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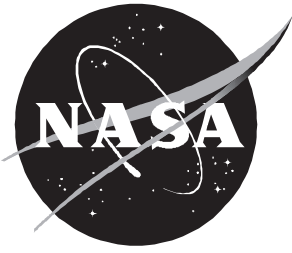


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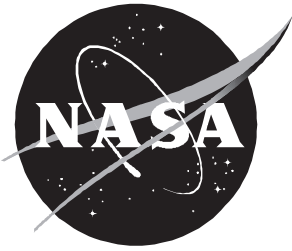
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Abstract

The δ -ray theory of track structure is compared with experimental data for the radial dose from heavy ion irradiation. The effects of electron transmission and the angular dependence of secondary electron ejection are included in the calculations. Several empirical formulas for electron range and energy are compared in a wide variety of materials in order to extend the application of the track-structure theory. The model of Rudd for the secondary electron spectrum in proton collisions, which is based on a modified classical kinematics binary encounter model at high energies and a molecular promotion model at low energies, is employed. For heavier projectiles, the secondary electron spectrum is found by scaling the effective charge. Radial dose calculations for carbon, water, silicon, and gold are discussed. The theoretical data agreed well with the experimental data.

Introduction

The δ -ray theory of track structure attributes the radiation damage from and the detection of the passage of heavy ions through matter to the ejection of electrons (δ rays) from the material by the passing ion (refs. 1–5). The track-structure theory has a long history of providing the correct description of a variety of phenomena associated with heavy ion irradiation. Track-structure theory provided the first description of the spatial distribution of energy deposition from ions by a formula for the radial distribution of dose, as introduced by Butts and Katz (ref. 1) and Kobetich and Katz (ref. 2). This description led to many experimental measurements of the radial dose (refs. 6–10). The response of physical detectors, such as organic scintillators (ref. 5), thermoluminescence detectors (TLD's) (ref. 5), alanine (ref. 11), nuclear emulsion (ref. 12), and the Fricke dosimeter (refs. 5 and 13), to heavy ions has been described with track-structure theory. Many biological effects, such as the thindown of mammalian cells (ref. 5), which was predicted nearly 20 years prior to the first experimental observation (ref. 14) have also been described. Track-structure theory is used to develop improved lithography methods by using ion beams for applications in microelectronics and microtechnology (ref. 15).

The radial dose distribution and the geometry of a target site are used in track-structure theory to map γ -ray response to ion response. The radial dose for intermediate distances from the track structure is known to decrease with the inverse square of the radial distance to the path of the ion, which has led to simplified formulas for many applications (refs. 1, 5, 16, and 17). The radial dose both near and far from the path of the ion is difficult to predict because of uncertainties in the electron range and energy relation, the angular dependence of the secondary electron production cross section, and the effects of δ -ray transport in matter, especially for

condensed-phase matter. However, many track-structure calculations have used simple, analytic forms for the radial dose from ions. The electron transmission and the angular dependence of electron ejection are ignored and simplified electron range-energy relations are used. In this paper, these factors are considered by following the method described in references 2, 3, and 17 and comparisons are made to experimental data for radial dose distributions. Substantial changes in the physical inputs of the calculations were made. These changes include an improved model for the secondary electron spectrum for proton collisions with atoms and molecules (ref. 19) and improved formulas for the electron range-energy and the stopping power.

Radial Dose Formalism

The calculation of the radial dose $D(t)$ as a function of the radial distance of the path of an ion of charge number Z and velocity β was formulated in references 2 to 4 and 18. In formulating the spatial distribution of energy deposition as charged particles pass through matter, the dominant mode of energy loss is assumed to be ionization due to electron ejection from the atoms of the target material. Electrons of range r that penetrate into a material a distance t have residual energy W , which is given by the energy ω to go the residual range $r - t$. The residual energy of an ejected electron (δ ray) is written in functional form as

$$W(r, t) = \omega(r - t) \quad (1)$$

In equation (1), r is the practical range (determined by extrapolating the linear portion of the absorption curve to the abscissa) of an ejected electron with energy ω . When the range-energy relation in a given target material is known, the residual energy is then evaluated with equation (1).

The energy dissipated E at a depth t by a beam containing one electron per cm^2 is represented in reference 2 as

$$E = \frac{d}{dt}(\eta W) \quad (2)$$

where η is the probability of transmission of the electrons.

As noted in reference 4, equation (2) neglects several effects. First, it may neglect backscatter, although it may be argued that the energy lost from a layer dt by backscatter is compensated by energy gained from backscatter from later layers. Second, all electrons are represented by an underscatter class. Third, the energy deposited by the electrons that penetrate to a thickness $t > r$ is neglected. Such shortcomings could be overcome by direct solution of the electron transport (ref. 20) or through the use of Monte Carlo methods (ref. 21). However, the model of Kobetich and Katz from reference 2 has the advantage of simplicity with reasonable accuracy.

The transmission function used is based on the expressions of Dupouy et al. (ref. 22) as modified by Kobetich and Katz (ref. 4) and is given by

$$\eta(r, t) = \exp[-(qt/r)^p] \quad (3)$$

with

$$q = 0.0059 Z_T^{0.98} + 1.1 \quad (4)$$

and

$$p = 1.8 (\log_{10} Z_T)^{-1} + 0.31 \quad (5)$$

where Z_T is the atomic number of the target material, and r and t are in units of g/cm^2 .

In order to estimate the number of free electrons ejected by an ion per unit length of ion path with energies between ω and $\omega + d\omega$, the formula given by Bradt and Peters (ref. 23) was used by Kobetich and Katz (ref. 2)

$$\frac{dn}{d\omega} = \frac{2\pi NZ^* e^4}{mc^2 \beta^2} \frac{1}{\omega^2} \left[1 - \frac{\beta^2 \omega}{\omega_m} + \frac{\pi \beta Z^{*2}}{137} \sqrt{\frac{\omega}{\omega_m}} \left(1 - \frac{\omega}{\omega_m} \right) \right] \quad (6)$$

where e and m are the electron charge and mass, N is the number of free electrons per cm^2 in the target, and ω_m is the classical kinematic value for the maximum energy that an ion can transfer to a free electron and is given by

$$\omega_m = \frac{2mc^2 \beta^2}{1 - \beta^2} \quad (7)$$

In equation (6), Z^* is the effective charge number of the ion, which was represented in reference 24 as

$$Z^* = Z \left[1 - \exp\left(\frac{-125\beta}{Z^{2/3}}\right) \right] \quad (8)$$

The electron-binding effects were considered by Kobetich and Katz (ref. 2) after the experimental findings of Rudd et al. (ref. 25), who found that ω may be interpreted as the total energy imparted to the ejected electron with a kinetic energy of W , so that ω in equation (6) is replaced by

$$\omega = W + I \quad (9)$$

Results from equation (6) must be summed for composite materials. The average charge and mass number and the density of several materials are listed in table 1. Values of mean excitation I_i from references 26 and 27 and values for electron density N_i are listed in table 2.

