1997

Explicit and Implicit Multidimensional Compact High-Resolution Shock-Capturing Methods: *Formulation*

Helen C. Yee

NASA Ames Research Center, yee@nas.nasa.gov

Follow this and additional works at: <http://digitalcommons.unl.edu/nasapub>

Yee, Helen C., "Explicit and Implicit Multidimensional Compact High-Resolution Shock-Capturing Methods: *Formulation*" (1997). *NASA Publications*. 243.

<http://digitalcommons.unl.edu/nasapub/243>

This Article is brought to you for free and open access by the National Aeronautics and Space Administration at DigitalCommons@University of Nebraska - Lincoln. It has been accepted for inclusion in NASA Publications by an authorized administrator of DigitalCommons@University of Nebraska - Lincoln.

Explicit and Implicit Multidimensional Compact High-Resolution Shock-Capturing Methods: *Formulation*¹

H. C. Yee

NASA Ames Research Center, Moffett Field, California 94035

Received October 2, 1995; revised September 27, 1996

Two families of explicit and implicit compact high-resolution shock-capturing methods for the multidimensional compressible Euler equations for fluid dynamics are constructed. Some of these schemes can be fourth- and sixth-order accurate away from discontinuities. For the semi-discrete case their shock-capturing properties are of the total variation diminishing (TVD), total variation bounded (TVB), total variation diminishing in the mean (TVDM), essentially nonoscillatory (ENO), or positive type of scheme for 1D scalar hyperbolic conservation laws and are positive schemes in more than one dimension. These higher-order compact schemes require the same grid stencil per spatial direction as their second-order noncompact cousins. The added terms over the second-order noncompact cousins involve extra vector additions but no added flux evaluations. Due to the construction, these schemes can be viewed as approximations to genuinely multidimensional schemes in the sense that they might produce less distortion in spherical type shocks and are more accurate in vortex type flows than schemes based purely on 1D extensions. The extension of these families of compact schemes to coupled nonlinear systems can be accomplished using the Roe approximate Riemann solver, the generalized Steger and Warming flux-vector splitting, or the van Leer type flux-vector splitting. Modification to existing high-resolution second- or third-order noncompact shock-capturing computer codes is minimal. High-resolution shock-capturing properties can also be achieved via a variant of the second-order Lax–Friedrichs numerical flux without the use of Riemann solvers for coupled nonlinear systems with comparable operations count to their classical shock-capturing counterparts. An efficient and compatible high-resolution shock-capturing filter for spatially fourth- and sixth-order classical compact and noncompact schemes is discussed. The simplest extension to viscous flows can be achieved by using the standard fourth-order compact or noncompact formula for the viscous terms. © 1997 Academic Press

I. INTRODUCTION

Spatially high-order compact schemes have attracted much attention in recent years due to their narrow grid stencil and a possible enhanced accuracy over their noncompact cousins. The majority of these developments are

aimed at wave propagation phenomena in computational aeroacoustic and computational electromagnetics, compressible shear-layer flow and direct numerical simulation of turbulence. The reader is referred to [1–4] for more details. The papers by Lele and Davis discuss wave resolution and phase errors for linear wave propagation. Although formal extension of their schemes to nonlinear systems is a straightforward, systematic extension of their idea to minimize phase errors and enhance wave resolution for coupled nonlinear systems of equations remains to be seen. Unlike the standard compact schemes that use symmetric compact operators, most of the recent development in compact methods uses asymmetric compact operators. They also require additional numerical dissipation for high gradient flows and generate spurious oscillations across shock waves and contact discontinuities even with added linear numerical dissipation. At present, there is no systematic extension of these asymmetric compact schemes to have high-resolution shock-capturing capability. Hybrid schemes using these types of compact methods in conjunction with completely different construction of high-resolution shock-capturing methods to enhance shock resolution were also proposed (see, e.g., [5]). A shortcoming of this type of hybridization is that the numerical solution might experience a nonsmooth transition at the switch to a different type of scheme, in addition to being sensitive to the choice of the numerical flux or slope limiter. For 2D and 3D complex shock wave and contact surface interactions, the switch mechanism can become less trivial.

The motivation of the present work is to construct schemes that retain some of the unique properties of compact schemes and have good shock resolution without resorting to the above type of hybridization. The base schemes used are compact schemes with symmetric compact operators for ease of extension to high-resolution shock-capturing schemes. It is anticipated that the proposed schemes will have a larger scope of applications than the aforementioned schemes. Independently, Steve Davis of Mississippi State proposed a similar idea [6] but with different construction than the present work. Here we define a compact scheme in

¹ A condensed version appeared in the *Proceedings of the 6th International Symposium on Computational Fluid Dynamics*, Sept. 4–8, 1995, Lake Tahoe, Nevada. A Major portion of this paper was published as NASA TM-110364, August 1995.

a broader sense than the traditional definition. For a desired order of accuracy, a scheme is defined as compact if its grid stencil is at least one grid point less than standard noncompact schemes (in each spatial direction).

