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Surface complexation modeling for predicting solid phase arsenic concentrations in the sediments of the Mississippi River Valley alluvial aquifer, Arkansas, USA

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ABSTRACT

The potential health impact of As in drinking water supply systems in the Mississippi River Valley alluvial aquifer in the state of Arkansas, USA is significant. In this context it is important to understand the occurrence, distribution and mobilization of As in the Mississippi River Valley alluvial aquifer. Application of surface complexation models (SCMs) to predict the sorption behavior of As and hydrous Fe oxides (HFO) in the laboratory has increased in the last decade. However, the application of SCMs to predict the sorption of As in natural sediments has not often been reported, and such applications are greatly constrained by the lack of site-specific model parameters. Attempts have been made to use SCMs considering a component additivity (CA) approach which accounts for relative abundances of pure phases in natural sediments, followed by the addition of SCM parameters individually for each phase. Although few reliable and internally consistent sorption databases related to HFO exist, the use of SCMs using laboratory-derived sorption databases to predict the mobility of As in natural sediments has increased. This study is an attempt to evaluate the ability of the SCMs using the geochemical code PHREEQC to predict solid phase As in the sediments of the Mississippi River Valley alluvial aquifer in Arkansas. The SCM option of the double-layer model (DLM) was simulated using ferrihydrite and goethite as sorbents quantified from chemical extractions, calculated surface-site densities, published surface properties, and published laboratory-derived sorption constants for the sorbents. The model results are satisfactory for shallow wells (10.6 m below ground surface), where the redox condition is relatively oxidic or mildly sub-oxidic. However, for the deep alluvial aquifer (21–36.6 m below ground surface) where the redox condition is suboxidic to anoxic, the model results are unsatisfactory.

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1. Introduction

The movement and transport of As in groundwater can be significantly slowed or enhanced by chemical or biogeochemical reactions occurring at mineral–water interfaces. In general, physico-chemical processes such as precipitation and dissolution, surface complexation, and ion exchange determine the interaction of As with solid sorbent surfaces (Figueira da Silva, 2005). The most common and dominant As attenuation reaction is surface complexation with hydrous metal oxides (Sracek et al., 2004; Langmuir, 1997; Korte and Fernando, 1991; Shevenell et al., 1999). In theory, surface complexation models (SCMs) are based on fundamental chemical and physical principles that are controlled by measurable parameters such as specific surface area, surface-site density, elec-

trical and chemical potentials of the surfaces, and intrinsic surface constants associated with reactive surface sites and adsorbate ions, etc. (Figueira da Silva, 2005; Zachara and Westall, 1999; Miller, 2000; Dzombak and Morel, 1990; Davis et al., 2004). Fundamental sorption reactions that take place at metal oxide surfaces are fully describable using surface complexation theory (Dzombak and Morel, 1990; Hemond, 1995; Goldberg, 1998; Koretsky, 2000; Sposito, 1989).

Scientific literature documents considerable experimental data for As and other trace elements in systems with one mineral phase, and SCMs have been applied to accurately describe these data (Dzombak and Morel, 1990; Goldberg, 1998; Swedlund and Webster, 1999; Dixit and Hering, 2003, 2006; Ali and Dzombak, 1996; Davis et al., 1978; Westall and Hohl, 1980; Belzile and Tessier, 1990; Manning and Goldberg, 1996, 1997; Sadiq, 1997). The application of SCMs to natural sediments of varying mixtures of minerals is difficult because of the presence of secondary minerals and organic coatings (Davis et al., 2004; Coston et al., 1995; Padmanabhan and Mermut, 1996; Penn et al., 2001). A component

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additivity (CA) approach is commonly used for SCMs, where it is assumed that a mineral assemblage is composed of a mixture of one or more pure phases, whose surface chemical reactions are known from independent experiments of each phase (Davis et al., 1998, 2004; Cowan et al., 1992; Turner et al., 1996; Arnold et al., 2001; Prikryl et al., 2001). The next step is to measure the relative amounts of surface areas of each mineral present in the soils or sediments. Then, adsorption of the mixture of mineral phases can be predicted by an equilibrium calculation, without any fitting of experimental data for the mixture (Honeyman, 1996). In the CA approach, it is commonly assumed that one mineral phase dominates adsorption (Davis et al., 1998; Schmeide et al., 2000; Barnett et al., 2002; Waite et al., 2000), which facilitates a straightforward equilibrium calculation if the exposed surface area and surface-site density of that mineral phase in the soil or sediment can be quantified. SCMs typically use a combination of minerals with varying surface properties in order to describe the formation of surface complexes of elements present in groundwater on different mineral surfaces.

Successful SCM simulation depends on appropriate selection of internally consistent intrinsic surface constants, accurate chemical analysis of groundwater, and proper quantification of sorbents and their surface properties in each sediment sample. Although many published sorption databases related to As and other species on different sorbent surfaces exist (Dixit and Hering, 2003, 2006; Manning and Goldberg, 1996; Sigg, 1979; Appelo et al., 2002; Van Geen et al., 1994), few reliable and internally consistent sorption databases are available to quantify all of the surface species of interest and relevant parameters of the models (Dzombak and Morel, 1990; Sverjensky and Sahai, 1996; Sahai and Sverjensky, 1997a,b). This situation has changed somewhat in recent years with the increased availability of sorption data for surface reactions related to As and other elements on different metal oxide surfaces. However, little information has been reported on the predictability and applicability of SCMs to complex natural sediments (Miller, 2000, 2001; Davis et al., 1998, 2004; Appelo et al., 2002; US Geological Survey, 1994; Wang et al., 1997; Turner and Pabalan, 1999; Tessier et al., 1996; Fukushi and Sato, 2005). A review of the literature indicates that the use of SCMs to predict the environmental mobility of As or other trace metals in groundwater has been limited (Dzombak and Morel, 1990; Tessier et al., 1996; Miller, 2001; Smith and Jenne, 1991). Geochemist's Workbench (Bethke, 2006), PHREEQC (Parkhurst and Appelo, 1999), and MINT-EQA2 (Allison et al., 1991) are the most versatile of the presently available geochemical codes that use SCMs for incorporating multiple levels of uncertainty.