Rudd has provided a parameterization of the electron spectrum after proton impact that was based on a binary encounter model modified to agree with the Bethe theory at high energies and with the molecular promotion model at low energies (ref. 19). For water, the contributions from five shells are included (ref. 19). This model of Rudd is considered herein and scaled to heavy ions by using effective charge. In figure 1, the secondary electron spectrum from equation (6) and the model of Rudd for several proton energies are shown. Large differences between the models occur for all electron energies below proton energies of about 1 MeV and for small electron energies at all proton energies.

Electrons of energy ω are ejected at an angle θ relative to the path of a moving ion and described by classical kinematics as

$$\cos^2 \theta = \frac{\omega}{\omega_m} \quad (10)$$

for the collision between a free electron and an ion. Equation (10) indicates that close to the path of the ion, where distances are substantially less than the range of δ rays ($\omega \ll \omega_m$), it is sufficient to consider that all δ rays are normally ejected. The energy that the electrons dissipate in cylindrical shells with an axis along the path of the ion may then be found from the energy dissipation of normally incident electrons. If the δ rays far from the path of an ion have an important role in a particular response, then the angular dependence, as well as the dependence of electron range, on the velocity of the ion becomes crucial.

If ϵ is the energy flux carried by δ rays through a cylindrical surface of radius t whose axis is the path of

the ion, the energy density E deposited in a cylindrical shell of unit length and mean radius t is given by

$$E = \frac{-1}{2\pi t} \frac{d\varepsilon}{dt} \quad (11)$$

The total energy flux is found by integrating the energy flux carried by a single electron, given by ηW , over the distribution of the δ ray and summing the contributions of all atoms in the material

$$\varepsilon(t) = \sum_i \int_{\omega_t}^{\omega_m - I_i} d\omega W(t, \omega) \eta(t, \omega) \frac{dn_i}{d\omega} \quad (12)$$

In equation (12), the lower limit ω_t is the energy for an electron to travel a distance t , and the upper limit $\omega_m - I_i$ is the maximum kinetic energy that can be given to the electron by the passing ion. Using equation (11) and equation (12), the energy density distribution may be written as

$$E(t) = \frac{-1}{2\pi t} \sum_i \int_{\omega_t}^{\omega_m - I_i} d\omega \frac{\partial}{\partial t} [\eta(t, \omega) W(t, \omega)] \frac{dn_i}{d\omega} \quad (13)$$

and $E(t)$ is identified as the radial distribution of dose.

To consider the angular dependence of the ejected electrons, the energy deposited by a ray ejected at an angle θ in a cylindrical shell of radius t centered on the path of the ion is assumed to be the same as the energy deposited by an electron normally incident on a slab at depth $t/\sin\theta$, as shown in figure 2. Kobetich and Katz assume that differences between the geometry of the slab and the cylindrical shell do not greatly affect the energy density distribution, because the differences in the energy density at t caused by the electrons scattered in path A are compensated by those scattered in path B of figure 2 (ref. 3).

The energy density distribution, which includes an angular distribution of the ejected electrons, is assumed to be

$$E(t) = \frac{-1}{2\pi t} \sum_i \int d\Omega \int_{\omega_t(\theta)}^{\omega_m - I_i} d\omega \frac{\partial}{\partial t} \times [\eta(t, \omega, \theta) W(t, \omega, \theta)] \frac{dn_i}{d\omega d\Omega} \quad (14)$$

The angular dependence of ω_t , η , and W is shown in equation (10). Experimental measurements for the double differential cross section of electron ejection are available for only a few ions and mostly at modest ion energies of <10 MeV/amu (refs. 28–31).

A qualitative model for the angular distribution of the secondary electrons assumes that distribution peaked

about the classical kinematic ejection value described by equation (10), so that

$$\frac{dn}{d\omega d\Omega} = \frac{dn}{d\omega} f(\theta, \omega) \quad (15)$$

where

$$f(\theta, \omega) = \frac{N}{[\theta - \theta_c(\omega)]^2 + \frac{K}{\omega}} \quad (16)$$

with $\theta_c(\omega)$ determined as the root of equation (10), N is a normalization constant, and K is a constant. The constant K may have some dependence on the energy of the incident ion and target material; however, K is estimated as 0.015 keV from the data of references 28 to 31. Results of equations (15) and (16), which use the model of Rudd (ref. 19) for $dn/d\omega$ in equation (15), are shown in figures 3(a) and 3(b).

Range and Energy Formula in Arbitrary Media

The electron range and energy relationship is difficult to evaluate theoretically and, because of the complexity of the electron transport problem, empirical expressions based on experimental measurements have been developed (refs. 2, 4, and 32–36). Over a limited energy range, a power law of the form $r = k\omega^\alpha$ will be approximately correct and is used in references 1, 34, and 36. The residual range of the power law is easily found by inversion and leads to an analytic form for the radial distribution of dose with the simplifying assumptions of normal ejection and unit electron transmission. A more accurate form, which is given in reference 32 and modified in reference 4, is the formula

$$r = A\omega \left[1 - \frac{B}{1 + C\omega} \right] \quad (17)$$

where

$$A = \left(0.81Z_T^{-0.38} + 0.18 \right) \times 10^{-3} \text{ g} \left(\text{cm}^2 \cdot \text{keV} \right)^{-1} \quad (18)$$

$$B = 0.21Z_T^{-0.555} + 0.78 \quad (19)$$

$$C = \left(1.1Z_T^{0.29} + 0.21 \right) \times 10^{-3} \text{ keV}^{-1} \quad (20)$$

which was determined by extensive comparison with experimental data for practical range in many materials. Equation (17) is inverted to provide $\omega = \omega(r)$.

As a final parameterization, the range formula of reference 33 is considered

$$r = a_1 \left[\frac{1}{a_2} \log(1 + a_2 \tau) - a_3 \tau (1 + a_4 \tau^{a_5}) \right] \quad (21)$$

where

$$\begin{aligned} \tau &= \omega/m \\ a_1 &= b_1 A_T / Z_T^{b_2} \\ a_2 &= b_3 Z_T \\ a_3 &= b_4 - b_5 Z_T \\ a_4 &= b_6 - b_7 Z_T \\ a_5 &= b_8 / Z_T^{b_9} \end{aligned} \quad (22)$$

The values of b_i from reference 33 are listed in table 3. Equation (21) reduces to equation (17) when $a_2 \tau \ll 1$ and $a_5 = 1$. A parameterization of the inversion of equation (21) is provided in reference 33 as

$$\tau = c_1 \left(\exp \left\{ r \left[c_2 + c_3 / (1 + c_4 r^{c_5}) \right] / c_1 \right\} - 1 \right) \quad (23)$$

where

$$\begin{aligned} c_1 &= d_1 / Z_T \\ c_2 &= d_2 Z_T^{d_3 / A_T} \\ c_3 &= d_4 - d_5 Z_T \\ c_4 &= d_6 / Z_T^{d_7} \\ c_5 &= d_8 / Z_T^{d_9} \end{aligned} \quad (24)$$

with d_i listed in table 3.

A logarithm and polynomial relationship has been used by Iskef, et al. (ref. 35) and more recently by Zhang, et al. (ref. 36). This, however, is less useful for the radial dose model because the inversion formula for $\omega = \omega(r)$ is not found easily.