This work was prompted by the unsatisfactory resolution of second-order total variation diminishing (TVD) schemes used for simulating mixing layer flows with coarse and nonadaptive grids (see, e.g., [7], and by the idea of [8, 9]). Abarbanel and Kumar proposed a spatially fourth-order compact scheme without the associated tridiagonal matrix inversion of standard compact schemes. It is computationally more attractive than standard compact scheme constructions. Just like schemes proposed in [2–4], their compact scheme exhibits poor shock resolution even with added linear numerical dissipation. Another idea by Cockburn and Shu that the author follows is the definition of a local mean. It is used as a reference for introducing local limiting to avoid spurious oscillation while keeping the formal accuracy of a class of compact schemes. However, this so-called total variation diminishing in the mean (TVDM) idea does not completely suppress spurious oscillations due to the limiting of the local mean step even for scalar hyperbolic conservation laws.

The objective of this work is fourfold. The first objective is to modify the Abarbanel–Kumar compact scheme to be high-resolution at discontinuities and extend this idea to include a larger class of high-resolution shock-capturing schemes. A more efficient variant of the form best suited for multidimensional steady-state computations will be discussed. The second objective is to extend the Cockburn–Shu fourth-order TVDM scheme to include a larger class of explicit and implicit high-resolution schemes. A modification of their idea and the use of different numerical fluxes are proposed to minimize the spurious oscillations due to the TVDM operator. The third objective is to analyze the relative advantages and disadvantages and the usage of these two families of schemes. The fourth objective is to combine the compact stencil with a variant of second-order Lax–Friedrichs numerical flux to increase efficiency (minimize operation counts) for combustion, thermal, and chemical nonequilibrium flow applications. This particular form can have the option of not requiring Riemann solvers for coupled nonlinear systems of equations. While slightly more diffusive than other numerical fluxes that require Riemann solvers, the cost saving is very noticeable. One remedy to compensate for the slight degradation in resolution is to use a less diffusive flux limiter, the artificial compression method [10], and/or grid clustering and grid adaptation at high gradient and shock regions.

Some of these proposed schemes can be fourth- or sixth-order accurate away from discontinuities. For the semidiscrete case their shock-capturing properties are of the TVD, total variation bounded (TVB), TVDM, essentially nonoscillatory (ENO), or positive type [11,12] for nonlinear 1D

scalar hyperbolic conservation laws and are positive schemes in more than one dimension. See Yee [13] and references cited therein for background on noncompact high-resolution shock-capturing schemes. These proposed schemes require a smaller grid stencil than their noncompact cousins. Both families of fourth- and sixth-order schemes require a grid stencil width of five points for TVD and positive types of schemes and seven points for ENO types of schemes in each spatial direction. On the other hand, typical grid stencils for noncompact second- and fourth-order high-resolution shock-capturing schemes are 5–7 and 9–11 points, respectively, in each spatial direction. The family of schemes based on Abarbanel and Kumar does not require the standard matrix inversion [14,15] and special numerical boundary treatment [1,16] associated with typical compact schemes. The added terms over the second-order noncompact cousins involves extra vector additions but no added flux evaluations. Due to the construction, both families of schemes can be viewed as approximations to genuinely multidimensional schemes in the sense that they might produce less distortion in spherical type shocks and are more accurate in vortex type flows than schemes based purely on 1D extensions. The degree of distortion and resolution in spherical type shocks depends also on the choice of flux limiters and the numerical flux construction.

For more than one dimension, the added work over the noncompact second or third-order counterparts only involves extra vector additions in each spatial direction. No additional Riemann solver or additional flux limiter computations over the second- or third-order noncompact counterparts are involved. Most of the proposed explicit TVDM compact forms require a 5×5 tridiagonal matrix inversion over their noncompact counterparts in 2D. The effort to modify existing high-resolution noncompact shock-capturing computer codes to have the compact form for both families is minimal. The present modification to Cockburn and Shu's TVDM form produces better shock resolution than their Lax–Friedrichs splitting variant. One advantage of the TVDM version is that a spatially and temporally fourth-order compact form for both time-accurate and time-marching approaches can be readily obtained as opposed to the inability to extend the Abarbanel and Kumar modification in a similar manner for time-accurate computations.