In general, impacts from As to municipal-supply water systems in Arkansas are low as most of the municipal-supply water systems abstract water from deeper Tertiary aquifers where As is usually <0.5 µg/L. It has been reported that irrigation water wells completed in the shallow (25–30 m below ground surface) Mississippi River Valley alluvial aquifer in southeastern Arkansas has As concentrations (<0.5–77 µg/L) exceeding the US EPA standard of 10 µg/L (Kresse and Fazio, 2002, 2003; Sharif, 2007; Sharif et al., 2008a,b). Approximately 200 public water supply wells draw water from the shallow Mississippi River Valley alluvial aquifer serving about 450,000 people. So, the potential health impact of As to drinking water supply systems in Arkansas is still significant. Hydrogeochemical data and the redox environment in the Mississippi River Valley alluvial aquifer suggest reductive dissolution of HFO as the dominant As release mechanism (Kresse and Fazio, 2002, 2003; Sharif, 2007; Sharif et al., 2008a,b). Gypsum solubility and simultaneous SO_4^{2-} reduction with co-precipitation of As and sulfide is an important limiting process controlling the concentration of dissolved As in groundwater. Spatial and temporal variability of As in groundwater is controlled by spatial distribution and

the redox state of individual redox zones in the aquifer, which is controlled by recharge potential, permeability of the surface aquitard, intensity of irrigation, and local flow dynamics in the aquifer. The redox state is the primary control on the rate of HFO reduction and the amount of As in groundwater (Sharif et al., 2008a,b).

This paper is part of a comprehensive research program with a primary goal of understanding the distribution and mobilization of As in groundwater in the Mississippi River Valley alluvial aquifer (Bayou Bartholomew watershed) of southeastern Arkansas. The purpose of this paper is to evaluate the ability of the SCMs based on a CA approach using DLM in the geochemical code PHREEQC to predict solid phase As occurrence in the sediments collected from six boreholes drilled into the Mississippi River Valley alluvial aquifer. The DLM was used with a number of adjustable or measured parameters, including the stability or equilibrium constants, total site concentration of reactive surface hydroxyl groups, total specific surface area, total solid concentration, and water–mineral ratio.

2. Study area

The study area, approximately 225 km², is located in the southern part of Jefferson County, Arkansas (Fig. 1). It is bounded by the Arkansas River to the NE and Bayou Bartholomew to the SW. The area comprises the northeastern part of the Bayou Bartholomew watershed and is entirely covered by Holocene alluvial deposits of the Mississippi and Arkansas rivers. The Holocene alluvial deposits are represented by a downward-coarsening sequence from clays, silts and fine sands at the surface (herein referred to as the surface aquitard), to coarse sands and gravels at the base. Pleistocene alluvial deposits of the Mississippi and Arkansas rivers form terraces with minor exposures of Tertiary-age strata along topographically high areas, and are found beyond the western part of the study area (Kresse and Fazio, 2002). The thickness of the surface aquitard varies from <6 to 12 m. The thickness of the alluvial aquifer ranges from 18 to 43 m (Kleiss et al., 2000). An assemblage of channel fill, point bar, and back-swamp deposits associated with present and former channels of the Mississippi and Arkansas rivers produced heterogeneity in lithology and resulted in large spatial and vertical variations in the hydraulic properties within the aquifer system (Joseph, 1999). The regional direction of groundwater flow is generally to the south and east except where affected by intense groundwater withdrawals (Schrader, 2001). Row-crop agriculture represents the major land use in the floodplain, whereas silviculture dominates the land use in the terrace portion of the watershed. Eastern Arkansas receives an annual precipitation of 1.2–1.4 m (Freiwald, 1985).

3. Materials and methods

Three pairs of nested monitoring wells (10.6 and 36.6 m deep) were drilled, installed and developed at three contrasting sites selected as a high As (>50 µg/L) area in the NW (DRL1), a medium As (10–50 µg/L) area in the south (DRL2), and a low As (<10 µg/L) area in the NE (DRL6). The capital letters "D" and "S" are used after the site designation letters (DRL1, DRL2 or DRL6) to describe deep and shallow monitoring wells, respectively.

The materials and methods consist of collection and preservation of soil cuttings (Sharif et al., 2008a,b), preparation of sediment samples for a modified 5-step sequential extraction procedure (Tessier et al., 1979; Chao and Zhou, 1983), X-ray diffraction (XRD) and scanning electron microscopy (SEM) analysis, groundwater sampling, field monitoring and laboratory analyses. The following section is excerpted from previous papers (Sharif, 2007; Sharif et al., 2008a,b).

