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Global Analysis of Saturation Artifacts in the VIIRS Infrared Channels and the Effects of Sample Aggregation

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First Global Analysis of Saturation Artifacts in the VIIRS Infrared Channels and the Effects of Sample Aggregation

Thomas N. Polivka, Edward J. Hyer, Jun Wang, and David A. Peterson

Abstract—Unlike previous spaceborne Earth observing sensors, the Visible Infrared Imaging Radiometer Suite (VIIRS) employs onboard sample aggregation to reduce downlink bandwidth requirements and preserve spatial resolution across the scan. To examine the potentially deleterious impacts of onboard sample aggregation when encountering detector saturation, nearly four months of the National Oceanic and Atmospheric Administration’s Nightfire product are analyzed, which contains a subset of the hottest observed nighttime pixels. An empirical method for identifying saturation is devised. The M12 band (3.69 μm) is the most frequently saturating band with 0.15% of the Nightfire pixels at or near the ～359-K detector saturation limit; some saturation is also found in M14, M15, and M16 (8.58, 10.74, and 11.86 μm). Artifacts consistent with detector saturation are seen with M12 temperatures as low as 330 K in the scene center. This partial saturation and aggregation influence must be considered when using VIIRS radiances for quantitative characterization of hot emission sources such as fires and gas flaring.

Index Terms—Fires, infrared measurements, nightfire, remote sensing, sample aggregation, saturation, Suomi National Polar-Orbiting Partnership (S-NPP), Visible Infrared Imaging Radiometer Suite (VIIRS).

I. INTRODUCTION

On October 28, 2011, the Suomi National Polar-Orbiting Partnership (S-NPP) satellite was launched from the Vandenberg Air Force Base in California, and it now orbits with a mean altitude of 840 km above the Earth in sun-synchronous orbit. Located aboard S-NPP, the Visible Infrared Imaging Radiometer Suite (VIIRS) is a 22-band scanning radiometer with a nominal spatial resolution of 375 m in the five imagery bands (I-bands) and 750 m in both the 16 moderate-resolution bands (M-bands) and the day–night band (DNB) [1]–[4] (see Table I). The sensor data records (SDRs) of calibrated radiances and brightness temperatures cover a spectral range from 0.411 to 11.87 μm and are used in a wide range of Earth observation applications, including fire detection and characterization, retrieval of cloud and aerosol properties, and land and sea surface temperature estimation [5]. The VIIRS sensor was designed to improve upon legacy instruments, such as the Moderate Resolution Imaging Spectroradiometer (MODIS), the Advanced Very High Resolution Radiometer, and the Operational Line Scanner. One significant enhancement relative to these legacy sensors is that VIIRS does not experience the significant off-nadir pixel growth affecting sensors such as MODIS; VIIRS pixels at the scan edge are only two to four times the size of nadir pixels, whereas MODIS exhibits a growth factor of 10 [2]. For the M-bands, VIIRS delivers SDRs of calibrated radiances and brightness temperatures with a pixel instantaneous field of view (IFOV) of 0.75 × 0.79 km at nadir, which increases to 1.66 × 1.71 km at the edge of the scan [1], whereas the five imagery bands have smaller IFOVs ranging from 0.38 × 0.39 km to 0.83 × 0.86 km at the scan edge.

The spatial resolution of VIIRS is preserved across the scan by employing asymmetrical detectors in conjunction with a unique sample aggregation scheme, as illustrated in Fig. 1, which combines multiple samples from one rectangular detector into single raw data record (RDR) pixels consisting of digital counts. This processing is done onboard the satellite, except for the dual-gain bands whose aggregation is done on the ground [2]. As a result, the RDR has three aggregation zones. The 3:1 aggregation zone refers to scan angles between 0° (nadir) and 31.72°, where the value of each pixel is actually the average of three individual samples. Similarly, in the 2:1 aggregation zone (scanning angles between 31.72° and 44.86°), two samples from the same detector are aggregated to form a pixel. No sample aggregation is performed in the