The majority of the proposed implicit schemes are especially suited for time-marching approaches to steady-state numerical solutions, since higher-order spatial accuracy can be achieved with minimal effort and the steady states are independent of the time step. If the delta formulation [17,18] is used, the minor modification to existing second-order noncompact high-resolution shock-capturing schemes involves only the explicit operator. The proper choice of time discretizations for the proposed two families of schemes for wave propagation and computational aeroacoustic type of applications has not been addressed. Thus,

the time discretizations discussed in this paper might not be optimized for the particular types of flows in the sense of wave resolution and phase error discussed in [19, 2–4] and the Workshop on Aeroacoustics [20]. This topic is a subject of ongoing research.

This is the first of a two part series of papers under the same topic. This part is devoted to the formulation and the second part is devoted to numerical results for fluid dynamics applications. Section II reviews the Abarbanel–Kumar scheme and the author’s modification of their scheme. Section III describes the extension of their scheme to high resolution at shocks and contact discontinuities. It includes the formulation with forcing or nonlinear source terms. It also includes the construction of a spatially sixth-order schemes without increasing the grid stencil width over the fourth-order form. Extension of these schemes to viscous flows is also discussed. Section IV extends the Cockburn–Shu compact scheme to a larger family of schemes and extends the scalar schemes to the multidimensional Euler equations using the various Riemann solvers. An efficient yet compatible high-resolution shock-capturing filter for these compact schemes is also discussed. A major portion of the material was published, not including the sixth-order formulations, as an internal NASA TM-110364, August 1995 [21].

II. COMPACT SCHEMES FOR THE 3-D EULER EQUATIONS

In vector notation, the 3D compressible time-dependent Euler equations in conservation form for an equilibrium real gas can be written as

$$U_t + F_x + G_y + H_z = S, \quad (2.1a)$$

where $U_t = \partial U / \partial t$, $F_x = \partial F / \partial x$, $G_y = \partial G / \partial y$, and $H_z = \partial H / \partial z$ with the U , F , G , and H vectors given by

$$U = \begin{bmatrix} \rho \\ \rho u \\ \rho v \\ \rho w \\ e \end{bmatrix}; \quad F = \begin{bmatrix} \rho u \\ \rho u^2 + p \\ \rho uv \\ \rho uw \\ eu + pu \end{bmatrix}; \quad (2.1b)$$

$$G = \begin{bmatrix} \rho v \\ \rho uv \\ \rho v^2 + p \\ \rho vw \\ ev + pv \end{bmatrix}; \quad H = \begin{bmatrix} \rho w \\ \rho uw \\ \rho vw \\ \rho w^2 + p \\ ew + pw \end{bmatrix}.$$

The vector $S = S(x, y, z, t)$ can be the forcing or source term

depending on the problem. The dependent variable U is the vector of conservative variables, and $(\rho, u, v, w, p)^T$ is the vector of primitive variables. Here ρ is the density, u, v , and w are the velocity components, $\rho u, \rho v$, and ρw are the x -, y - and z -components of the momentum per unit volume, p is the pressure, $e = \rho[\varepsilon + (u^2 + v^2 + w^2)/2]$ is the total energy per unit volume, and ε is the specific internal energy.

For a thermally perfect gas, the equation of state is

$$p = \rho RT, \quad (2.2)$$

where R is the specific gas constant and T is the temperature with $\varepsilon = \varepsilon(T)$. For constant specific heats (calorically perfect gas)

$$\varepsilon = c_v T, \quad (2.3)$$

where c_v is the specific heat at constant volume.

The above flow equations are restricted to non-chemically reacting gases. If reacting gases were to be included, the species continuity equations involving mass transport of chemical species i due to a concentration gradient in the species should be added. Thus, the scalar density function ρ becomes a vector of species mass density and the corresponding F, G, H , and S are also more complicated leading to the increase of the vector length of U, F, G, H , and S . See Anderson [22] and Park [23] for more detail. Although the discussion is restricted to nonreacting flows, the form of the schemes remains the same for reacting flows. Efficient implementation of these schemes similar to the noncompact TVD type of schemes to reacting flows can follow the same procedure as in Yee and Shinn [24] and Yee [13]. Difficulty in avoiding the wrong speed of propagation with discontinuous data associated with the stiff source term remains to be addressed. See [25–32] for discussion of this subject. Note that for equilibrium real gas and nonequilibrium flows, the form of the Riemann solvers and flux–vector splittings are different from the perfect gas counterparts. See [13] and references cited therein for these formulae.