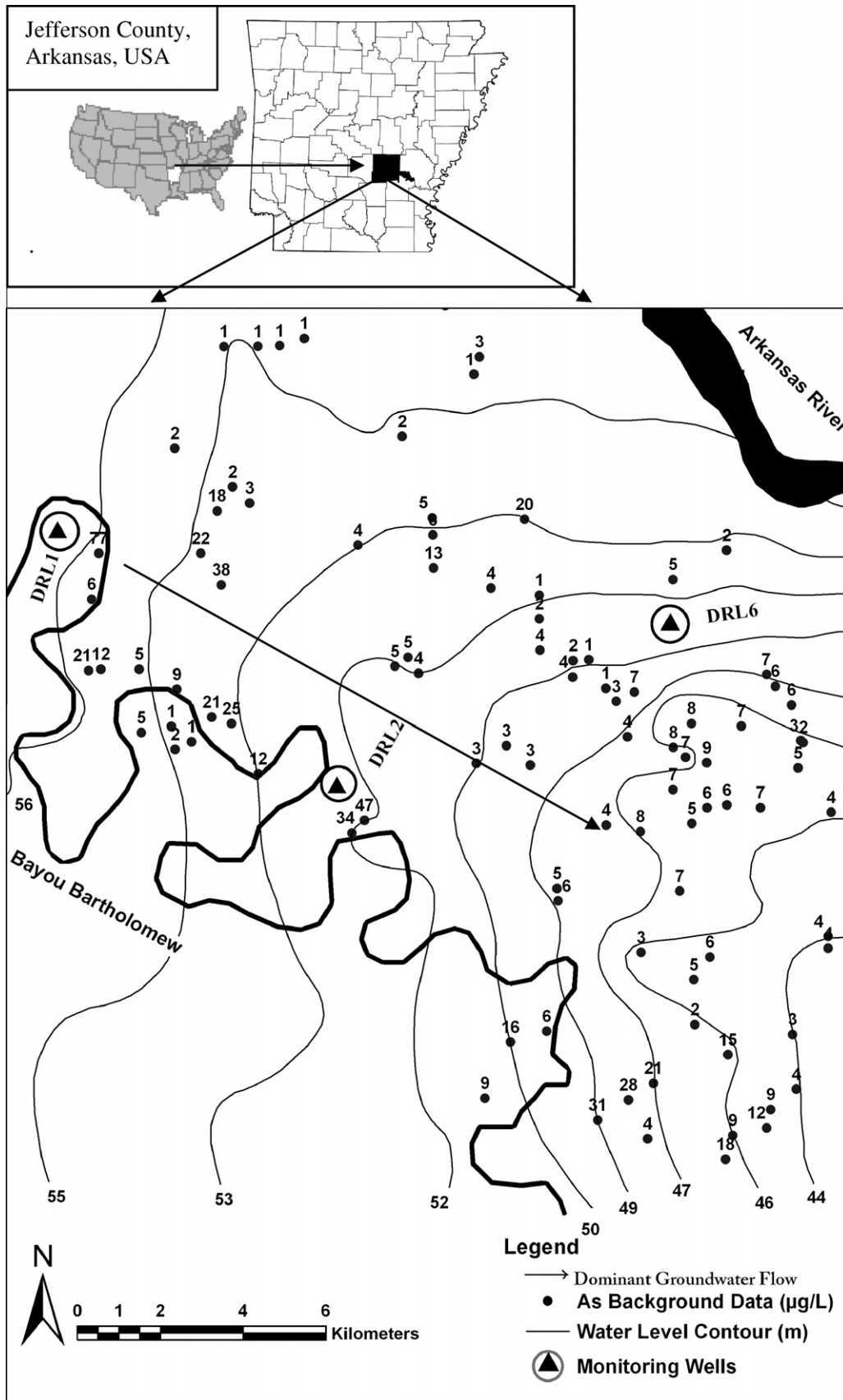


Fig. 1. Location of study area, monitoring well sites, water level map, and As background data in groundwater (Note: modified from Fig. 1 of Sharif et al. (2008a,b)).

3.1. Preparation of sediment samples and sequential extraction

Sealed sections of the stored sediment samples were opened and sub-sampled in February 2006 for grain-size, porosity and geochemical analyses. Approximately 100 g of stored sediment cores were separated and dried below 40 °C in an oven. The sediment samples were crushed using a conventional porcelain pestle and mortar, and passed through a 1 mm screen. These screened sediment samples were used for a 5-step sequential extraction procedure (Tessier et al., 1979; Chao and Zhou, 1983) for major cations and trace metals, and As. Grain-size analysis of the fine fraction was conducted with little or no crushing on dried pre-screened samples by a micro-pipette method (Miller and Miller, 1987). Porosity was measured by weighing 50 mL hand-packed sediments in a graduated cylinder. Water was slowly added to the 50 mL mark and the sample shaken to remove air bubbles and saturate evenly with water. Gravimetric porosity $[(1 - (\rho_b/\rho_s))]$ was calculated by mean particle density (ρ_s = mass of solids/volume of solids) and dry bulk density (ρ_b = mass of dry solids/volume of dry solids). The 5-step sequential extraction procedure (Tessier et al., 1979; Chao and Zhou, 1983) was completed using 2 g dry-sieved sediment by the procedures listed below. Details of the 5-step sequential extraction procedure and results are presented in Sharif (2007) and Sharif et al. (2008a,b). The results of leachable fractions of As extracted by step 3 (Chao reagent) and step 5 (hot HNO₃) were used in the simulation of SCMs as shown in Tables 1 and 2:

1. *Exchangeable*: 16 mL of 1 M Na acetate to pH 8.2 for 1 h.
2. *Carbonates*: 16 mL of 1 M Na acetate to pH 5 for 4 h.
3. *Amorphous Fe and Mn oxides*: 40 mL of 0.25 M NH₂OH–HCl in 0.25 M HCl; heated to 50 °C for 30 min.
4. *Organic matter*: 6 mL of 0.02 M HNO₃ and 10 mL of 30% H₂O₂ to pH 2 with HNO₃; heated to 85 °C for 2 h, and later 6 mL of 30% H₂O₂ added and heated to 85 °C for 3 h.
5. *Hot HNO₃-leachable*: 15 mL 7 M HNO₃ for 2.5 h at 70 °C for the first 30 min. and later at 100 °C for the next 2 h.