### Table I

<table>
<thead>
<tr>
<th>Launch date</th>
<th>28 October, 2011</th>
</tr>
</thead>
<tbody>
<tr>
<td>Orbit description</td>
<td>Near-circular, near-polar, sun-synchronous</td>
</tr>
<tr>
<td>Mean orbital altitude</td>
<td>840 km</td>
</tr>
<tr>
<td>Inclination</td>
<td>98.7°</td>
</tr>
<tr>
<td>Orbital period</td>
<td>101.5 min.</td>
</tr>
<tr>
<td>Ascending equator local crossing time</td>
<td>13:30 ± 10 min.</td>
</tr>
<tr>
<td>Swath width</td>
<td>~3000 km</td>
</tr>
<tr>
<td>Number of bands</td>
<td>5 I-bands, 16 M-bands, 1 DNB</td>
</tr>
<tr>
<td>Nominal spatial resolution</td>
<td>375 m (I-bands), 750 m (M-bands, DNB)</td>
</tr>
<tr>
<td>Spectral range</td>
<td>0.411–11.87 μm</td>
</tr>
<tr>
<td>Detectors per band</td>
<td>32 (I-bands), 16 (M-bands), 672 (DNB)</td>
</tr>
<tr>
<td>Lines per scan</td>
<td>32 (I-bands), 16 (M-bands), DNB</td>
</tr>
</tbody>
</table>
1:1 aggregation zone (scan angles greater than 44.86°); thus, each pixel is calculated from a single detector sample. Once the RDR has been generated, it is later processed into a calibrated SDR, retaining the characteristics from aggregation.

While the VIIRS aggregation scheme effectively reduces pixel footprint growth across the scan, it also results in fundamental differences in the data characteristics among the three aggregation zones, particularly when detector saturation occurs. The VIIRS onboard electronics module does not flag the data if an individual sample saturates before aggregation occurs. Consequently, the aggregation of samples does not account for saturation effects, which may result in biases or artifacts for pixels containing active biomass burning or other heat sources that have the potential to cause detector saturation. In the case when an individual sample is saturated and then aggregated with unsaturated samples, the resulting pixel will have a radiation bias associated with saturation, even if the reported pixel radiance is well below the detector saturation limit. This study investigates the frequency and effects of saturated samples in the VIIRS infrared (IR) channels and evaluates the potential for biases and artifacts in the VIIRS SDR caused by onboard sample aggregation. This study represents a first attempt to derive an empirical method for identifying possible partial saturation and determine thresholds to filter partially or fully saturated pixels in bands that are relevant to the detection and characterization of hot targets.

II. DATA SET DESCRIPTION

In order to facilitate the analysis of saturation potential in VIIRS data, a NOAA Joint Polar Satellite System Proving Ground product named “Nightfire” is used in this study [6]. Nightfire is utilized because it contains an extensive set of prescreened “hot” pixels, allowing for fast analysis of months of data. The Nightfire algorithm selects thermally anomalous pixels detected in the VIIRS shortwave infrared (SWIR) 1.6-μm band (M10) [6], rather than utilize the 4-μm range that is traditionally used for fire detection [7]. VIIRS is unusual in that it records some near-infrared (NIR) and SWIR data during nighttime (bands M7, M8, and M10 in Table II), which allows for easy and rigorous detection of hot sources due to the lack of background (solar) radiation. The nighttime background radiance at 1.6 μm is very low, generally of the same order of magnitude as dark current noise in the sensor. M10 is therefore selected as the primary band of Nightfire to detect thermally radiant objects, particularly gas flares with burning temperatures up to 1800 K [6]. During nighttime, pixels more radiant than the background digital count (DC) plus four standard deviations of DC are first flagged as thermally anomalous candidate pixels. The background DC is the mean DC of all nonhot pixels (DC value ≤ 100) contained in each aggregation zone for one VIIRS granule, and the standard deviation is calculated using the same criteria. To filter the noise in M10 caused by high-energy particles that frequently hit the sensor within the South Atlantic Anomaly (SAA) [3], [8] and auroral areas, the Nightfire algorithm conducts a second check on the hot pixel detected by M10 with other NIR/SWIR bands (M7 and M8) using the same technique as for M10. Finally, the algorithm attempts to fit a Planck curve to the retrieved radiances to obtain the temperature and area of the emitting source using the simplex optimization method [9]. A more thorough discussion of the Nightfire algorithm can be viewed in [6].