In figures 4 to 6, electron range and the energy of the ion from equation (7) is plotted for several materials. In the low to intermediate energy range, the formula agrees closely; however, large differences occur below 1 MeV/amu, especially for lighter materials. Above 1000 MeV/amu, large differences also occur which grow with the increasing charge of the target material. In figure 7, the formulas of Iskef et al. (ref. 35), Waligorski et al.

(ref. 37), Kobetich and Katz (ref. 4), and Tabata et al. (ref. 33) for water are also shown. In figure 8, dW/dr from equation (17) or equation (21) is compared with experimental data from references 38 and 39 for stopping power of an electron in water. The model of Tabata et al. (ref. 33) agrees well with experimental data to about 1.0 keV. This model will be used for the electron range energy in radial-dose calculations.

Calculations of Radial Dose

In figures 9(a) and 9(b), the effects of electron transmission on calculations of radial dose in water are shown. Calculations are for proton projectiles; however, the radial dose is determined approximately by Z^{*2}/β^2 from which results for other ions can be found. Figures 9(a) and 9(b) illustrate that the transmission factor affects the radial dose calculation only very close to and very far from the path of the ion. The normalization and the expected decrease of radial dose with increasing distance as $1/t^2$ are unchanged by including the transmission factor.

In figure 10, the radial dose calculations are compared with experimental data from references 6 to 9 for several projectiles with ion energies from 0.25 to 377 MeV/amu. Figure 10 illustrates the decrease in radial dose with increasing distance $1/t^2$ in the intermediate distance range. Close to the ion track ($t < 10$ nm) a contribution to the radial dose from molecular excitations, as discussed in reference 37, is expected but is not included in the present calculations. It is important to keep the contributions from excitation and ionizations distinct, because the secondary electron dose from ionization is assumed to be responsible for physical effects by heavy ions.

At large distances, the inclusion of angular dependence in equation (14) offers a substantial improvement in the accuracy of calculations. Equation (15) provides an improvement in accuracy over the ejection angle model of classical kinematics (eq. (10)) at lower energies (< 2 MeV/amu). At higher energies, equation (15) appears to underestimate the radial dose at large distances. Clearly, more information on the double differential cross section for electron ejection is required.

In figures 11(a) to 11(c), the effects of the radial dose calculations for several velocities in carbon, silicon, and gold are illustrated. The data shown in figure 11 were determined with equation (6) from the secondary electron spectrum. This model is capable of providing the radial dose for an arbitrary ion in a wide variety of materials.

Concluding Remarks

A model for the radial distribution of energy deposited about the path of a heavy ion developed prior to most experimental measurements of this distribution was improved. Theoretical results from the improved model were compared with experimental data for a variety of ions. Improved models of electron-range energy and stopping power and the electron-ejection spectra and angular distribution were used in calculations. Excellent agreement with experimental data was found; however, more information on the double differential cross section for electron ejection is required. Calculations of the radial dose from heavy ions in several materials of interest for spacecraft design and microelectronics are presented. The radial dose model developed in this report is useful in determining the response of many detectors and components to space radiations.

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Table 1. Average Atomic Number (\bar{Z}), Average Mass Number (\bar{A}), and Density of Materials

Material	Composition ^a	\bar{Z}	\bar{A}	Density, g/cm ³
Carbon	C	6.0	12.0	1.95
Aluminum	Al	13.0	27.0	2.702
Silicon	Si	14.0	28.0	2.33
Copper	Cu	29.0	63.0	8.92
Tin	Sn	50.0	120.0	7.28
Gold	Au	79.0	197.0	19.30
Lead	Pb	82.0	208.0	11.34
Lexan Polycarbonate	C ₁₆ H ₁₄ O ₃	6.1	12.1	1.20
Cellulose Nitrate	C ₆ H ₈ O ₉ N ₂	7.02	14.0	1.35
Water	H ₂ O	7.22	14.3	1.0
Air	0.755N, 0.232O, 0.013Ar	7.52	15.1	0.001293
Quartz	SiO ₂	10.8	21.7	2.66
Muscovite Mica	KAl ₃ Si ₃ O ₁₆ (OH) ₂	11.0	22.4	2.8
Sodium Iodide	NaI	46.6	111.0	3.67
Ilford G-5 Emulsion	0.41H 0.07226C 0.01932N 0.06611O 0.01189S 0.3491Br 0.4741Ag 0.00312I	35.8	81.1	3.815

^aComposition listed by percentage weight.

Table 2. Electron Density and Binding Energy of Several Materials

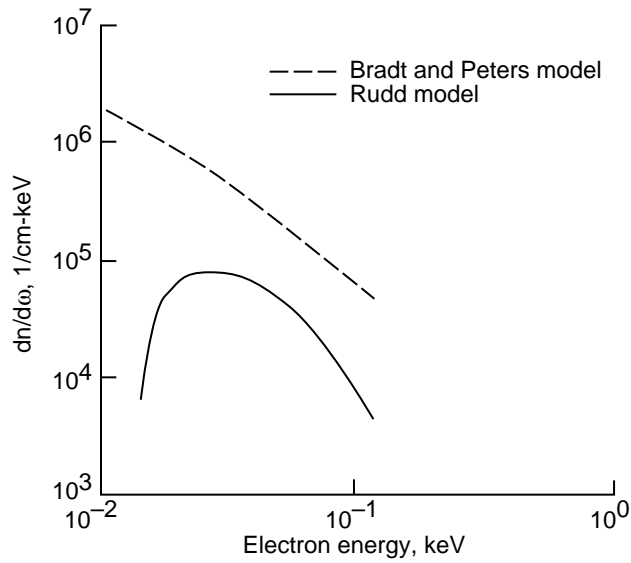
Materials	Composition	^a Electron density $\times 10^{23}$, electrons/cm ³	^a Mean excitation energy $\times 10^{10}$, ergs/electron
Carbon	C	5.86	1.11
Aluminum	Al	7.85	2.61
Silicon	Si	7.00	3.84
Copper	Cu	24.50	5.03
Tin	Sn	18.40	8.27
Gold	Au	46.60	12.23
Lead	Pb	27.10	13.23
Lexan Polycarbonate	C	2.73	1.11
	H	0.397	0.248
	O	0.685	1.43
Cellulose Nitrate	C	1.15	1.11
	H	0.256	0.248
	O	2.30	1.43
	N	0.447	1.36
Water	H	0.675	0.248
	O	2.69	1.43
Air	N	0.00299	1.36
	O	0.000904	1.43
	Ar	0.0000456	2.72
Quartz	Si	3.73	2.72
	O	4.27	1.43
Muscovite Mica	K	0.671	3.36
	Al	1.38	2.61
	Si	1.48	2.72
	O	5.08	1.43
	H	0.0706	0.248
Sodium Iodide	Na	1.62	2.40
	I	7.80	8.65
Ilford G-5 Emulsion	H	0.322	0.248
	C	0.830	1.11
	N	0.222	1.36
	O	0.760	1.43
	S	0.0214	3.04
	Br	3.51	5.93
	Ag	4.74	7.80
I	0.0299	8.65	

^aFrom references 26 and 27.

