation of transformity for liquid fuels derived from the energy split model using 2004 data for U.S. refineries. In this case all the feedbacks were neglected and only the net output was considered for the calculation of transformity and emery per mass. When using a white box model, the main output (liquid fuels) is determined as result of the external inputs plus the internal feedbacks from solids and gases, leading to a transformity for liquids of 65,636 sej/J (Fig. 3a). The energy split assumption gives liquid fuels the highest transformity with solids and gases each having the same slightly lower (~5%) transformity (Fig. 3a). The fact that liquids and solids-gases have different transformities is due to the fact that gases and solids are fed back to the system in order to produce liquids (the main target of a refinery), therefore adding their emery to the production process. The specific emergies follow a trend with liquid fuels having a specific emery considerably greater than solids (~25%), but less than gases (~7%) consistent with the higher heat value per unit mass for the gas. Nevertheless transformities of gases and solids are not significant since the

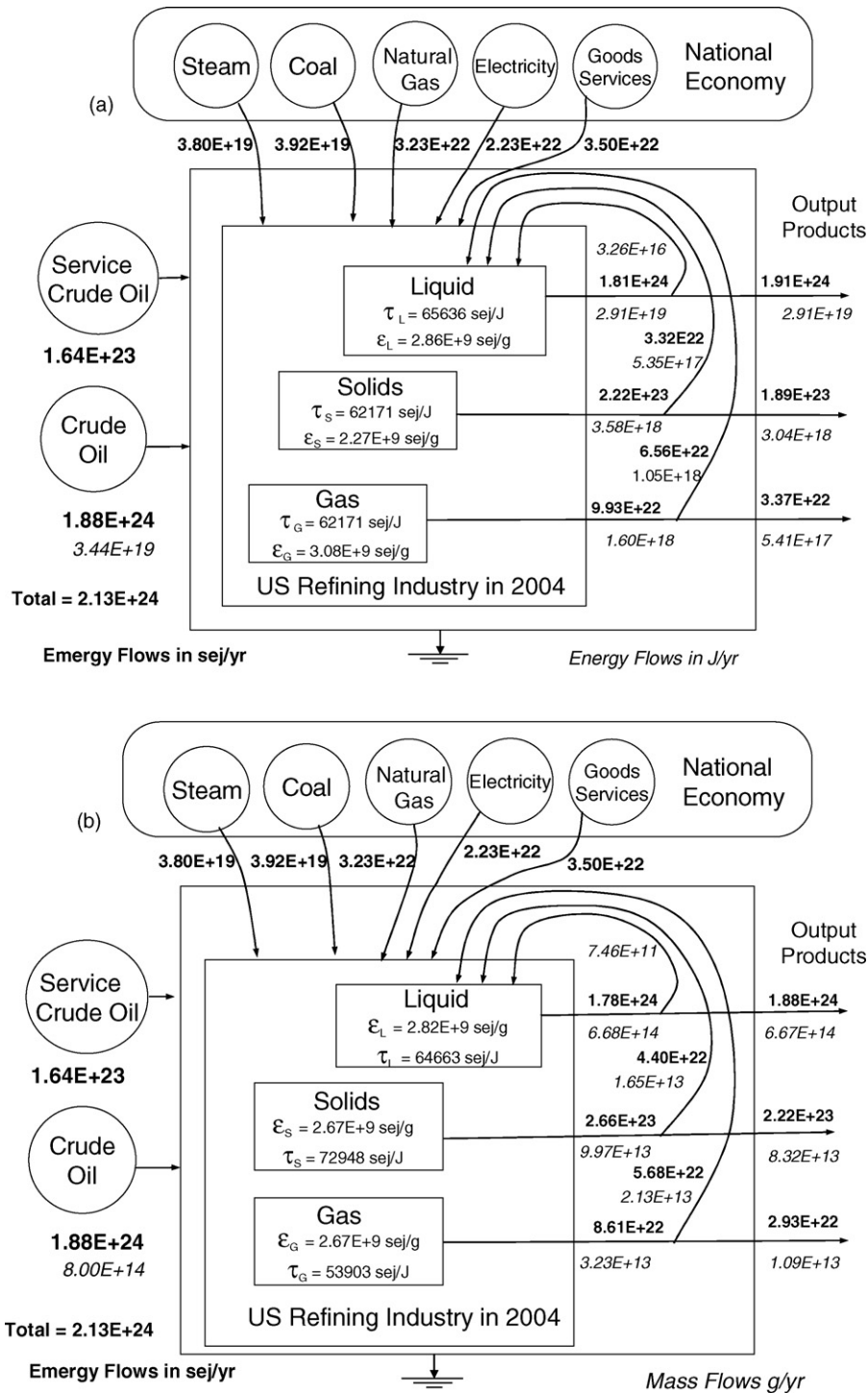


Fig. 3 – (a and b) White box energy diagrams of the U.S. refining industry in 2004, considering energy split (a) and mass split (b). The emergy of liquids is derived by adding the emergy contributions of gases and solids (feedbacks) necessary for their production. Emergies are in bold; energies in italic.

process is not optimized for their production and they are just considered as additional production factors. In fact the use of feedbacks substitutes for the use of additional inputs from outside the system.