The hot HNO₃ extraction (Andersson et al., 1991) step in the sequential extraction procedures was used instead of the rigorous

HF-HClO₄ extraction described in the original method to represent the least environmentally-available As. A total of 60 sediment samples were extracted by using these extraction procedures. The extracted solutions were shipped to the Arkansas Department of Environmental Quality (ADEQ) laboratory, Little Rock, Arkansas, for analysis by inductively coupled plasma mass spectrometry (ICP-MS).

XRD and SEM analyses of sediments were conducted and are described in detail in Sharif (2007) and Sharif et al. (2008a,b). Detailed descriptions of the groundwater sampling, field monitoring, and laboratory analyses protocols and procedures are also included in the previously cited publications.

3.2. Geochemical modeling

The equilibrium SCM of PHREEQC (Parkhurst and Appelo, 1999) was used to predict the differences between sorbed As on HFO phases derived from sequentially extracted chemical data and modeled simulations. The DLM model of Dzombak and Morel (1990) was used to simulate surface complexation reactions. The model sorbents were selected as ferrihydrite and goethite. Ligand sorption was considered to occur at two sorption sites on ferrihydrite with a density of 0.005 mol/mol Fe for the strong site, and 0.2 mol/mol Fe for the weak site (Dzombak and Morel, 1990). Ligand sorption for goethite was considered to occur at only one sorption site with a density of 0.0000384 mol sites/m² (Manning and Goldberg, 1996). The surface areas of ferrihydrite and goethite were considered as 600 m²/g and 43.7 m²/g, respectively (Dzombak and Morel, 1990; Manning and Goldberg, 1996). The surface-site density of sorbent phases for individual sediment samples was calculated from: (1) the Fe concentrations in the sediment extracts generated using Chao reagent (Table 1) and hot HNO₃ (Table 2) of Tessier's 5-step sequential extraction procedures, (2) the water–rock ratio from measured porosity, (3) assumed molecular weight, and (4) default surface-site density of sorbent phases (Dzombak and Morel, 1990; Manning and Goldberg, 1996). The WATEQ4F thermodynamic database of PHREEQC was used for surface reactions between As and ferrihydrite. The database was modified by adding silica sorption data on ferrihydrite from Swedlund

Table 1

Surface site densities of ferrihydrite and goethite based on chemical data extracted by Chao reagent. Site density is expressed as mol sites/mol Fe.

Sr. no.	Sample ID	Lithology	Depth, m bgs	Fe (Chao), mg/kg	kg Seds. per kg H ₂ O	Ferrihydrite, g/kg H ₂ O	Ferrihydrite strong site	Ferrihydrite weak site	Goethite single site
1	DRL12615	Clayey silt	6.1	9.2E+02	8.00	11.67	6.57E–04	2.63E–02	1.96E–03
2	DRL12617	Sandy silt	6.4	6.8E+02	7.35	7.92	4.46E–04	1.78E–02	1.33E–03
3	DRL12618	Clayey silt	7.0	8.3E+02	8.00	10.53	5.93E–04	2.61E–02	1.77E–03
4	DRL12621	Silty sand	7.6	2.7E+02	5.72	2.48	1.39E–04	5.58E–03	4.16E–04
5	DRL12623-1	Clayey silt	8.5	6.2E+02	8.00	7.85	4.42E–04	1.77E–02	1.32E–03
6	DRL12624	Clayey silt	8.8	6.7E+02	8.00	8.49	4.78E–04	1.91E–02	1.42E–03
7	DRL12625-1	Sand	11.0	5.7E+02	6.18	5.55	3.13E–04	1.25E–02	9.32E–04
8	DRL12634	Sand	24.4	1.5E+02	6.18	1.51	8.53E–05	3.41E–03	2.54E–04
9	DRL12635	Sand	25.9	1.3E+02	6.18	1.32	7.45E–05	2.98E–03	2.22E–04
10	DRL12638-3	Sand	33.5	3.9E+02	3.98	2.46	1.39E–04	5.55E–03	4.14E–04
11	DRL12639-3	Sand	36.6	5.5E+02	6.18	5.41	3.04E–04	1.22E–02	9.07E–04
12	DRL12640	Clay lens	36.6	1.5E+03	8.00	19.65	1.11E–03	4.43E–02	3.30E–03
13	DRL22610	Silty sand	6.7	6.1E+02	7.35	7.16	4.03E–04	1.61E–02	1.20E–03
14	DRL22611	Silt	7.6	2.0E+03	8.00	24.90	1.40E–03	5.61E–02	4.18E–03
15	DRL22612	Sand	9.1	4.7E+02	6.18	4.62	2.60E–04	1.04E–02	7.75E–04
16	DRL22613-2	Sand	10.7	1.6E+03	6.18	15.51	8.73E–04	3.49E–02	2.60E–03
17	DRL22618-2	Sand	18.3	6.4E+01	6.18	0.62	3.52E–05	1.41E–03	1.05E–04
18	DRL22620-2	Sand	21.3	1.2E+02	6.18	1.17	6.59E–05	2.64E–03	1.96E–04
19	DRL22623	Sand	30.5	1.9E+02	6.18	1.86	1.05E–04	4.19E–03	3.12E–04
20	DRL62615	Clayey sand	8.5	1.4E+03	7.95	17.10	9.63E–04	3.85E–02	2.87E–03
21	DRL62616	Silty sand	8.8	1.5E+03	7.35	17.15	9.66E–04	3.86E–02	2.88E–03
22	DRL62618	Silty sand	10.1	1.0E+04	7.35	117.16	6.60E–03	2.64E–01	1.97E–02
23	DRL62619	Sand	10.2	7.1E+02	6.18	6.93	3.90E–04	1.56E–02	1.16E–03
24	DRL62625	Sand	18.3	1.8E+03	6.18	18.02	1.01E–03	4.06E–02	3.02E–03
25	DRL62626	Sand	21.3	1.3E+03	6.18	12.83	7.22E–04	2.89E–02	2.15E–03
26	DRL62628	Sand	24.4	8.4E+02	6.18	8.26	4.65E–04	1.86E–02	1.39E–03

Table 2
Surface site densities of ferrihydrite and goethite based on chemical data extracted by hot HNO₃. Site density is expressed as mol sites/mol Fe.