2.1. Background

As discussed in the introduction, there exists many compact schemes in the literature. Here a compact scheme that does not require the matrix inversion associated with the standard compact scheme is addressed. The fourth-order in space and second-order in time Abarbanel–Kumar compact scheme for (2.1) with $S = 0$ takes the form

$$U_{j,k,l}^{n+1} + \theta[\lambda^x \mathcal{D}_x F^{n+1} + \lambda^y \mathcal{D}_y G^{n+1} + \lambda^z \mathcal{D}_z H^{n+1}] \\ + \mathcal{D}_{0xyz} U_{j,k,l}^{n+1} = U_{j,k,l}^n \\ - (1 - \theta)[\lambda^x \mathcal{D}_x F^n + \lambda^y \mathcal{D}_y G^n + \lambda^z \mathcal{D}_z H^n] \\ + [\mathcal{D}_{0xyz} U_{j,k,l}^n - \lambda^x \mathcal{D}_{0yz} D_x F^n \\ - \lambda^y \mathcal{D}_{0xz} D_y G^n - \lambda^z \mathcal{D}_{0xy} D_z H^n], \quad (2.4a)$$

where $\lambda^x = \Delta t/\Delta x$, $\lambda^y = \Delta t/\Delta y$, $\lambda^z = \Delta t/\Delta z$, and

$$\mathcal{D}_x F = \frac{1}{2}[F_{j+1,k,l} - F_{j-1,k,l}], \quad (2.4b)$$

$$\mathcal{D}_y G = \frac{1}{2}[G_{j,k,l+1} - G_{j,k,l-1}], \quad (2.4c)$$

$$\mathcal{D}_z H = \frac{1}{2}[H_{j,k,l+1} - H_{j,k,l-1}], \quad (2.4d)$$

$$\mathcal{D}_{0xyz} = \frac{1}{6}[\mathcal{D}_{0x} + \mathcal{D}_{0y} + \mathcal{D}_{0z}], \quad (2.4e)$$

$$\mathcal{D}_{0yz} = \frac{1}{6}[\mathcal{D}_{0y} + \mathcal{D}_{0z}], \quad (2.4f)$$

$$\mathcal{D}_{0xz} = \frac{1}{6}[\mathcal{D}_{0x} + \mathcal{D}_{0z}], \quad (2.4g)$$

$$\mathcal{D}_{0xy} = \frac{1}{6}[\mathcal{D}_{0x} + \mathcal{D}_{0y}], \quad (2.4h)$$

$$\mathcal{D}_{0x}(U_{j,k,l}) = U_{j+1,k,l} - 2U_{j,k,l} + U_{j-1,k,l}, \quad (2.4i)$$

$$\mathcal{D}_{0y}(U_{j,k,l}) = U_{j,k,l+1} - 2U_{j,k,l} + U_{j,k,l-1}, \quad (2.4j)$$

$$\mathcal{D}_{0z}(U_{j,k,l}) = U_{j,k,l+1} - 2U_{j,k,l} + U_{j,k,l-1}, \quad (2.4k)$$

and e.g.,

$$\mathcal{D}_{0y}(F_{j+1,k,l}) = F_{j+1,k+1,l} - 2F_{j+1,k,l} + F_{j+1,k-1,l}, \quad (2.4l)$$

where $U_{j,k,l}$ is the discrete approximation of U at $(j \Delta x, k \Delta y, l \Delta z, n \Delta t)$ and $\theta = \frac{1}{2}$. In (2.4a,b,c,d), the subscript (j, k, l) has been dropped from the fluxes F , G , and H to simplify the notation (i.e., $\mathcal{D}_x F$ means $\mathcal{D}_x(F_{j,k,l})$). To avoid complicated super and subscript notation, the standard numerical analysis notations $\mathcal{D}_0^x$ and $\mathcal{D}_+^x \mathcal{D}_-^x$ used to denote the three-point central difference approximation of $(\cdot)_{xx}$ and $(\cdot)_{xy}$ are not employed.

