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Thermodynamics of the UPt$_3$ superconducting phase diagram

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In this paper we present a thermodynamic analysis of the UPt$_3$ superconducting phase diagram in the $H$-$T$ plane. The analysis relates the specific-heat jumps to the slopes of the four phase-transition lines. The existing data are found to be in good mutual agreement, and consistent with the assumption that the inner phase-transition line at low field, $T_c^*$, is second order for both $H||\hat{c}$ and $H\parallel\hat{c}$. For $H\parallel\hat{c}$, the inner phase-transition line at higher field, $H_{FL}$, is first order albeit with a small latent heat. For $H||\hat{c}$, it can be second order.

The heavy-fermion superconductor UPt$_3$ is a strong candidate for unconventional superconductivity. A number of experiments have shown the existence of multiple superconducting phases. Early measurements of the ultrasonic attenuation in the superconducting state revealed a peak in the attenuation as a function of field.1–3 This peak can be interpreted as a phase transition and the position of this line in the $H$-$T$ plane at finite fields as a phase boundary. This transition line was named the $H_{FL}$ transition as it was conjectured that it may be the signature of a transition in the flux lattice. Subsequent heat-capacity measurements showed two superconducting transitions, even at zero field, separated by about 50 mK.4 These heat-capacity signatures moved to lower temperatures and closer together as the field was increased.5,6

The position at which the phase-transition lines met was still an open question as the measurements were made on different samples and the ultrasonic attenuation signature faded out as one approached $H_{c2}$. A number of phase diagrams for superconducting UPt$_3$ had been proposed.

Recent ultrasonic velocity measurements7,8 on the heavy-fermion superconductor UPt$_3$ have confirmed the existence of three superconducting phases which appear to meet at a single point on the $H_{c2}$ curve. These measurements are the first to reveal the entire superconducting phase diagram on a single sample using a single measurement technique. Our measurements give strong support for a single multicritical point at which three superconducting phases and the normal phase meet. Yip, Li, and Kumar9 have derived thermodynamic constraints for such a multicritical point if at least three of the lines are second order. Since the upper critical field curve (above and below the multicritical point) is second order, if we assume that the transition $T_c^*$ is also second order (no evidence of a latent heat has been seen at this transition), then we can apply this analysis to the phase diagram obtained from ultrasonic measurements.

In Fig. 1 we show a schematic phase diagram for UPt$_3$. We follow the notations of Ref. 9. The phases are designated by the letters $A$, $B$, $C$, and $D$. The multicritical point is denoted by $P$, and we shall use $p_1$, $p_2$, $p_3$, and $p_4$ as the slopes at $P$ of the lines $AN$, $BN$, $CA$, and $CB$, respectively. $AN$ and $BN$ are the $H_{c2}$ curves below and above the multicritical point, $CA$ is the $T_c^*$ line and $CB$ is the $H_{FL}$ line. We define $r_3^A$ and $r_3^B$ as the ratios of the heat-capacity jumps $\Delta C_{AN}/\Delta C_{BN}$ and $\Delta C_{CA}/\Delta C_{BN}$, respectively.

It has been shown in Ref. 9 that, under the above assumptions, the slope of line $BC$ is given by

$$p_4 = \frac{p_3 r_3^A + p_1 - p_{12} - E^{1/2}}{r_3^B p_3^2 + r_1^2 - p_{12}^2},$$

where

$$E \equiv -cr_3^2,$$  

$$c \equiv r_3^B (1 - p_{13})^2 - (p_{13} - p_{12})^2,$$  

$$d \equiv r_3^B (1 - p_{12})^2.$$  

FIG. 1. Schematic phase diagram and notations.
and $p_{ij} = p_i/p_j$.

Since the slopes in our sound velocity measurement are more accurately measured than the specific-heat jumps in Refs. 5 and 6, we invert Eq. (1) to give $r_2$ in terms of the slopes and $r_1$. To do this we rewrite Eq. (1) as

$$r_2^2 = -b + c f^{1/2} / a^2$$

with

$$a = p_{13}(p_{13} p_{41} - 1),$$

$$b = r_1^2 (p_{41} - p_{12} p_{12} p_{41}),$$

Up on squaring both sides, we obtain a quadratic equation in $r_2^2$ which we can solve readily. The result is

$$r_2^2 = -b + c f^{1/2} / a^2$$

where

$$f = (2ab + c) - 4a^2 (b^2 - d).$$

There are two possible signs for Eq. (8). By examining Eq. (5) it is clear that the criterion is such that the combination occurring on the left-hand side of Eq. (5) must be nonpositive. We see that, since all the slopes are negative and $|p_{41}| > |p_{12}|$, $a$ is always negative for our present situation. The condition thus requires the sign be chosen so that