Sr. no.	Sample ID	Lithology	Depth, m	Fe (HNO ₃), mg/kg seds	kg Seds. per kg H ₂ O	Ferrihydrite, g/kg H ₂ O	Ferrihydrite strong site	Ferrihydrite weak site	Goethite single site
1	DRL12615	Clayey silt	6.1	9100	8.00	115.75	6.5E-03	2.6E-01	1.9E-02
2	DRL12617	Sandy silt	6.4	7375	7.35	86.19	4.9E-03	1.9E-01	1.4E-02
3	DRL12618	Clayey silt	7.0	15,300	8.00	194.62	1.1E-02	4.4E-01	3.3E-02
4	DRL12621	Silty sand	7.6	4700	5.72	42.72	2.4E-03	9.6E-02	7.2E-03
5	DRL12623-1	Clayey silt	8.5	11,050	8.00	140.56	7.9E-03	3.2E-01	2.4E-02
6	DRL12624	Clayey silt	8.8	12,825	8.00	163.13	9.2E-03	3.7E-01	2.7E-02
7	DRL12625-1	Sand	11.0	3475	6.18	34.16	1.9E-03	7.7E-02	5.7E-03
8	DRL12634	Sand	24.4	518	6.18	5.09	2.9E-04	1.1E-02	8.5E-04
9	DRL12635	Sand	25.9	1080	6.18	10.62	6.0E-04	2.4E-02	1.8E-03
10	DRL12638-3	Sand	33.5	1593	3.98	10.06	5.7E-04	2.3E-02	1.7E-03
11	DRL12639-3	Sand	36.6	4700	6.18	46.21	2.6E-03	1.0E-01	7.8E-03
12	DRL12640	Clay lens	36.6	7600	8.00	96.67	5.4E-03	2.2E-01	1.6E-02
13	DRL22610	Silty sand	6.7	3550	7.35	63.97	3.6E-03	1.4E-01	1.1E-02
14	DRL22611	Silt	7.6	12,775	8.00	161.48	9.1E-03	3.6E-01	2.7E-02
15	DRL22612	Sand	9.1	1943	6.18	24.55	1.4E-03	5.5E-02	4.1E-03
16	DRL22613-2	Sand	10.7	17,300	6.18	218.68	1.2E-02	4.9E-01	3.7E-02
17	DRL22618-2	Sand	18.3	618	6.18	6.07	3.4E-04	1.4E-02	1.0E-03
18	DRL22620-2	Sand	21.3	1208	6.18	11.87	6.7E-04	2.7E-02	2.0E-03
19	DRL22623	Sand	30.5	868	6.18	8.53	4.8E-04	1.9E-02	1.4E-03
20	DRL62615	Clayey sand	8.5	8450	7.95	106.81	6.0E-03	2.4E-01	1.8E-02
21	DRL62616	Silty sand	8.8	4175	7.35	48.79	2.7E-03	1.1E-01	8.2E-03
22	DRL62618	Silty sand	10.1	16,950	7.35	198.09	1.1E-02	4.5E-01	3.3E-02
23	DRL62619	Sand	10.2	1155	6.18	11.36	6.4E-04	2.6E-02	1.9E-03
24	DRL62625	Sand	18.3	2625	6.18	25.81	1.5E-03	5.8E-02	4.3E-03
25	DRL62626	Sand	21.3	3175	6.18	31.22	1.8E-03	7.0E-02	5.2E-03
26	DRL62628	Sand	24.4	2078	6.18	20.42	1.2E-03	4.6E-02	3.4E-03

Table 3
Important sorption reactions with surface constants of As with ferrihydrite and goethite that were added to WATEQ4F thermodynamic database in PHREEQC.