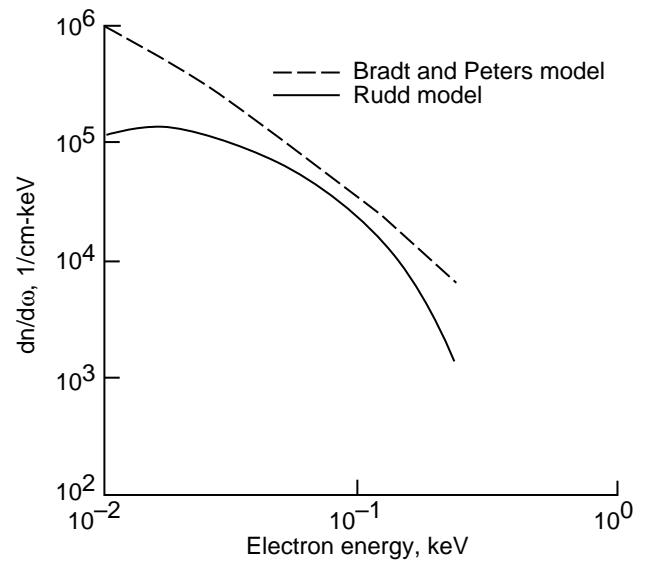
Table 3. Values of Constants b_i and d_i

i	b_i^a	d_i^a
1	0.2335 ± 0.0091	$(2.98 \pm 0.30) \times 10^3$
2	1.290 ± 0.015	6.14 ± 0.29
3	$(1.78 \pm 0.36) \times 10^{-4}$	1.026 ± 0.020
4	0.9891 ± 0.0010	$(2.57 \pm 0.12) \times 10^3$
5	$(3.01 \pm 0.35) \times 10^{-4}$	0.34 ± 0.19
6	1.468 ± 0.090	$(1.47 \pm 0.19) \times 10^3$
7	$(1.180 \pm 0.097) \times 10^{-2}$	0.692 ± 0.039
8	1.232 ± 0.067	0.905 ± 0.031
9	0.109 ± 0.017	0.1874 ± 0.0086

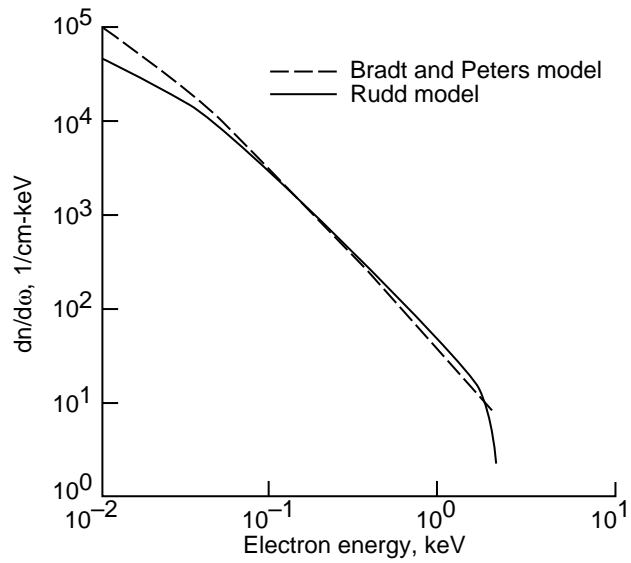
^aFrom reference 33.



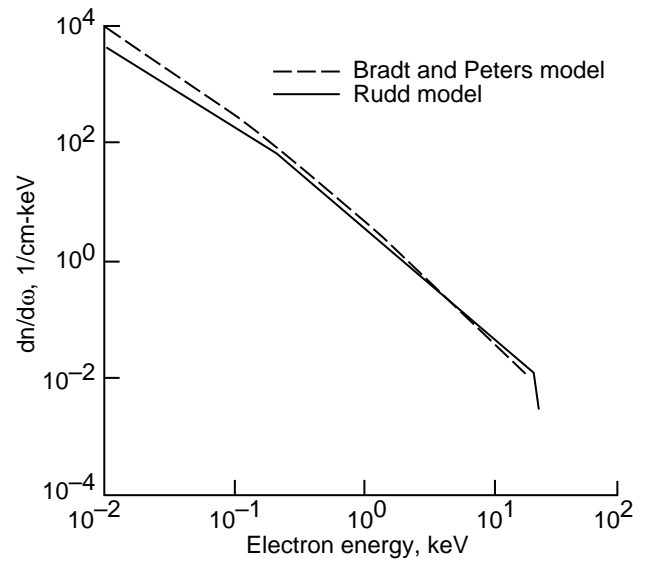
(a) Spectrum with 0.05 MeV proton in water.



(b) Spectrum with 0.1 MeV proton in water.



(c) Spectrum with 1 MeV proton in water.



(d) Spectrum with 10 MeV protons in water.

Figure 1. Secondary electron spectrum from incident protons in water.