$$\pm f^{1/2} - c > 0.$$  

In Table I we list the slopes at the multicritical point for H16e. Using these values and Eq. (8), we calculate $r_2^2$ as a function of $r_1^2$. The results are shown in Fig. 2. The heat-capacity data of Hasselbach, Taillefer, and Flouquet show that, as the multicritical point is approached, the size of the lower heat-capacity jump decreases, approaching a very small value at the multicritical point; i.e., $r_2^2 \approx 0$. There appears to be no discontinuity in the size of the upper heat-capacity jump at the multicritical point so that one would expect $r_2^2 \approx 0$. Figure 2 shows that $r_2^2$ decreases from 0.116 at $r_1^2 = 1.0$ to 0 at $r_1^2 = 1.14$. [It is useful to note that, near this region $a, b < 0$ and $c, d > 0$. Thus, by Eq. (10), the $+$ sign in Eq. (8) has to be taken.] Thus, the experimental facts that the value of $r_1$ is close to 1 and the specific-heat jump on line $AC$ approaches a very small value as one approaches the multicritical point are consistent (c.f., Ref. 10). This can be regarded as supporting evidence for the assumption that line $AC$ is second order.

The thermodynamic analysis also allows us to determine the order of the transition $BC$. In Ref. 9 it has been shown that the condition for it to be second order is that $E = 0$. At $r_1^2 = 1.0$, $r_2^2 = 0.116$, we find that $E = 0.0974$, and when $r_1^2 = 1.14$, $r_2^2 = 0$, we find that $E = 0.154$ (see Fig. 2). If one is willing to accept the hypothesis that the ratios of the specific-heat jumps and the slopes of the transition lines are determined to an accuracy of $\sim 10\%$ or better, then it is extremely unlikely that $BC$ is a second-order transition, i.e., it is impossible to have $E = 0$ satisfied by varying the values of $p$'s and $r_1$ within their error bars. This point can be stated in an alternative way. $E = 0$ implies, by Eqs. (2) and (5),

$$r_2^2 = \frac{d}{c} = \frac{b}{a},$$

which requires $r_2^2 = 0.45$, $r_2^2 = 0.55$ or $r_2^2 = 0.27$, $r_2^2 = 0.98$; i.e., the specific-heat jump on the $H_{c2}$ line just below the multicritical point (i.e., $AN$) has to be only about $1/2$ of its value above it (i.e., $BN$) or less, while that on line $AC$ should be comparable to that on $BN$. These values strongly disagree with those from the experiments. 5

Granted that $BC$ is first order, we can then determine the latent heat associated with this phase transition. Following the reasoning in Ref. 9, it is easy to deduce the formula for the latent heat by subtracting the first derivatives of the free energy on either side of the transition

$$L = (\delta T) (\Delta C_{BN}) \left[ r_2^2 (1 - P_i) + r_2^2 (1 - P_4) - (1 - P_4) \right],$$

where $\delta T$ is the deviation of the temperature at the point of interest from that of the multicritical point (hence, in our present situation it is always negative), $\Delta C_{BN}$ is the jump in the specific-heat across line $BN$, the sign of which is such that it is positive for a (physical) positive specific-heat jump when one lowers the temperature through the $B \rightarrow N$ transition. At $r_1^2 = 1.0$, $r_2^2 = 0.116$, we find that the value of the quantity inside the square bracket is $-0.046$, and when $r_1^2 = 1.14$, $r_2^2 = 0$, we get $-0.06$. (Notice that $L > 0$ as it should be.) As a result, the predicted value of the latent heat is small near the multicritical point (note that it is linear in the distance away from this point and vanishes exactly at $P$; however, the analysis only holds close to the point $P$). Using the heat-capacity

\begin{table}[h]
\centering
\caption{Slopes for H16e (T/K).}
\begin{tabular}{cccccc}
\hline
$p_1$ & $p_2$ & $p_3$ & $p_4$ & $r_1^2$ & $r_2^2$ \\
\hline
-3.7 & -5.85 & -10.2 & -0.6 & 0.91 & 0.18 \\
1.0 & 0.11 & 1.14 & 0.0 & \\
\hline
\end{tabular}
\end{table}
data of Hasselbach, Taillefer, and Flouquet\(^4\) and a value of \(-0.05\) for the quantity inside the square brackets, we obtain a latent heat of 0.14 mJ/mol at a temperature 50 mK below the multicritical point. The heat capacity of \(\text{UPt}_3\) is about 225 mJ/mol K, implying that, in order to see the latent heat signature, one would require a temperature resolution better than 0.6 mK at 400 mK. This may explain the fact that the latent heat across the BC transition has not been observed.\(^5\)

For \(H||\hat{e}\) (Table II), \(p_1\) and \(p_2\) are nearly equal. The small difference between them (0.06 T/K) is close to the limits of our resolution. If we take them to be exactly equal at the point \(P\) (i.e., there is no kink in \(H_{c2}\) for \(H||\hat{e}\)), then, using Eq. (8), we see that \(r_3\) vanishes at \(r_1 = 1\). At this \(r_1\), \(E\) goes exactly to zero, implying that BC is a second-order transition. Specific-heat experiments\(^6\) have indicated that \(r_1\) is very close to 1, and \(r_3\) very small.