While Nightfire provides atmospheric-corrected data, only the uncorrected calibrated radiances for the eight M-bands (see Table II) for each pixel are examined in this study. Atmospherically-corrected data and retrieved hot spot properties are not investigated. Statistical examination of the Nightfire data (see Table II) indicates a discontinuity between data before and after March 17, 2013. Therefore, the earlier data are excluded, leaving Nightfire data from March 18, 2013 to July 14, 2013 available for use in this study. After screening out records with missing data (less than 0.01% of the data), this time period yields 1 861 865 thermally anomalous pixels. The geographic distribution of the filtered Nightfire data is shown in Fig. 2, highlighting regions of frequent biomass burning (Central Africa, Central America, Southeast Asia), as well as regions that commonly flare gas, such as the Persian Gulf, North Dakota, and Nigeria.

III. ANALYSIS AND RESULTS

The analysis is divided into three parts. First, the nine M-bands from Table II are scrutinized by constructing

![Image](https://via.placeholder.com/150)

**Table II**

<table>
<thead>
<tr>
<th>Band</th>
<th>Spectral Range (μm)</th>
<th>Central λ (μm)</th>
<th>Specification Max1</th>
<th>Obs. Max1</th>
<th>Above Spec. Fraction1 (%)</th>
<th>Obs. Fraction2 (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>M7</td>
<td>0.843 – 0.881</td>
<td>0.86</td>
<td>349</td>
<td>24.2</td>
<td>0</td>
<td>N/A</td>
</tr>
<tr>
<td>M8</td>
<td>1.225 – 1.252</td>
<td>1.24</td>
<td>165</td>
<td>80.3</td>
<td>0</td>
<td>N/A</td>
</tr>
<tr>
<td>M10</td>
<td>1.571 – 1.629</td>
<td>1.60</td>
<td>71.2</td>
<td>75.0</td>
<td>0</td>
<td>N/A</td>
</tr>
<tr>
<td>M12</td>
<td>3.598 – 3.791</td>
<td>3.69</td>
<td>353</td>
<td>359</td>
<td>0.22</td>
<td>0.15</td>
</tr>
<tr>
<td>M13</td>
<td>3.987 – 4.145</td>
<td>4.06</td>
<td>634</td>
<td>533</td>
<td>0</td>
<td>N/A</td>
</tr>
<tr>
<td>M14</td>
<td>8.407 – 8.748</td>
<td>8.58</td>
<td>336</td>
<td>349</td>
<td>0.002</td>
<td>0.0005</td>
</tr>
<tr>
<td>M15</td>
<td>10.254 – 11.248</td>
<td>10.74</td>
<td>345</td>
<td>359</td>
<td>0.001</td>
<td>0.0003</td>
</tr>
<tr>
<td>M16</td>
<td>11.405 – 12.322</td>
<td>11.86</td>
<td>340</td>
<td>356</td>
<td>0.001</td>
<td>0.0003</td>
</tr>
</tbody>
</table>

1Unit is W/m² sr-μm for M7, M8, M10; K for M12-M16; W/cm² sr for the DNB.
2Percentage of pixels above 99.9% of the design specification maximum from [1].
3Percentage of pixels above 99.9% of the observed maximum.
4Primary VIIRS fire detection band.
5The DNB has a very broad spectral range [10] and was not analyzed for saturation.
histograms to identify which bands are fully saturating. Full saturation would be manifested by sudden or unexpected peaks in frequency at the highest radiance bin. Second, the most frequently saturating band’s data are separated by aggregation mode to determine if there is a relationship with sample saturation and aggregation scheme. In this case, scatterplots of the data between saturating and nonsaturating bands are constructed to look for distinct populations of pixels unique to each mode. The third and final step of the analysis attempts to verify the relationship between sample saturation and aggregation by statistically simulating the effects of partial saturation. This is accomplished by using the properties of the unaggregated data (from the 1:1 aggregation zone) to generate synthetic populations of detector data that can be aggregated to match the VIIRS sample aggregation scheme and comparing the resulting histograms of the synthetic data with the observed distributions of each aggregation mode.