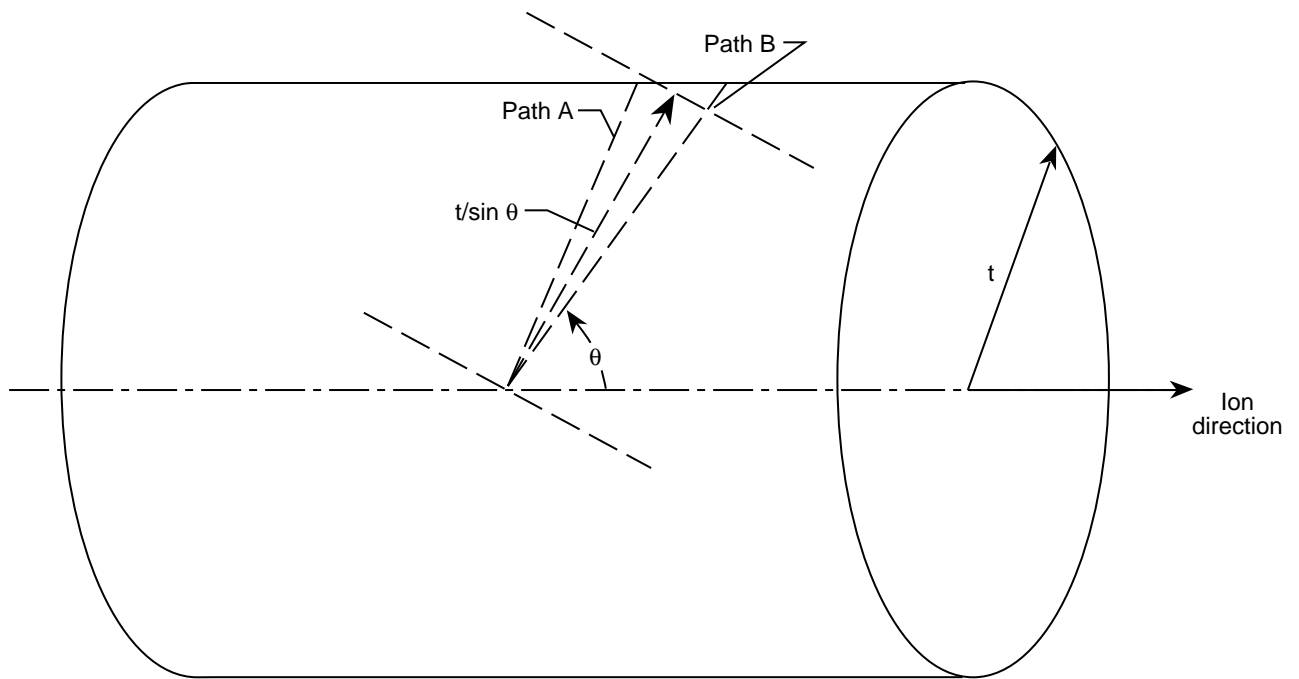
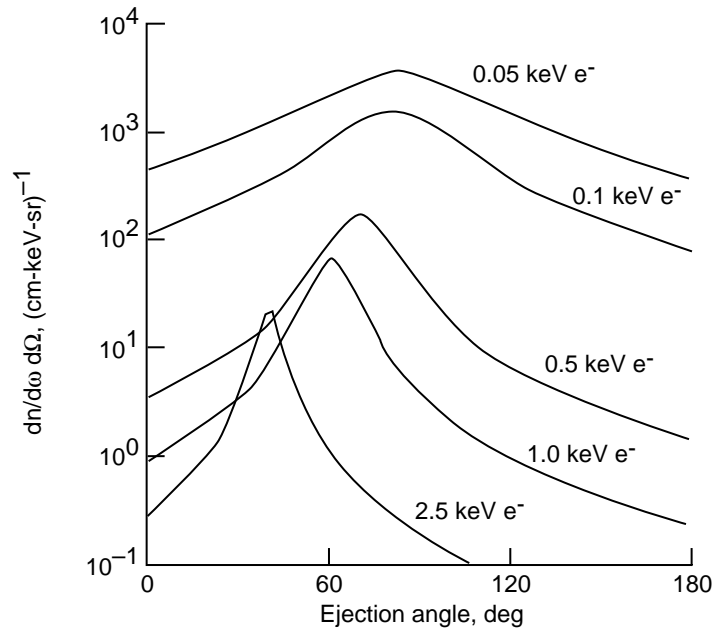
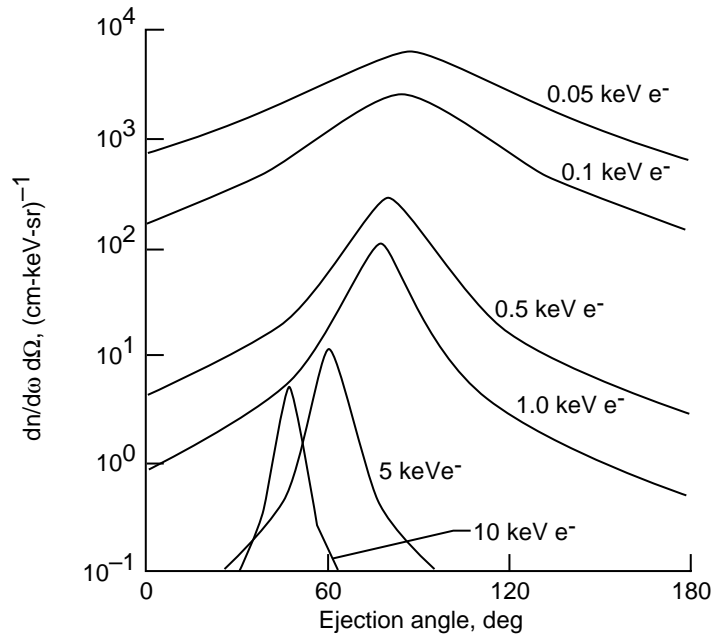


Figure 2. Transmission of electrons ejected at an angle to path of ion through cylindrical surface.



(a) Cross section for 2 MeV protons.



(b) Cross section for 10 MeV protons.

Figure 3. Double differential cross section for electron ejection in water.

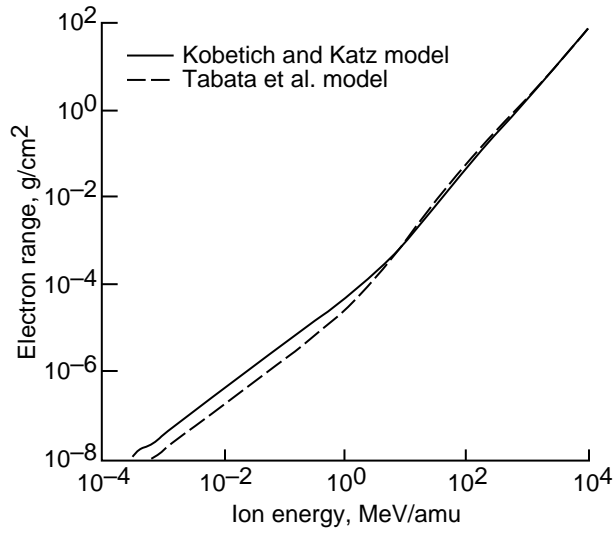


Figure 4. Electron range as function of ion energy in carbon.

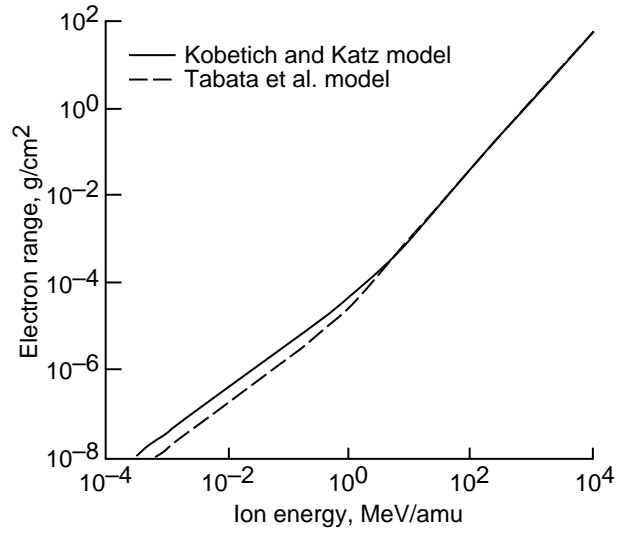


Figure 5. Electron range as function of ion energy in silicon.

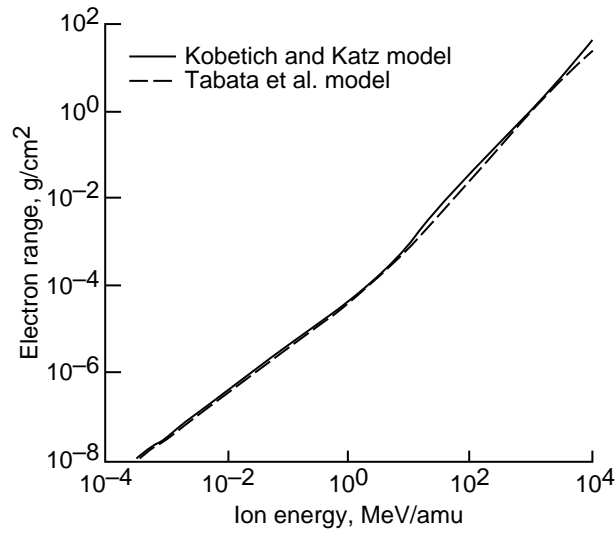


Figure 6. Electron range as function of ion energy in gold.