Surface reaction	Log K_{int}	References
<i>Ferrihydrite</i>		
Hfo_OH + H ₄ SiO ₄ = Hfo_H ₃ SiO ₄ + H ₂ O	4.28	Swedlund and Webster (1999)
Hfo_OH + H ₄ SiO ₄ = Hfo_H ₂ SiO ₄ + H ₂ O + H ⁺	-3.22	Swedlund and Webster (1999)
Hfo_OH + H ₄ SiO ₄ = Hfo_H ₂ SiO ₄ + H ₂ O + 2H ⁺	-11.69	Swedlund and Webster (1999)
<i>Goethite</i>		
Goe_OH + H ⁺ = Goe_OH ²⁺	7.52	Dixit and Hering (2003)
Goe_OH = Goe_O ⁻ + H ⁺	-10.6	Dixit and Hering (2003)
Goe_OH + H ₃ PO ₄ = Goe_H ₂ PO ₄ + H ₂ O	8.05	Sigg (1979)
Goe_OH + H ₃ PO ₄ = Goe_HPO ₄ ⁻ + H ⁺ + H ₂ O	3.40	Sigg (1979)
Goe_OH + H ₃ PO ₄ = Goe_PO ₄ ⁻² + H ₂ O + 2H ⁺	-2.20	Sigg (1979)
Goe_OH + AsO ₄ ⁻³ + 3H ⁺ = Goe_H ₂ AsO ₄ + H ₂ O	30.94	Dixit and Hering (2003)
Goe_OH + AsO ₄ ⁻³ + 2H ⁺ = Goe_HAsO ₄ ⁻ + H ₂ O	26.75	Dixit and Hering (2003)
Goe_OH + AsO ₄ ⁻³ + H ⁺ = Goe_AsO ₄ ⁻² + H ₂ O	20.16	Dixit and Hering (2003)
Goe_OH + AsO ₃ ⁻³ + 3H ⁺ = Goe_H ₂ AsO ₃ + H ₂ O	39.87	Dixit and Hering (2003)
Goe_OH + AsO ₃ ⁻³ + 2H ⁺ = Goe_HAsO ₃ ⁻ + H ₂ O	32.34	Dixit and Hering (2003)
Goe_OH + H ₄ SiO ₄ ⁻³ = Goe_H ₃ SiO ₄ + H ₂ O	4.35	Sigg (1979)
Goe_OH + H ₄ SiO ₄ = Goe_H ₂ SiO ₄ ⁻ + H ₂ O + H ⁺	-3.04	Sigg (1979)
Goe_OH + 2H ⁺ + CO ₃ ⁻² = Goe_HCO ₃ + H ₂ O	20.78	Van Geen et al. (1994)
Goe_OH + H ⁺ + CO ₃ ⁻² = Goe_CO ₃ ⁻ + H ₂ O	12.71	Van Geen et al. (1994)
Goe_OH + CO ₃ ⁻² = Goe_OHCO ₃ ⁻²	3.56	Appelo et al. (2002)
Goe_OH + F ⁻ = Goe_F + OH ⁻	-4.54	Sigg (1979)
Goe_OH + SO ₄ ⁻² + 2H ⁺ = Goe_HSO ₄ + H ₂ O	13.61	Ali and Dzombak (1996)
Goe_OH + SO ₄ ⁻² + H ⁺ = Goe_SO ₄ ⁻ + H ₂ O	8.19	Ali and Dzombak (1996)
Goe_OH + SO ₄ ⁻² = Goe_OSO ₄ ⁻³ + H ⁺	-6.26	Ali and Dzombak (1996)
Goe_OH + SO ₄ ⁻² + Cu ²⁺ = Goe_OHCuSO ₄	9.46	Ali and Dzombak (1996)
Goe_OH + Zn ²⁺ + H ₂ O = Goe_OZn(OH) ₂ + 3H ⁺	-18.34	Palmqvist et al. (1999)
Goe_OH + Zn ²⁺ = Goe_OZn ⁺ + H ⁺	-2.14	Palmqvist et al. (1999)
Goe_OH + Fe ²⁺ + H ₂ O = Goe_OFeOH ⁺ + 2H ⁺	-10.95	Dixit and Hering (2006)
Goe_OH + Fe ²⁺ = Goe_OFe ⁺ + H ⁺	-0.60	Dixit and Hering (2006)
Goe_OH + Cu ²⁺ = Goe_OCu ⁺ + H ⁺	2.93	Weirich (2000)
Goe_OH + Ni ²⁺ = Goe_ONi ⁺ + H ⁺	0.46	Weirich (2000)
Goe_OH + H ₃ BO ₃ = Goe_H ₂ BO ₃ ⁻ + H ₂ O	5.52	Goldberg and Glaubig (1985)
Goe_OH + Ca ²⁺ = Goe_OCa ⁺ + H ⁺	-7.18	Ali and Dzombak (1996)
Goe_OH + Mg ²⁺ = Goe_OMg ⁺ + H ⁺	-5.94	Sigg (1979)

and Webster (1999), which is internally consistent with the sorption database of Dzombak and Morel (1990). The surface reactions for goethite were taken from the RES3T (Rossendorf Expert System for Surface and Sorption Thermodynamics) thermodynamic sorption database (Brendler et al., 2002), which includes sorption constants for the DLM model summarized from different sources. The sorption database of goethite was normalized by converting the reference site density to 2.31 sites/nm² for all surface reactions to get internal consistency, following the procedures of Kulik (2002). Important sorption reaction constants that were added to the WATEQ4F thermodynamic database of PHREEQC are given in Table 3. The model was tested on 26 selected sediment samples collected along the depth profile of six boreholes (DRL1S, DRL1D, DRL2S, DRL2D, DRL6S and DRL6D). The data for chemical analyses of groundwater from corresponding monitoring wells were used in the respective model input (Sharif, 2007; Sharif et al., 2008a,b). Groundwater chemistry of the shallow well was used in the model input for sediments up to a depth of 10.6 m. Groundwater chemistry of the deep well was used in the model input for sediments collected from 18 to 36.6 m.

4. Results

Detailed results for sediment geochemistry, groundwater chemistry, XRD and SEM analyses, and interpretation of these analyses in the light of redox conditions and As mobilization mechanisms are described by Sharif (2007) and Sharif et al. (2008a,b). The following section summarizes the As mobilization mechanisms reported elsewhere (Sharif, 2007; Sharif et al., 2008a,b) and the results of the SCM approach.

4.1. As mobilization mechanisms

Arsenic is positively correlated to Fe extracted by Chao reagent ($r = 0.83$) and HNO₃ ($r = 0.85$). Iron speciation data in sediments vary with depth in the aquifer (Sharif et al., 2008b). Increasing depth has a positive relationship ($r = 0.56$) with the solid phase Fe(II)/Fe ratio (the ratio of Fe concentration in the extracts of Chao

reagent and hot HNO₃), but it has a negative relationship ($r = -0.45$) with As extracted by Chao reagent. The solid phase Fe(II)/Fe ratio is positively correlated ($r = 0.76$) to As extracted by Chao reagent. Although the solid phase Fe(II)/Fe ratio increases with depth, the amount of reducible Fe (HFO), as well as its complexed As, decreases with depth. One cannot ignore the possibility of historic flushing of significant dissolved As derived from reductive dissolution of HFO by advective transport, coupled with less sorptive capacity of HFO with later development of crystallinity at depth. Interpretation of geochemical data reveals that both amorphous and crystalline Fe oxide phases in the shallow aquifer are under relatively oxidizing conditions, and represent a potential sink for As. Amorphous and crystalline Fe oxide phases in the deep aquifer are under a reducing environment, favoring reductive dissolution of HFO and concomitant release of As into groundwater. The sharp depletion of SO₄²⁻ concentrations in groundwater from shallow (DRL1S) to deep (DRL1D) monitoring wells may be the result of simultaneous reduction of HFO and SO₄²⁻ with co-precipitation of dissolved As into sulfides. This is supported by a mutual exclusivity of As with SO₄²⁻ from 118 well-water analyses in the Bayou Bartholomew watershed (Kresse and Fazio, 2002).