A. Band-by-Band Detection of Saturation

From the radiance histograms of each band (see Fig. 3), significant saturation is observed in the 3.69-μm (M12) band, which is highlighted by the sudden density peak at 3.39 W/m² · sr · μm, representing 0.15% of the data (red arrow). The approximate radiances corresponding to the theoretical limits described by [1] are indicated by the vertical dashed red lines in Fig. 3. The maximum observed radiance is slightly higher than the theoretical maximum; 3.39 W/m² · sr · μm has a corresponding brightness temperature of \( \sim 359 \) K at the center wavelength of 3.69 μm in comparison with the 353-K brightness temperature limit reported by [1]. The incidence of partial pixel saturation as a possible side effect of aggregation is noted near 1.3, 1.8, and 2.3 W/m² · sr · μm, which can be seen by the slight and smoothed peaks near those radiance values. Fig. 4 shows the global distribution of fully saturated (3.39 W/m² · sr · μm) M12 pixels aggregated to a 1° × 1° grid; many of the same regions with hot spots in Fig. 2 are visible, but the SAA is notably absent.

Clustering of values near the maximum observed bins from Fig. 3 gives qualitative evidence of possible saturation in the M14, M15, and M16 bands (marked by the blue arrows). However, for bands other than M12, the percentage of pixels that lie above 99.9% of the nominal saturation levels and observed maximum values is very low (e.g., less than 0.002%, Table II, right columns), suggesting that saturation effects in nocturnal scenes are very rare in these bands. Bands M10 and M13 do not experience saturation in this data set.

B. M12 Saturation Aggregation Zone Dependence

In order to determine the effects of sample saturation in the M12 band, the data are segregated according to aggregation zone. Scatterplots of 3.69 μm/4.06 μm (M12/M13) ratio versus 4.06 μm (M13) for each aggregation zone are shown in Fig. 5. The ratio of M12/M13 is used for comparison since M13 does not saturate and lies in close spectral proximity to M12. The three panels illustrate the 1:1, 2:1, and 3:1 aggregation zones, respectively. The 1:1 pixels [see the green dots in Fig. 5 (left)] show the baseline pattern for M12, where the ratio of M12/M13 varies up to the detector saturation point of 3.39 W/m² · sr · μm.
For M13 radiances above this limit, M12/M13 is truncated, indicating that M12 is saturating while M13 is not (labeled 1 in Fig. 5 [left]). The variability of M12/M13 at low M13 radiances shows a spread of ratios due to different thermal properties, owing to the atmospheric effects and the Planck function’s sensitivity to temperature for differing wavelengths. Despite this, as the M13 radiance increases, the M12/M13 ratio converges to a curve determined by the M12 saturation limit.

The 2:1 aggregation zone [see Fig. 5 (center)] shows a similar pattern with one important and noticeable difference. As the M13 radiance increases, the M12/M13 ratio converges to two clusters with a spread of points between them. The lower cluster (labeled 1) reflects the case when one sample saturates while the other aggregated sample does not. As the ratio increases for the same M13 radiance value, there is still one saturated M12 sample, but the neighboring aggregated M12 sample is reporting increased radiances until both samples saturate (labeled 2). That is visible as the detector saturation limit of the M12/M13 ratio with the same M12 radiance of 3.39 W/m² · sr · μm.

Finally, in the case of the 3:1 aggregation scheme [see Fig. 5 (right)], there are three populations of curves, owing to the three samples that are averaged together. The lowest cluster represents the case when one of the aggregated M12 samples saturates (labeled 1) but the two other samples do not. The middle ratio population for a given M13 radiance is for a situation where two samples saturate but the third does not (labeled 2). Finally, the uppermost population is where all three aggregated M12 samples saturate (labeled 3).

C. Diagnosing and Verifying New Saturation Thresholds

To confirm that these features are consistent with aggregation effects, a statistical method was devised to simulate the observed distribution of radiances in each aggregation zone. Thirty million values are randomly drawn from the observed M12 1:1 aggregation zone. The 2:1 aggregation zone is simulated by drawing 15 million random pairs from the 1:1 aggregation zone and averaging each pair, whereas the 3:1 aggregation zone is simulated by drawing 10 million triplets from the 1:1 aggregation zone and averaging them. The results of these simulations are displayed in Fig. 6, which is divided into nine panels. In each panel, the colored bars show the observed distribution from the Nightfire data, and the black lines show the statistically created distributions. The three rows represent the aggregation zones starting with 1:1 at the top and ending with 3:1 at the bottom, whereas the three columns are M12 radiance, M13 radiance, and M12/M13 ratios, from left to right. Solid bars represent the observed distributions of radiances, and the black outlines represent the synthetic distributions made by averaging samples drawn from the edge scan data set (see Section III-C for details).