The time differencing in (2.4) is the second-order trapezoidal formula. The extra terms that contribute to the spatially fourth-order compact scheme are the last term on the left- and right-hand side of equation (2.4a). Without these two terms, the implicit scheme is the classical non-compact second-order central difference scheme, i.e.,

$$\begin{aligned} U_{j,k,l}^{n+1} + \theta[\lambda^x \mathcal{D}_x F^{n+1} + \lambda^y \mathcal{D}_y G^{n+1} + \lambda^z \mathcal{D}_z H^{n+1}] \\ = U_{j,k,l}^n - (1 - \theta)[\lambda^x \mathcal{D}_x F^n + \lambda^y \mathcal{D}_y G^n + \lambda^z \mathcal{D}_z H^n]. \end{aligned} \quad (2.5)$$

Note that in their original paper, Abarbanel and Kumar allow $\theta = 1$ but their formulation is valid only for $\theta = \frac{1}{2}$. See Section 2.2 for additional discussion and for a larger family of implicit schemes for steady-state computations. To obtain the spatially fourth-order compact differencing, Abarbanel and Kumar started with (2.5) with $\theta = 0$ (the forward Euler time discretization) and three-point central difference for the convection terms. They then took a Taylor series expansion about $(x, y, z, t) = (j \Delta x, k \Delta y, l \Delta z, n \Delta t)$ and obtained a modified equation of the form

$$\begin{aligned} U_t + \frac{\Delta t}{2} U_{tt} + \cdots = - \left[F_x + \frac{\Delta x^2}{3!} F_{xxx} + \cdots \right] \\ - \left[G_y + \frac{\Delta y^2}{3!} G_{yyy} + \cdots \right] \\ - \left[H_z + \frac{\Delta z^2}{3!} H_{zzz} + \cdots \right], \end{aligned} \quad (2.6)$$

or

$$\begin{aligned} U_t + F_x + G_y + H_z = - \left[\frac{\Delta t}{2} U_{tt} + \frac{\Delta x^2}{3!} F_{xxx} \right. \\ \left. + \frac{\Delta y^2}{3!} G_{yyy} + \frac{\Delta z^2}{3!} H_{zzz} \right] + \cdots. \end{aligned} \quad (2.7)$$

To obtain a fourth-order spatial differencing, they modified (2.5) with $\theta = 0$ by subtracting out the square bracket term on the right-hand side of (2.7) and used (2.1) to obtain

$$F_{xxx} = -U_{txx} - G_{yxx} - H_{zxx}, \quad (2.8a)$$

$$G_{yyy} = -U_{tyy} - F_{xyy} - H_{zyy}, \quad (2.8b)$$

$$H_{zzz} = -U_{tzz} - F_{xzz} - G_{yzz}, \quad (2.8c)$$

$$U_{tt} = \frac{\partial}{\partial t} [-F_x - G_y - H_z]. \quad (2.8d)$$

The terms F_{xxx} , G_{yyy} and H_{zzz} need only be approximated to second-order due to their coefficients $\Delta x^2/3!$, $\Delta y^2/3!$, and $\Delta z^2/3!$ (see Eq. (2.7)). Abarbanel and Kumar approximate (2.8) at $(j \Delta x, k \Delta y, l \Delta z, n \Delta t)$ by

$$\begin{aligned} (F_{xxx})_{j,k,l} \approx \frac{1}{\Delta x^2} \left\{ -\frac{\partial}{\partial t} \mathcal{D}_{0x}(U_{j,k,l}) \right. \\ \left. - \mathcal{D}_{0x} \left[\frac{G_{j,k,l+1} - G_{j,k,l-1}}{2 \Delta y} + \frac{H_{j,k,l+1} - H_{j,k,l-1}}{2 \Delta z} \right] \right\}, \end{aligned} \quad (2.9a)$$

$$\begin{aligned} (G_{yyy})_{j,k,l} \approx \frac{1}{\Delta y^2} \left\{ -\frac{\partial}{\partial t} \mathcal{D}_{0y}(U_{j,k,l}) \right. \\ \left. - \mathcal{D}_{0y} \left[\frac{F_{j+1,k,l} - F_{j-1,k,l}}{2 \Delta x} + \frac{H_{j,k,l+1} - H_{j,k,l-1}}{2 \Delta z} \right] \right\}, \end{aligned} \quad (2.9b)$$

$$\begin{aligned} (H_{zzz})_{j,k,l} \approx \frac{1}{\Delta z^2} \left\{ -\frac{\partial}{\partial t} \mathcal{D}_{0z}(U_{j,k,l}) \right. \\ \left. - \mathcal{D}_{0z} \left[\frac{F_{j+1,k,l} - F_{j-1,k,l}}{2 \Delta x} + \frac{G_{j,k,l+1} - G_{j,k,l-1}}{2 \Delta y} \right] \right\}, \end{aligned} \quad (2.9c)$$