If we assume the small difference between \(p_1\) and \(p_2\) is real (i.e., there is, in fact, a small kink in \(H_{c2}\)), then we find that \(r_3\) vanishes when \(r_1 = 0.98\). Thus, the experimental evidence that \(r_3\) is indeed small and that \(r_1\) is close to one are consistent with each other and can be taken as evidence that the AC transition is second order. Moreover, at almost the same value of \(r_1\) (to within 1%), \(E\) vanishes, implying that the BC transition can be second order for \(H||\hat{e}\). One can also easily check that \(E\) is indeed very small for these specific-heat jumps, and even if it is not, an examination of Eq. (12) shows that the latent heat would be extremely small. However, we cannot rule out the possibility that it is first order.

We now comment on the data of Bruls \textit{et al}.\(^5\) A feature that distinguishes their data from ours is that the slopes of the transition lines are practically continuous across the point \(P\). Indeed, they draw their phase diagrams with precisely this feature. An analysis of this phase diagram, however, leads to significantly different thermodynamics from ours. With the assumptions \(p_1 = p_4\), \(p_2 = p_3\), one easily sees from Eq. (8) that

\[
r_3 = \frac{2a^2 - c \pm |c|}{2a^2}.
\]

Note that now \(c = r_3(1-p_1^2) > 0\), \(a\) is still negative, and, hence, as before, the + sign has to be chosen. This requires \(r_3 = 1\) and, by examining the expression for \(E\) [Eq. (2)] or Eq. (11), that the BC transition is necessarily second order, i.e., \(P\) is necessarily a tetracritical point. Using the result \(r_3 = 1\) and the fact that the total specific-heat jump from the normal phase to phase \(C\) should have identical values independently of whether one goes above or below the tetracritical point \(P\), one finds that the specific-heat jumps are continuous along the phase-transition lines (i.e., \(\Delta C_{AN} = \Delta C_{CR}, \Delta C_{AN} = \Delta C_{CA}\)). This is in strong contrast to the fact that the specific jump on \(AC\) is much smaller than that on \(AN\) or \(BN\) at \(P\).\(^6\) In fact, the Frankfort phase diagrams are as if one just superimposes two completely noninteracting order parameters.

A recent experiment by Trappmann, Löhneysen, and Taillefer\(^1\) measured the changes in \(T_c\) and \(T^*\) with pressure. The pressure-temperature phase diagram obtained appears to show a point at which three phases meet. A similar analysis of that phase diagram can be made (with pressure replacing magnetic field as the thermodynamic variable). If the transitions are all second order, then an additional phase-transition line should emerge from this point, unless all the lines are tangential with each other\(^7\) (see Refs. 12 and 13). An experiment to distinguish between these two possibilities is highly desirable.

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\begin{table}[h]
\centering
\caption{Slopes for \(H||\hat{e}\) (T/K).}
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline
\(p_1\) & \(p_2\) & \(p_3\) & \(p_4\) & \(r_3^1\) & \(r_3^2\) \\
\hline
-5.33 & -5.39 & -9.81 & -1.68 & 0.98 & 0.0 \\
\hline
\end{tabular}
\end{table}


10. The specific heat reported in Fig. 4 of Ref. 5 at lower transition is the sum of the contribution from both transitions, which Ref. 9 has erroneously taken to be the entire contribution from the lower transition only. Hence, Ref. 9 has investigated a parameter region irrelevant for the present phase diagram, and their conclusion that the measured specific-heat jumps are inconsistent with the slopes should be ignored.


12. One can see this by a microscopic picture as in that of Ref. 13.
There is one transition above the critical pressure $P^*$ only if the splitting field (the square of the magnetization in Ref. 13) vanishes above this pressure. For this to be possible this splitting field has to vanish as $(P - P^*)^2$ (not linearly). This pressure dependence will produce a phase diagram with three second-order transition lines meeting at a point at a common slope. If the splitting field is linear in $P - P^*$, then above $P^*$ there should still be two phase transitions.