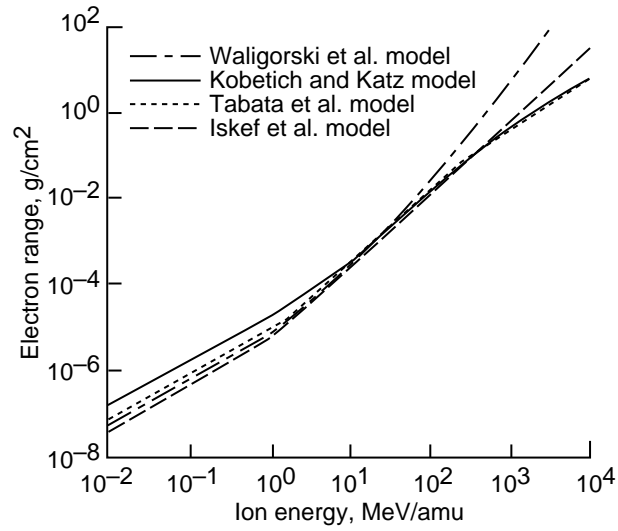


Figure 7. Electron range as function of ion energy in water.

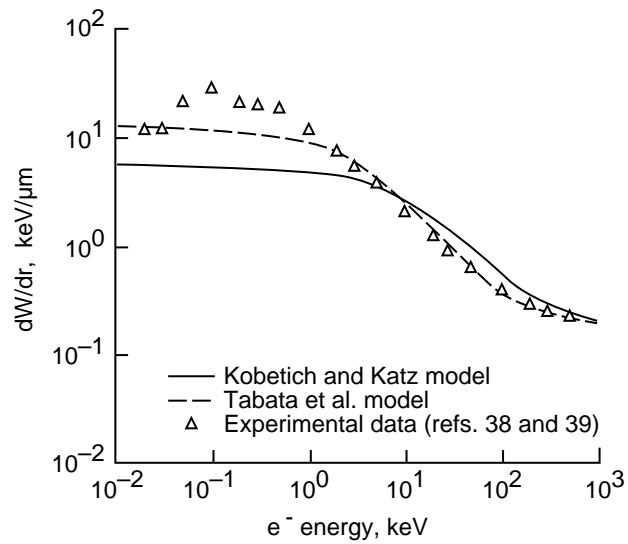
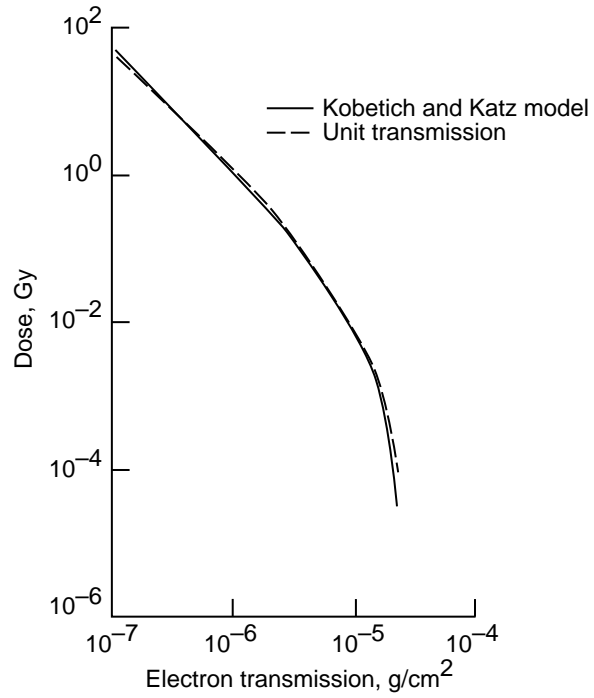
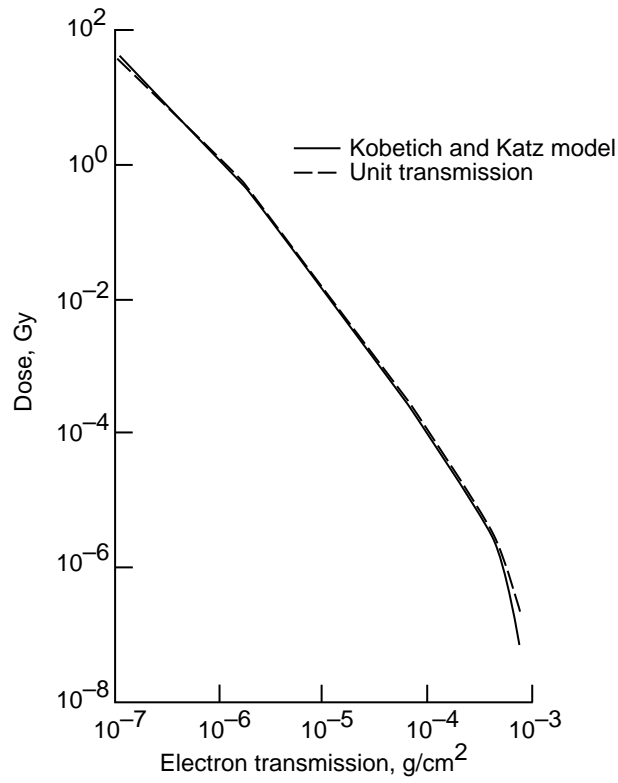


Figure 8. Theoretical and experimental data of dW/dr in water.

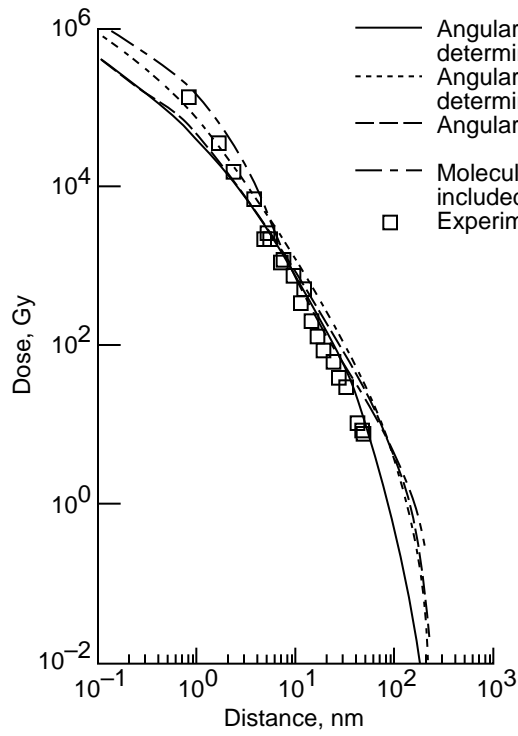


(a) For 1 MeV/amu.