4.2. Surface complexation modeling

The DLM option of the SCM in the geochemical code PHREEQC was implemented using ferrihydrite and goethite as the sorbents. The model was run using As data for sediments extracted by Chao reagent (As attached to amorphous Fe and Mn oxides and oxyhydroxides) and hot HNO₃ (As attached to crystalline Fe and other metal oxides). The model results are satisfactory for DRL1S, where the redox condition is relatively oxic or mildly suboxic. However, for the deep alluvial aquifer (21–36.6 m) where the redox condition is suboxic to anoxic, the model results are unsatisfactory. The model shows a contrasting variation between modeled and extracted As in the sediments along the depth profile. Primarily, the model output is very sensitive to the sediment type and the extraction method used, which controls the surface-site density and sorption intensity. The model output is very sensitive to groundwater composition, which controls competitive sorption of

Table 4

Model results using As extracted by Chao reagent.

Sample ID	Lithology	Depth, m bgs ^a	Extracted As	Model	Difference (%) between
			Chao reagent (mg/kg)	Derived As (mg/kg)	Modeled and extracted As (Chao reagent)
DRL12615	Clayey silt	6.1	0.68	0.34	49
DRL12617	Sandy silt	6.4	0.49	0.26	47
DRL12618	Clayey silt	7.0	0.57	0.32	44
DRL12621	Silty sand	7.6	0.23	0.10	55
DRL12623-1	Clayey silt	8.5	0.43	0.24	45
DRL12624	clayey silt	8.8	0.52	0.25	52
DRL12625-1	Sand	10.2	0.24	0.22	8
DRL12634	Sand	24.4	0.04	0.90	-2149
DRL12635	Sand	25.9	0.21	0.79	-286
DRL12638-3	Sand	33.5	0.14	1.72	-1167
DRL12639-3	Sand	36.6	0.17	3.17	-1767
DRL12640	Clay lens	36.6	1.10	8.99	-717
DRL22610	Silty sand	6.7	0.22	1.42	-548
DRL22611	Silt	7.6	0.56	4.71	-737
DRL22612	Sand	9.1	0.12	1.63	-1258
DRL22613-2	Sand	10.6	0.65	5.48	-746
DRL22618-2	Sand	18.3	0.12	0.52	-333
DRL22620-2	Sand	21.3	0.37	0.97	-162
DRL22623	Sand	30.5	0.12	1.55	-1192
DRL62615	Clayey sand	8.5	0.33	8.42	-2491
DRL62616	Silty sand	8.8	0.21	11.72	-5501
DRL62618	Silty sand	10.1	5.10	78.5	-1439
DRL62619	Sand	10.2	2.02	4.43	-119

^a bgs: Below ground surface.

Table 5
Model results using As extracted by hot HNO₃.

Sample ID	Lithology	Depth, m bgs ^a	Extracted As	Model	Difference (%) between
			HNO ₃ (mg/kg)	Derived As (mg/kg)	Modeled and extracted As (HNO ₃)
DRL12615	Clayey silt	6.1	1.74	0.8	53
DRL12617	Sandy silt	6.4	1.41	0.7	54
DRL12618	Clayey silt	7.0	2.88	1.4	51
DRL12621	Silty sand	7.6	0.79	0.4	45
DRL12623-1	Clayey silt	8.5	1.29	1.0	21
DRL12624	Clayey silt	8.8	1.62	1.2	29
DRL12625-1	Sand	10.2	0.23	0.3	-37
DRL12634	Sand	24.4	0.14	0.4	-165
DRL12635	Sand	25.9	0.31	0.8	-158
DRL12638-3	Sand	33.5	0.36	1.1	-216
DRL12639-3	Sand	36.6	1.15	3.4	-196
DRL12640	Clay lens	36.6	3.45	5.4	-57
DRL22610	Silty sand	6.7	0.42	9.39	-2122
DRL22611	Silt	7.6	1.72	21.18	-1133
DRL22612	Sand	9.1	0.27	4.16	-1470
DRL22613-2	Sand	10.6	3.60	37.58	-944
DRL22618-2	Sand	18.3	0.14	1.56	-1056
DRL22620-2	Sand	21.3	1.00	3.05	-204
DRL22623	Sand	30.5	0.20	2.14	-959
DRL62615	Clayey sand	8.5	0.86	33.88	-3828
DRL62616	Silty sand	8.8	0.46	25.67	-5480
DRL62618	Silty sand	10.1	22.8	66.34	-191
DRL62619	Sand	10.2	2.40	4.6	-92

^a bgs: Below ground surface.

As with other ions (e.g. HCO₃⁻, PO₄³⁻, H₄SiO₄⁰ and Fe²⁺) on reactive surface sites of sorbents.

For DRL1S (0–10 m), the model results (Tables 4 and 5) using ferrihydrite and goethite under-predicted (<50%) the extracted As concentration in sediments. Sediments from all other boreholes except DRL1S using ferrihydrite and goethite highly over-predicted (up to 56 times) the extracted As concentration in sediments.