The resulting scheme is then spatially fourth-order. Following the idea of Beam and Warming [18] and assuming the homogeneous property of the Euler equations with $\Delta U_{j,k,l}^n = U_{j,k,l}^{n+1} - U_{j,k,l}^n$, one can obtain an ADI delta formulation

$$\begin{aligned} & \left[I + \frac{1}{6} \mathcal{D}_{0x} + \theta \Delta t \frac{\partial}{\partial x} A^n \right] \left[I + \frac{1}{6} \mathcal{D}_{0y} + \theta \Delta t \frac{\partial}{\partial y} B^n \right] \\ & \times \left[I + \frac{1}{6} \mathcal{D}_{0z} + \theta \Delta t \frac{\partial}{\partial z} C^n \right] \Delta U_{j,k,l}^n \quad (2.10) \\ & = -\lambda^x (I + \mathcal{D}_{0yx}) \mathcal{D}_x F^n - \lambda^y (I + \mathcal{D}_{0xz}) \mathcal{D}_y G^n \\ & \quad - \lambda^z (I + \mathcal{D}_{0xy}) \mathcal{D}_z H^n. \end{aligned}$$

One can approximate $(\partial/\partial x)(A)$, $(\partial/\partial y)(B)$, and $(\partial/\partial z)(C)$ using the same three-point central differencing. Due to the delta formulation, for steady-state computations one can drop the $\frac{1}{6}\mathcal{D}_{0x}$, $\frac{1}{6}\mathcal{D}_{0y}$ and $\frac{1}{6}\mathcal{D}_{0z}$ terms. See the next section for a different way of deriving the similar form with a wider family of implicit schemes. One can also difference $(\partial/\partial x)(A)$, $(\partial/\partial y)(B)$, and $(\partial/\partial z)(C)$ by a first-order upwind differencing, e.g., the first-order conservative or nonconservative linearized implicit operator developed by the author [33] or the first-order flux vector splitting of Steger and Warming [34] and van Leer [35].

2.2. A Modification to the Abarbanel–Kumar Implicit Scheme for Steady-State Computations

The implicit scheme (2.4) or (2.10) can be used for time-accurate as well as steady-state computations. For time-accurate computations, the scheme ($\theta = \frac{1}{2}$) is temporally second order. Observe that the terms

$$\frac{1}{6}[\mathcal{D}_{0x} + \mathcal{D}_{0y} + \mathcal{D}_{0z}]U_{j,k,l} \quad (2.11)$$

appearing in the explicit side of (2.4a) can be interpreted as added second-order numerical dissipation to the over all scheme. For time-accurate calculations (2.11) might have some effect on the smearing of shock waves depending on the procedure in solving the resulting nonlinear systems of algebraic difference equations. After a steady state is reached, these added second-order numerical dissipation vanish. This fact becomes more apparent by examining the delta formulation (2.10). The inherent property of (2.4a) and (2.10) carries over to the high-resolution modification to be discussed in Section III. The reason is that, unlike the classical way of supplying a linear numerical dissipation, the design principle of high-resolution shock-capturing methods is constructed to automatically supply the appropriate dissipation from one grid point to the next. Any additional terms like (2.11) would further smear the shock wave. Therefore, (2.4) or (2.10) supply less numerical

dissipation for time-marching to steady states than time-accurate calculations. In addition, (2.11) contributes added computation and might degrade the diagonal dominant properties of the implicit operator (if first-order upwind differencing were used in (2.10) or other relaxation methods). To overcome the undesirable property of (2.4) for steady-state applications, we start with the semi-discrete form and Taylor series expand the three-point central spatial differencing about $(j \Delta x, k \Delta y, l \Delta z)$. Instead of (2.8), the steady part of (2.1) is used to approximate F_{xxx} , G_{yyy} , and H_{zzz} ; i.e., replace (2.8) with

$$F_{xxx} = -G_{yxx} - H_{zxx}, \quad (2.12a)$$

$$G_{yyy} = -F_{xyy} - H_{zyy}, \quad (2.12b)$$

$$H_{zzz} = -F_{xzz} - G_{yzz}, \quad (2.12c)$$

and (2.9) with

$$(F_{xxx})_{j,k,l} \approx -\mathcal{D}_{0x} \left[\frac{G_{j,k+1,l} - G_{j,k-1,l}}{2 \Delta y} + \frac{H_{j,k,l+1} - H_{j,k,l-1}}{2 \Delta z} \right] / \Delta x^2, \quad (2.13a)$$

$$(G_{yyy})_{j,k,l} \approx -\mathcal{D}_{0y} \left[\frac{F_{j+1,k,l} - F_{j-1,k,l}}{2 \Delta x} + \frac{H_{j,k,l+1} - H_{j,k,l-1}}{2 \Delta z} \right] / \Delta y^2, \quad (2.13b)$$

$$(H_{zzz})_{j,k,l} \approx -\mathcal{D}_{0z} \left[\frac{F_{j+1,k,l} - F_{j-1,k,l}}{2 \Delta x} + \frac{G_{j,k+1,l} - G_{j,k-1,l}}{2 \Delta y} \right] / \Delta z^2. \quad (2.13c)$$