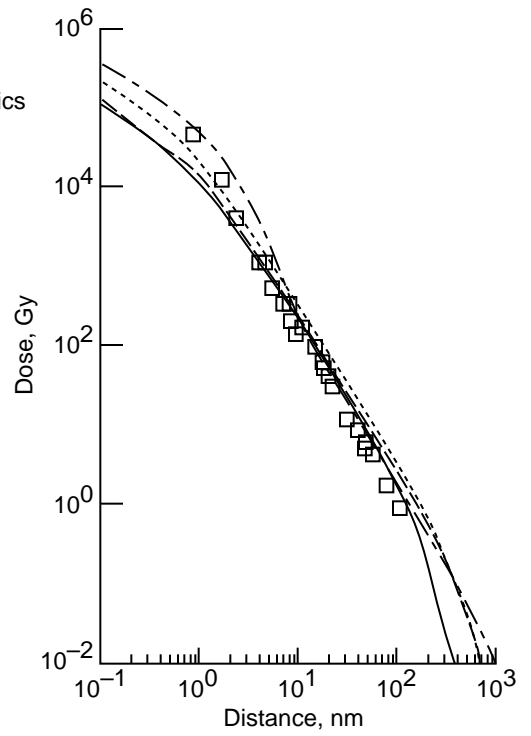


(b) For 10 MeV/amu.

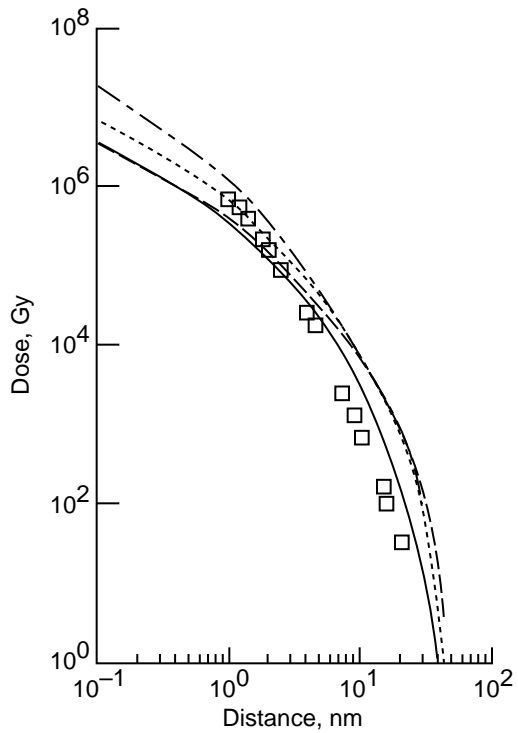
Figure 9. Effects of electron transmission on calculation of radial dose in water.



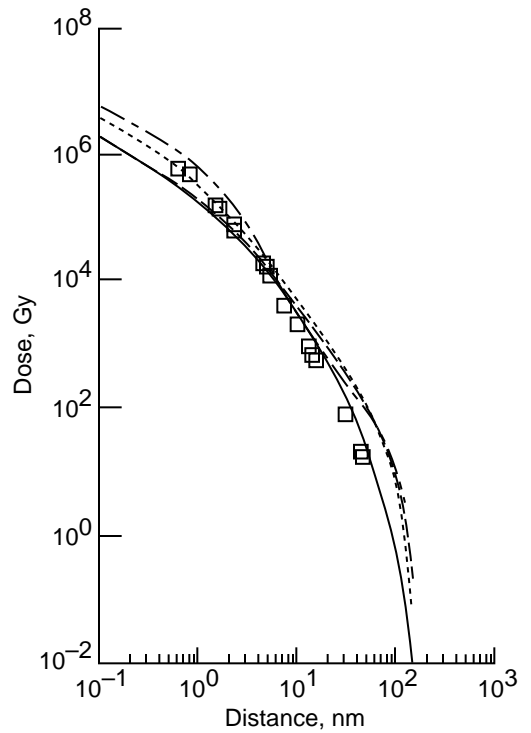
(a) For 1 MeV proton of water.



(b) For 3 MeV protons of water.

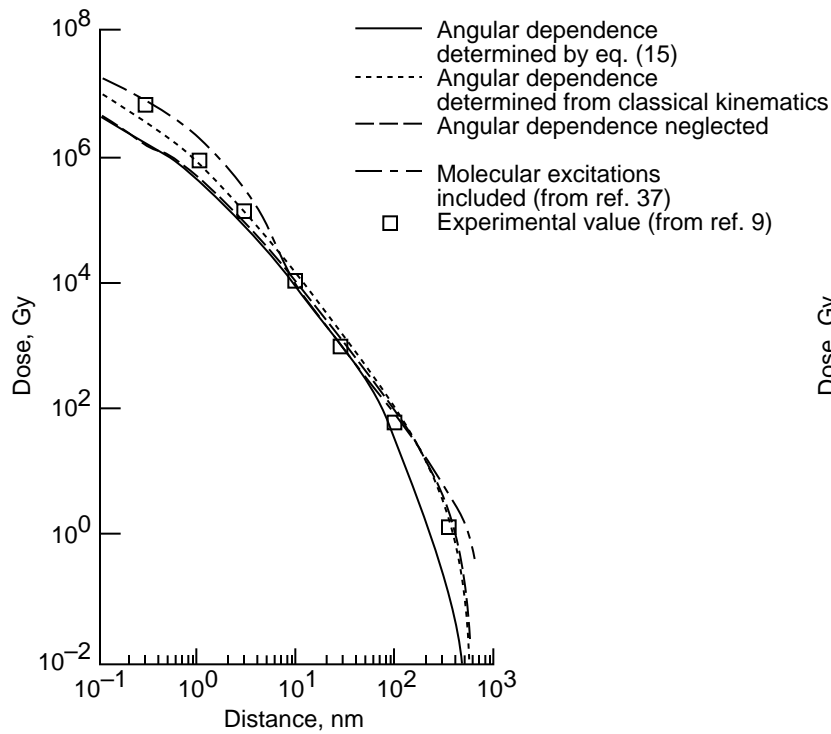


(c) For 0.25 MeV/amu ^4He ion.

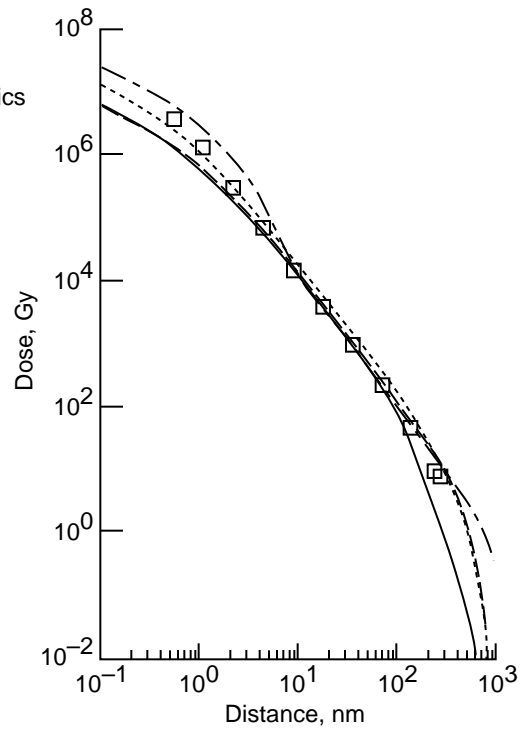


(d) For 0.75 MeV/amu ^4He ion.