Saturation can be seen to affect radiances as low as 1.7 W/m² · sr · μm (~337 K at 3.69 μm) for the 2:1 aggregation zone [see Fig. 6(d)]. In the 3:1 aggregation zone, the influence of an individual saturated sample becomes apparent at radiances of only 1.3 W/m² · sr · μm (~330 K). The second column shows the observed and synthetic distributions for the M13 (4.06 μm) band, where no unusual peaks in density are noted. The far right column shows suppression of high values of M12/M13 with aggregation, consistent with the effects of averaging. The geographic distribution of potential partially saturated pixels is displayed in Fig. 7, where data are mapped only if the radiance values reach above the thresholds of possible partial saturation (1.3 W/m² · sr · μm for 3:1 aggregation, 1.7 W/m² · sr · μm for 2:1 aggregation, and 3.39 W/m² · sr · μm for 1:1 aggregation). In comparison with the observed detector saturation limit (see Fig. 4), a much larger area is impacted by partial saturation.

While the general pattern of the observed and simulated distributions is similar, particularly the features caused by detector saturation, large discrepancies exist. One main difference stems from sample correlation. Normally, when VIIRS scans a scene, adjacent samples will observe a similar environment;
that is, if one sample scans a fire, the chances are high that the adjacent samples(s) will also scan hot terrain. This greatly increases the frequency of high temperatures occurring in the observations compared with randomly selected samples. Another compounding factor is the difference in IFOV, which is dependent on scan angle. While the pixel footprint change is reduced by aggregation, detector footprint sizes for VIIRS still increase significantly with scan angle. Thus, the detector IFOV near nadir is much smaller than at the scan edge, which leads to higher fire fractions and, subsequently, increased occurrence of very high radiances in the near-nadir samples when compared with the 1:1 aggregation zone samples. These two effects have increases the frequency of high temperatures occurring in the observations compared with randomly selected samples. Another compounding factor is the difference in IFOV, which is dependent on scan angle. While the pixel footprint change is reduced by aggregation, detector footprint sizes for VIIRS still increase significantly with scan angle. Thus, the detector IFOV near nadir is much smaller than at the scan edge, which leads to higher fire fractions and, subsequently, increased occurrence of very high radiances in the near-nadir samples when compared with the 1:1 aggregation zone samples. These two effects have similar impacts on the observed distribution; therefore, they cannot be easily separated for analysis or considered in the simulated distributions. This demonstrates that extrapolation from the 1:1 zone tends to underestimate the occurrence of saturation in the 2:1 and 3:1 aggregation regimes.

IV. SUMMARY AND CONCLUSION

This letter investigated the prevalence and influence of detector saturation when the VIIRS sample aggregation scheme is applied. It should be noted that saturation may occur more frequently than the Nightfire data set indicates because fires tend to burn hotter in the daytime than at night. The only band to suffer from significant deleterious detector saturation is the 3.69-μm band (M12), but there is some evidence to support saturation in the other single-gain thermal infrared (TIR) channels that might be more apparent in a larger data set. The maximum radiance values recorded by VIIRS in those bands are significantly higher than the pub lished maxima in [1]. For the M12 band, distinct clustering of pixel radiances below the detector saturation limit of 3.39 W/m²·sr·μm (≈359 K) appears in the data from the 2:1 and 3:1 aggregation zones. The 1:1 aggregation zone’s saturation limit is thus 3.39 W/m²·sr·μm (≈359 K), whereas the 2:1 aggregation zone exhibits saturation at 1.7 W/m²·sr·μm (≈337 K), and the 3:1 aggregation zone is susceptible to saturation only at 1.3 W/m²·sr·μm (≈330 K).

VIIRS does not record when saturation occurs in individual samples. Therefore, it is impossible to know if a pixel is affected by saturation in the M12 band beyond its respective saturation threshold. The potential for biases in pixel radiance due to unidentified saturation is a significant problem for quantitative use of the M12 band for applications that use hot pixels, such as for multispetsral fire property retrievals. M12’s intended use for sea surface temperature derivation [1], [11] should not be impacted, provided pixels are filtered to avoid hot sources such as gas flaring. For applications that require quantitative evaluation of hot sources, the aggregation scheme determines the upper limit of radiances known to be unsaturated.

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REFERENCES