May 1993

Nanostructural effects and interface magnetism in Co/Pd multilayers

Ping He  
*University of Nebraska - Lincoln*

Z.-S. Shan  
*University of Nebraska - Lincoln*

John A. Woollam  
*University of Nebraska-Lincoln, jwoollam1@unl.edu*

David J. Sellmyer  
*University of Nebraska-Lincoln, dsellmyer@unl.edu*

Follow this and additional works at: [http://digitalcommons.unl.edu/physicssellmyer](http://digitalcommons.unl.edu/physicssellmyer)  
Part of the [Physics Commons](http://digitalcommons.unl.edu/physicssellmyer)

[http://digitalcommons.unl.edu/physicssellmyer/110](http://digitalcommons.unl.edu/physicssellmyer/110)

This Article is brought to you for free and open access by the Research Papers in Physics and Astronomy at DigitalCommons@University of Nebraska - Lincoln. It has been accepted for inclusion in David Sellmyer Publications by an authorized administrator of DigitalCommons@University of Nebraska - Lincoln.
Nanostructural effects and interface magnetism in Co/Pd multilayers

Ping He, Z. S. Shan, John A. Woollam, and D. J. Sellmyer
University of Nebraska, Lincoln, Nebraska 68588-0511

A series of Co/Pd multilayers were made by dc magnetron sputter deposition on Al foil substrates. For these multilayered samples, Co layer thicknesses were less than 4 Å and Pd layers were varied from 4 to 22 Å. Sputtering rates were controlled by either sputtering power (10-50 W) or Ar sputtering pressure (3-15 mTorr). In both cases, lower deposition rates yielded higher perpendicular coercivity up to 2.6 kOe. Structures of the samples were studied using conventional θ-2θ x-ray diffractometry (XRD). It has been found that magnetic properties such as coercivity and saturation magnetization are sensitive to interfacial structures. A nanostructural model including interfacial parameters such as alloy layer composition is discussed and compared with the magnetization data. Both XRD and magnetization measurements show that the interfaces become more diffuse at higher sputtering pressures.

I. INTRODUCTION

Multilayered magnetic materials have become an active research area due to the new magnetic properties that are suitable for variety of applications such as magneto-optic (MO) recording. The new properties include large perpendicular anisotropy and high coercivity that often do not exist in single-layer films. For the application to magneto-optic recording media, Co/Pt and Co/Pd have been intensively investigated for several years. These two material systems are being considered for second generation MO recording media.

Because these magneto-optic multilayered systems consist of ultrathin material layers, it is likely that the thickness of interfaces and alloy composition at interfaces play a crucial role in the new magnetic and magneto-optical properties. In this study, we investigated interfacial structures and magnetism, including spin polarization of optical properties. In this study, we investigated interfacial parameters such as alloy layer composition is related to the magneto-optical properties and bilayer thickness to interfacial structures. Therefore, magnetic properties of Co/Pd multilayers can be better understood.

II. EXPERIMENT

Samples were sputter deposited onto water-cooled Al foil substrates under various sputtering conditions. Ar sputtering gas pressure was controlled by a mass flow meter. Multilayered structures were deposited by rotation of the substrates above the guns, and the time when a substrate stopped above either Co or Pd gun was controlled so that a desired amount of material was deposited. A total of 16 multilayer samples was prepared with different layered structures or different deposition conditions. According to different deposition conditions and structures, the multilayered samples can be divided into three groups, and the nominal layered structure and magnetic properties are summarized in Tables I and II.

The layered and crystalline structures of these samples were studied by x-ray diffractometry (XRD). Both small- and large-angle scans were made in the conventional θ-2θ scan mode. Magnetic properties, such as coercivity and magnetization, were measured on an alternating gradient force magnetometer (AGFM). The film composition of samples was determined by measuring the mass of each Co and Pd deposited, and was also verified by energy dispersive spectroscopy (EDS).

III. RESULTS AND DISCUSSIONS

Samples in groups I and II show the magnetic properties as a function of different deposition conditions, such as sputtering power of Pd gun for samples in group I and Ar sputtering pressure for samples in group II. The direct effect of changing sputtering power or sputtering pressure is to change the material deposition rate. All the samples in groups I and II show perpendicular hysteresis loops with squareness near 1, but the coercivity of these samples varies significantly. It can be seen from Fig. 1 that lower deposition rate caused by either lower sputtering power or higher sputtering pressure results in higher coercivity $H_c$ determined from hysteresis loops. Since the deposition rate

![FIG. 1. Coercivity $H_c$ vs deposition rates for samples in groups I and II. The deposition rate was changed by either sputtering power or sputtering pressure. The same deposition rate does not yield the same $H_c$. The inset is a typical perpendicular M-H loop (from sample II-3).](image)
TABLE I. Sputtering power (group I) and sputtering pressure (group II) effects on magnetism and interfaces. Nominal layered structure: Co(2 Å)/Pd(13 Å) \times 35.