Applying a two-parameter family of explicit and implicit time discretizations to the resulting semidiscrete form using (2.13) yields

$$\begin{aligned} & U_{j,k,l}^{n+1} + \frac{\theta}{1+\omega} [\lambda^x (I + \mathcal{D}_{0yz}) \mathcal{D}_x F^{n+1} + \lambda^y (I + \mathcal{D}_{0xz}) \mathcal{D}_y G^{n+1} \\ & \quad + \lambda^z (I + \mathcal{D}_{0xy}) \mathcal{D}_z H^{n+1}] = U_{j,k,l}^n \\ & \quad - \frac{1-\theta}{1+\omega} [\lambda^x (I + \mathcal{D}_{0yz}) \mathcal{D}_x F^n \\ & \quad + \lambda^y (I + \mathcal{D}_{0xz}) \mathcal{D}_y G^n + \lambda^z (I + \mathcal{D}_{0xy}) \mathcal{D}_z H^n] \\ & \quad + \frac{\omega}{1+\omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}]. \end{aligned} \quad (2.14a)$$

Here $0 \leq \theta \leq 1$. The scheme is temporally second-order if $\theta = \omega + \frac{1}{2}$, third-order if $\omega = 2\theta - \frac{5}{6}$ and first-order otherwise. When $\theta \neq 0$, the method is implicit. When $\omega = 0$, it recovers the one-parameter family case. That is, this two-parameter family includes the first-order implicit Euler ($\theta = 1, \omega = 0$), the second-order three-point backward differentiation ($\theta = 1, \omega = \frac{1}{2}$), and third-order implicit ($\theta =$

$\frac{1}{3}$, $\omega = -\frac{1}{6}$) methods. Additional higher-order implicit discretizations can be achieved using a three-parameter family of linear multistep methods. See [36, 37] for the formula. Various iterative, preconditioning and/or relaxation methods [38, 39] can be used to solve (2.14a) for steady-state computations. Note that unless $S \neq 0$ in (2.1), one cannot achieve the compact property for (2.14a) in 1D because the 1D form collapses to the standard second-order case.

The analog of (2.10) for the delta formulation of (2.14a) can be readily obtained. For steady-state applications, the terms $\frac{1}{6}(\mathcal{D}_{0y} + \mathcal{D}_{0z})$, $\frac{1}{6}(\mathcal{D}_{0x} + \mathcal{D}_{0z})$, and $\frac{1}{6}(\mathcal{D}_{0x} + \mathcal{D}_{0y})$ on the implicit left-hand side can be dropped. For the delta formulation, it yields

$$\begin{aligned} & \left[I + \frac{\theta \Delta t}{1 + \omega} \frac{\partial}{\partial x} A^n \right] \left[I + \frac{\theta \Delta t}{1 + \omega} \frac{\partial}{\partial y} B^n \right] \\ & \quad \times \left[I + \frac{\theta \Delta t}{1 + \omega} \frac{\partial}{\partial z} C^n \right] \Delta U_{j,k,l}^n \\ & = -\frac{1}{1 + \omega} [\lambda^x (I + \mathcal{D}_{0yz}) \mathcal{D}_x F^n \\ & \quad + \lambda^y (I + \mathcal{D}_{0xz}) \mathcal{D}_y G^n + \lambda^z (I + \mathcal{D}_{0xy}) \mathcal{D}_z H^n] \\ & \quad + \frac{\omega}{1 + \omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}]. \end{aligned} \quad (2.14b)$$

Again, for steady-state computations, one can difference $(\partial/\partial x)(A)$, $(\partial/\partial y)(B)$, and $(\partial/\partial z)(C)$ by first-order upwind differencing as discussed before.

Although scheme (2.14a) can be used for time-accurate computations, the spatial accuracy is no longer fourth-order. In this case, it appears that (2.14a) has an added advantage over the noncompact cousin (2.5). The extra cross derivative terms $\frac{1}{6}(\mathcal{D}_{0y} + \mathcal{D}_{0z}) \mathcal{D}_x F$, $\frac{1}{6}(\mathcal{D}_{0x} + \mathcal{D}_{0z}) \mathcal{D}_y G$, and $\frac{1}{6}(\mathcal{D}_{0x} + \mathcal{D}_{0y}) \mathcal{D}_z H$ can be viewed as approximations to genuinely multidimensional schemes. See Section 3.5 for some discussion.