5. Discussion

Selection of the proper HFO phases is one of the most important factors influencing the model fit, as each phase has a different specific surface area and sorption capacity. The ferrihydrite used in the simulation has a surface area and surface-site density over 13 times greater than that of goethite. There are various lines of evidence for the presence of both ferrihydrite and goethite in the sediments of the study area. Field evidence for the presence of ferrihydrite, such as fine Fe oxide staining or coating on sand grains, is readily observable. These hydrous Fe oxide coatings are easily observable under SEM. Goethite was detected by XRD in all the sediment samples. Magnetically separated minerals show both crystalline and amorphous morphologies under SEM. Saturation index calculations, and the results of inverse modeling, show that groundwater is undersaturated with respect to goethite and ferrihydrite, and these are dissolving along the flow path in the study area (Sharif et al., 2008a). There is no direct quantitative evidence for the presence of selected sorbent phases in the sediments. The amount of ferrihydrite and goethite was quantified from partial and operationally defined wet chemical extractions. Concentrations of Fe in sediments extracted by Chao reagent and hot HNO₃ extraction steps were used to back-calculate the amount of ferrihydrite and goethite using the molar ratios between ferrihydrite/Fe and goethite/Fe as 1.59. So, there are uncertainties in the selection and calculation of concentrations of the proper sorbent phases in the sediments used in the SCM.

Surface area and surface-site densities for selective sorbent phases are two important input parameters in the SCM simulation. Small variation in the surface-site densities of sorbents may pro-

duce a difference of several orders of magnitude in the modeled concentrations of As in sediments. The best available approach is to use the default surface parameters found in published papers (Dzombak and Morel, 1990; Dixit and Hering, 2003, 2006; Manning and Goldberg, 1996) as a starting point to incorporate these parameters into the model. Ambiguity and inconsistency exist in the selection of these two important surface parameters, which increases the level of uncertainty in the application of SCMs to predict As occurrence in sediments.

The model output is very sensitive to the concentration of As and other competitive ions in groundwater. The model showed that HCO₃⁻, H₄SiO₄, CO₃²⁻, PO₄³⁻ and Fe²⁺ occupied more than 98% of reactive surface sites of HFO; so, the concentrations of these ionic species in groundwater and their respective stability constants play an important role in regulating the complexation of As on HFO surfaces. PHREEQC lacks surface reactions between As and H₄SiO₄, which produces a high level of uncertainty in the prediction capacity of the model as it highly overpredicts modeled As. Surface reactions between As and H₄SiO₄ were incorporated into the model to improve the prediction capacity of the model (Swedlund and Webster, 1999). There are some inconsistencies in the values of intrinsic surface constants in the surface reactions of As related to HCO₃⁻, H₄SiO₄, CO₃²⁻, PO₄³⁻, and other ions in different published papers (Dzombak and Morel, 1990; Swedlund and Webster, 1999; Dixit and Hering, 2003, 2006; Wilkie and Hering, 1996). Very small variations of intrinsic surface constants for HCO₃⁻, H₄SiO₄, CO₃²⁻ and PO₄³⁻ produces a large difference in the model output; so, appropriate selection of intrinsic surface constants related to HCO₃⁻, H₄SiO₄, CO₃²⁻ and PO₄³⁻, and other ions is very important in model simulation. The SCM parameters for metal ion adsorption on reference phases (e.g. ferrihydrite) are usually based on experimental datasets generated in simple electrolyte solutions, which is very simplistic compared to complex natural groundwater conditions. The adsorption of major ions and organic acids in natural waters is known to cause significant changes in the point-of-zero-charge and iso-electric point of mineral phases (Fuerstenau et al., 1981; Davis and Kent, 1990), so the surface reactions in the model are not truly applicable for complex electrolyte solutions such as natural groundwaters. The surface reactions used in

the model are generated under different controlled environments in different laboratories, and under different electrolyte solutions. No evidence was found regarding the applicability of these surface reaction datasets under different redox conditions.

6. Conclusions

SCMs using internally consistent laboratory-derived sorption constants, calculated surface-site densities from chemical extraction data and published sorbent-site densities, measured water-rock ratios, and detailed chemical analyses of groundwater can be used to predict the distribution of As in sediments with a moderate to high level of uncertainty. The match between the modeled and extracted As by both Chao reagent and HNO₃ was not successful for sediments in the deeper part of the alluvial aquifer where redox conditions are suboxic to anoxic. Within this portion of the alluvial aquifer, the reducing environment favors reductive dissolution of HFO and concomitant release of sorbed As into groundwater. In the deep alluvial aquifer, HFO is considered as a potential source for dissolved As in groundwater. The SCM was relatively successful for a shallow borehole (DRL1S), where the redox environment is relatively oxidizing to very mildly reducing, and the reductive dissolution of HFO is not an important redox process. In DRL1S, HFO in the shallow aquifer is considered as a potential sink for As.

The accuracy of the model fit depends on the qualitative and quantitative determination of accurate solid sorbent phases, selection of proper extraction methods capable of extracting the target form of solid phases, inclusion of appropriate surface parameters and internally-consistent surface reaction constants for each of the sorbent phases, and detailed and accurate chemical analysis of groundwater, including speciation of As and Fe. The level of uncertainty inherent in the predicted capacity to detect As in sediments by SCMs can be improved by accurate quantification of sorbent phases and their surface-site densities for each sediment sample included in the model. The use of default surface-site densities proposed in the literature (Dzombak and Morel, 1990; Manning and Goldberg, 1996) to calculate modeled surface-site concentrations of individual sediment samples is not applicable for the entire depth profile, because redox environments and the relative aging status of HFO phases, which control the sorption capacity, are different at different depths. Determining individual surface properties of natural sorbents at different depths within different redox environments is necessary. Developing consensus on the appropriate extraction methods and sorption databases that can be used in SCMs for natural sediments is very important.

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