<table>
<thead>
<tr>
<th>Group I (Co gun power = 30 W, sputtering pressure = 6 mTorr)</th>
<th>Sample No.</th>
<th>I-1</th>
<th>I-2</th>
<th>I-3</th>
<th>I-4</th>
<th>I-5</th>
</tr>
</thead>
<tbody>
<tr>
<td>Pd gun power (W)</td>
<td>10</td>
<td>20</td>
<td>30</td>
<td>40</td>
<td>50</td>
<td></td>
</tr>
<tr>
<td>( H_x ) (Oe)</td>
<td>1700</td>
<td>1330</td>
<td>1300</td>
<td>1180</td>
<td>1130</td>
<td></td>
</tr>
<tr>
<td>( \sigma_r ) (emu/g)</td>
<td>226</td>
<td>228</td>
<td>224</td>
<td>228</td>
<td>226</td>
<td></td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Group II (Co, Pd gun power = 30 W)</th>
<th>Sample No.</th>
<th>II-1</th>
<th>II-2</th>
<th>II-3</th>
<th>II-4</th>
<th>II-5</th>
</tr>
</thead>
<tbody>
<tr>
<td>Sputter pressure (mTorr)</td>
<td>3</td>
<td>6</td>
<td>9</td>
<td>12</td>
<td>15</td>
<td></td>
</tr>
<tr>
<td>( H_x ) (Oe)</td>
<td>792</td>
<td>1190</td>
<td>1600</td>
<td>2180</td>
<td>2590</td>
<td></td>
</tr>
<tr>
<td>( \sigma_r ) (emu/g)</td>
<td>218</td>
<td>261</td>
<td>206</td>
<td>391</td>
<td>187</td>
<td></td>
</tr>
</tbody>
</table>

changes more significantly with the change of sputtering power rather than sputtering pressure. The sputtering power is the main factor that changes the sputtering yield\(^a\) and deposition rate. However, the change of \( H_x \) due to the change of sputtering power is modest. From the point of view of dynamic molecular theory, one atom on the surface will experience about 300 collisions per second with atoms of the gas when the pressure is about 1 mTorr. Therefore, the chamber ambient during film deposition plays an important role in the deposition process and has significant effects on the film quality. Therefore, the sputtering pressure is the major factor affecting \( H_x \) as shown in Fig. 1.

Small-angle XRD for samples in group I shows qualitatively similar peaks (which are not shown) in the sense that both the peak position and intensity do not vary much. As shown in Table I, the saturation magnetizations \( \sigma_r \) calculated from measured value of \( M-H \) hysteresis loop and Co mass, of samples in group I do not show any significant difference between them, suggesting that interfacial magnetism of these samples is basically the same. However, the intensity of the (111) peaks and small-angle peaks from samples in group II shows systematic changes with sputtering pressure, as shown in Fig. 2. Higher-order small-angle peaks and other large-angle peaks are not observed for samples in group II. It can be seen that when the sputtering pressure is greater than 9 mTorr, the small-angle peak disappears, indicating more diffuse interfaces or lack of well-defined layer boundaries, which may be caused by the frequent collisions between surface atoms and ambient gas atoms. The saturation magnetization \( \sigma_r \) of samples in group II exhibits a systematic decrease with an increase of sputtering pressure, as well. Since, as revealed by small-angle XRD of these samples, the higher the sputtering pressure, the more diffuse the interfaces, the decrease of \( \sigma_r \) may be caused by either the decrease of induced magnetic moments on Pd atoms, or the reduction of Curie temperature. As Shan et al. pointed out,\(^b\) the induced moments on Pd are a function of the number of nearest Co neighbors around Pd atoms. The fewer the Co neighbors around Pd atoms, the less the induced moments on Pd atoms. It should be noticed that more Pd atoms will be polarized because more Pd atoms are mixed with Co atoms due to the interdiffusion, which will increase the magnetization of the film. These two results have opposite effects on the overall magnetization \( \sigma_r \). The results listed in Tables I and II show that the decrease of induced moments on Pd is dominant. The other explanation of the decrease of induced moments is that when the interfaces are more diffuse, the Curie temperature \( T_c \) will decrease which can cause the decrease in magnetization. According to Co-Pd thermal equilibrium phase diagram, \( T_c \) is about room temperature at 90 at. % Pd.