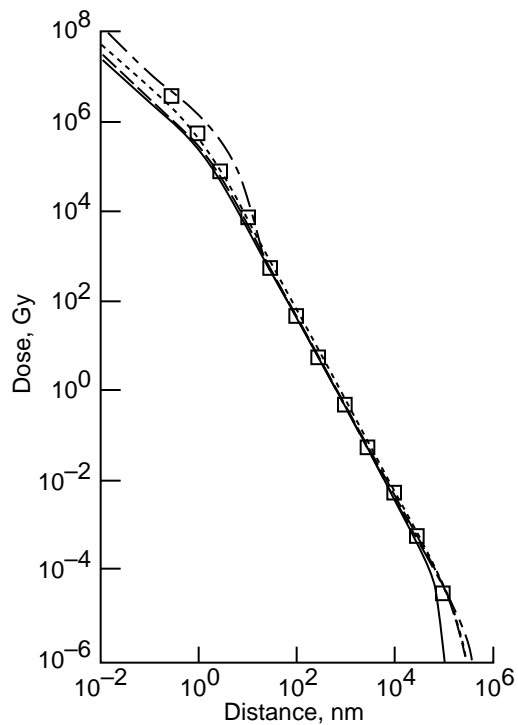
Figure 10. Calculations and experimental data of radial dose.



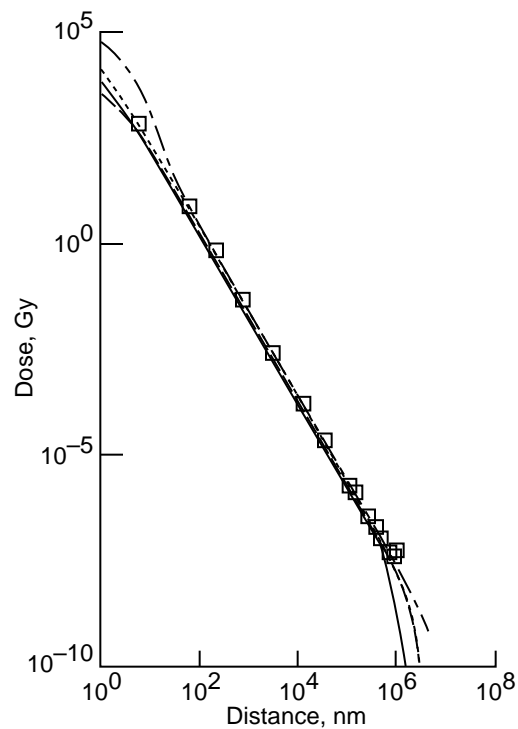
(e) For 2.0 MeV/amu ^{12}C ions.



(f) For 2.57 MeV/amu ^{16}O ions.



(g) For 90 MeV/amu ^{56}Fe ions.



(h) For 377 MeV/amu ^{20}Ne ions.

Figure 10. Concluded.

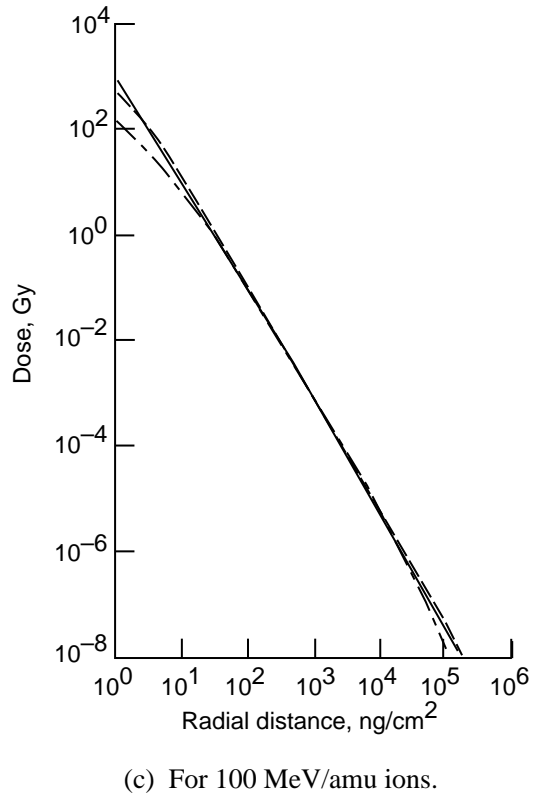
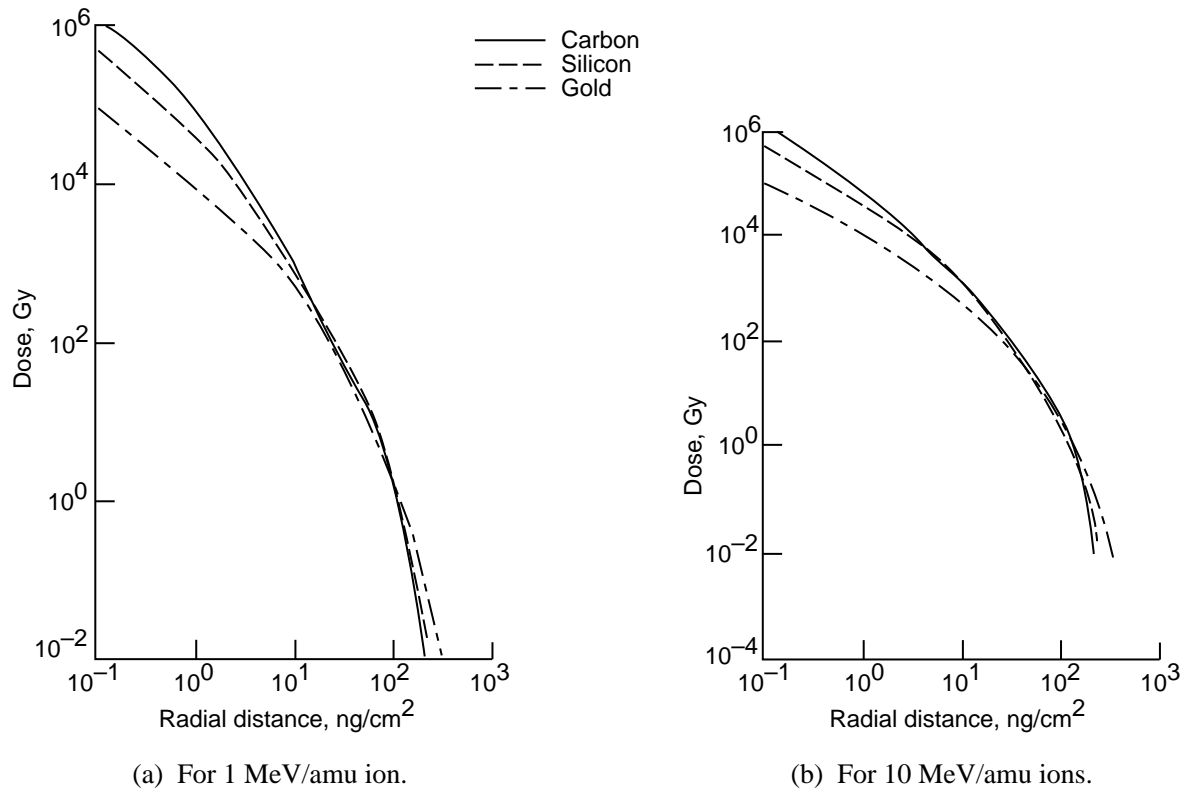


Figure 11. Radial dose in carbon, silicon, and gold.

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