The mass split (Fig. 3b) gives gases the lowest transformity (53,903 sej/J) and solids the highest (72,948 sej/J) with liquids

in an intermediate position (64,663 sej/J). This pattern may be consistent with theory, if solids, liquids and gases are viewed as the same product, i.e., a combustible substance. In this case the higher the heat value the lower the transformity, indicating that a joule of combustible substance in a gas is made more efficiently in the refining process than a joule of

Table 5 – The emergy per mass of the various refined crude oil products (adapted to the USA classification).

Refinery products	Calorific value (kJ/g)	Specific emergy (sej/g)		
		U.S.	Falconara	Average
Liquefied gases	47.3	3.08E+09	3.14E+09	3.11E+09
Motor gasoline	44.3	2.89E+09	2.95E+09	2.92E+09
Aviation gasoline	44.3	2.89E+09	2.95E+09	2.92E+09
Kerosene-type jet fuel	44.1	2.87E+09	2.93E+09	2.90E+09
Kerosene refinery	43.8	2.85E+09	2.91E+09	2.88E+09
Total distillate (diesel)	43.0	2.80E+09	2.86E+09	2.83E+09
Residual fuel oil	40.4	2.63E+09	2.69E+09	2.66E+09
Other oils for petrol. feed	40.2	2.62E+09	2.67E+09	2.64E+09
Lubes	40.2	2.62E+09	2.67E+09	2.64E+09
Waxes	40.2	2.62E+09		
Petroleum coke	32.5	2.12E+09		
Asphalt	40.2	2.62E+09	2.67E+09	2.64E+09
Still gas	49.5	3.23E+09	3.29E+09	3.26E+09
Miscellaneous	40.2	2.62E+09		

Calorific values are from IPCC (2006). Emergy per mass (in sej/g) is obtained multiplying the transformities (66,490 sej/J for Falconara and 65,162 sej/J for U.S. 1993–2004), common for all the fuels, by the calorific value of each fuel (J/g). Values based on an energy split of the emergy requirement. With respect to the average, the standard error varies from 1.31% to 1.53%.

liquid, which in turn is made more efficiently than solid fuel. If the petroleum derivatives are viewed as different products, then the transformities based on a mass split are inconsistent with theory. This partial evaluation whether based on mass or energy provides highly uncertain estimates for the transformities of solid and gaseous petroleum derivatives because both solids and gases are consumed in a refining process which is optimized to make liquid fuel. Comparing the results of the two white box scenarios, the transformity and specific emergy of liquid fuels differ by only 1.5% as a result of using an energy or a mass split to assign emergy. The energy split gives a larger value for transformity and a smaller value for specific emergy than does the split based on mass.

4. Conclusions

In this study the calculation of the transformity and of the specific emergies (emergy per mass) of the fuels derived from crude oil, was carried out. The most debated issue for this purpose was how to consider the fuels, i.e., are the petroleum derivatives splits or co-products. Both conceptual and practical considerations converged towards the split hypothesis. This fact allows us to sum the emergies of all the different fuels that feed the same process without problems of double counting. Within the split category emergy was split based on energy rather than mass for several reasons, chief among them was so that the 1st Law of Thermodynamics is in all cases satisfied. Using an energy split we found that the higher the quality (calorific value) of a fuel the higher its emergy per unit mass, which is also evidence that the emergy split based on energy is reasonable.

The evaluations were carried out using data from two regional refinery systems (Falconara, Italy and the San Francisco Bay area, USA) and a national system (the refining industry in the USA). All the results were consistent: so we suggest using a transformity of 65,826 sej/J, the average of the Italian and U.S. systems (1993–2004), for use in emergy anal-

yses where the origin of petroleum fuels is unknown. The standard error of this result is 1.4%, which is a rough indicator of the uncertainty of the estimate.

Emergy evaluation has received criticism for the calculation of the transformities, sometimes thought to be too fuzzy, i.e., with unspecified uncertainty. In this study we believe that we have made a modest contribution to strengthen the methodology, providing data for some of the most important inputs in the evaluation of systems controlled by human activities and interests that includes a 1st order estimate of the uncertainty in both data and models. These new figures reinforce the validity of previous analyses, since the transformity value derived in a different manner by Odum was only slightly different from the results of this study.

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