The magnetization \( \sigma_r \) of samples in group III is shown in Fig. 3. It can be seen that the initial increase of \( \sigma_r \) is due to the induced moment on Pd atoms which are surrounded

---

**TABLE II. Pd layer thickness effect on interface magnetism. Co layer thickness of 2 Å was fixed. Bilayer thickness was determined by small-angle XRD, and film composition by EDS.**

<table>
<thead>
<tr>
<th>Group III (nominal structure: Co(2 Å)/Pd(xÅ) \times 35)</th>
<th>Sample No.</th>
<th>III-1</th>
<th>III-2</th>
<th>III-3</th>
<th>III-4</th>
<th>III-5</th>
<th>III-6</th>
</tr>
</thead>
<tbody>
<tr>
<td>( x ) (Å)</td>
<td>4.0</td>
<td>7.0</td>
<td>10.0</td>
<td>13.0</td>
<td>16.0</td>
<td>22.0</td>
<td></td>
</tr>
<tr>
<td>( H_x ) (Oe)</td>
<td>744.0°</td>
<td>817.0°</td>
<td>1040.0</td>
<td>1190.0</td>
<td>1210.0</td>
<td>1010.0</td>
<td></td>
</tr>
<tr>
<td>( \sigma_r ) (emu/g)</td>
<td>202.0</td>
<td>229.0</td>
<td>249.0</td>
<td>246.0</td>
<td>245.0</td>
<td>249.0</td>
<td></td>
</tr>
<tr>
<td>Bilayer thick. (Å)</td>
<td>6.5</td>
<td>10.1</td>
<td>13.1</td>
<td>15.5</td>
<td>18.9</td>
<td>24.9</td>
<td></td>
</tr>
<tr>
<td>Film comp.(^c) (Co)</td>
<td>0.37</td>
<td>0.24</td>
<td>0.18</td>
<td>0.15</td>
<td>0.13</td>
<td>0.10</td>
<td></td>
</tr>
</tbody>
</table>

\(^a\)Squareness is less than 0.9.
\(^b\)The film composition is in atomic percent of Co.

\(5955 \quad J. \text{Appl. Phys., Vol. 73, No. 10, 15 May 1993} \quad \text{He et al.} \quad 5955\)
FIG. 3. Saturation magnetization $\sigma$, as function of Pd layer thickness for samples of group III. $\sigma$, is calculated using Co mass only. The major source of the error bars is from the measurement of Co mass in the multilayered films.

or partially surrounded by Co atoms. The shape of the curve in Fig. 3, in general, agrees with data obtained by others. One difference found in this study is that $\sigma$, (Fig. 3) stays roughly constant after $\sigma$, reaches a maximum at a Pd layer thickness of ~10 Å, indicating that Pd atoms added after the Pd layer is greater than 10 Å make no contribution to the magnetization, and thus these Pd atoms are not mixed with Co, as is reasonable. Therefore, if it is assumed that Co atoms diffuse in both directions into adjacent Pd layers, the interface thickness will be about 10 Å. The interdiffusion length is then estimated to be about 5 Å.

More information about Co-Pd interfaces may be obtained when magnetic, XRD, and EDS measurements are combined. A microstructural model$^{11}$ can be used to estimate the average composition of Co at interfaces or in the CoPd alloy layers. This model can be expressed as the following:

$$L = L_0 \left(1 - \frac{n_a}{n_b}\right) + \frac{n_a}{n_b} L_a \frac{x_Co^a}{x_Co^b},$$

where $L$ is the bilayer thickness which can be measured by small-angle XRD, $L_a$ the alloy layer (interface) thickness, $n_a$ and $n_b$ the atomic number densities of the alloy layers and pure Pd layers, and $x_Co^a$ and $x_Co^b$ (determined by EDS or other methods) the Co compositions in the alloy layers and in the film, respectively.

The bilayer thickness and over all Co composition of these samples in group III can be easily and accurately determined and are listed in Table II. The plot of $L$ vs $1/x_{Co}$ shows a straight line in Fig. 4. From the slope ($=2.45$ Å), intercept ($=-0.314$ Å), and alloy layer thickness ($=2 \times$ interdiffusion length $=10-12$ Å) which is estimated above, the average Co composition at the interfaces is found to be about 20–25 at. %.