Using the one-leg formulation of Dahlquist [40], an alternative to (2.14a), (2.14b) is

$$\begin{aligned} U_{j,k,l}^{n+1} & = U_{j,k,l}^n - \lambda^x (I + \mathcal{D}_{0yz}) \mathcal{D}_x F(\hat{U}_{j,k,l}) \\ & \quad - \lambda^y (I + \mathcal{D}_{0xz}) \mathcal{D}_y G(\hat{U}_{j,k,l}) \\ & \quad - \lambda^z (I + \mathcal{D}_{0xy}) \mathcal{D}_z H(\hat{U}_{j,k,l}) \\ & \quad + \frac{\omega}{1 + \omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}], \end{aligned} \quad (2.14c)$$

with $\hat{U} = (1 - \theta)/(1 + \omega)U^n + [\theta/(1 + \omega)]U^{n+1}$. For $\theta = \frac{1}{2}$ and $\omega = 0$, this one-leg formula is the well-known midpoint implicit method. Note that the noniterative linearized form (Beam and Warming [18], Yee and Sweby [30]) of the midpoint implicit formula reduces to the regular noniterative linearized trapezoidal formula. Also, there is no one-

leg version of the backward Euler method since (2.14c) reduces to (2.14a) for $\theta = 1$ and $\omega = 0$. Again, other higher than second-order implicit counterparts of (2.14a), (2.14b) and the one-leg formulations can also be obtained in a similar manner but the resulting scheme might involve more than three time levels. See Warming and Beam [41] for a discussion.

Iterative and/or relaxation procedures can be used to solve (2.14a) and (2.14c). If iterative relaxation procedures are used to solve (2.14), (2.14c) requires fewer flux evaluations and flux additions than (2.14a) for $\theta \neq 0$, $\theta \neq 1$, and $\omega \neq 0$. In this case, the linearized Jacobian of the fluxes at the “ n ” time-level for Newton-type iterative procedures can be used.

2.3. Compact Explicit Schemes for Steady-State Computations

One of the easiest procedures for obtaining higher than second-order time discretizations for multidimensional problems is the Runge–Kutta method. There are many variants of the Runge–Kutta method in the literature. See [37, 42] for details. The standard fourth-order Runge–Kutta takes the form

$$\begin{aligned} k_1 & = R^\circ(U^n) \\ k_2 & = R^\circ(U^n + \Delta t k_1/2) \\ k_3 & = R^\circ(U^n + \Delta t k_2/2) \\ k_4 & = R^\circ(U^n + \Delta t k_3) \end{aligned} \quad (2.15a)$$

$$U^{n+1} = U^n + \frac{\Delta t}{6} [k_1 + 2k_2 + 2k_3 + k_4].$$

Shu’s third-order Runge–Kutta (Shu [43]) form that is compatible with TVD, TVB, and ENO schemes takes the form

$$\begin{aligned} U^{(1)} & = U^n + \Delta t R^\circ(U^n) \\ U^{(2)} & = \frac{3}{4}U^n + \frac{1}{4}U^{(1)} + \frac{1}{4}\Delta t R^\circ(U^{(1)}) \\ U^{n+1} & = \frac{1}{3}U^n + \frac{2}{3}U^{(2)} + \frac{2}{3}\Delta t R^\circ(U^{(2)}). \end{aligned} \quad (2.15b)$$

The proper choice of time discretization that is compatible with a chosen spatial discretizations is crucial in achieving low phase and amplitude errors for time-accurate computations. This subject is ongoing research. Following the same form as (2.14a), a spatially fourth-order compact scheme can be obtained by defining R° as (dividing the square bracket of right-hand-side of (2.14a) by Δt and setting $\theta = 0$ and $\omega = 0$)

$$\begin{aligned} R^\circ & = -\frac{1}{\Delta x} [I + \mathcal{D}_{0yz}] \mathcal{D}_x F^n - \frac{1}{\Delta y} [I + \mathcal{D}_{0xz}] \mathcal{D}_y G^n \\ & \quad - \frac{1}{\Delta z} [I + \mathcal{D}_{0xy}] \mathcal{D}_z H^n. \end{aligned} \quad (2.15c)$$

Again, one can use (2.15) for time-accurate computations. The comments discussed in the paragraph above (2.14c) of Section 2.2 hold true for (2.15).

III. TWO-PARAMETER FAMILIES OF COMPACT HIGH-RESOLUTION SHOCK-CAPTURING SCHEMES

In the following discussion, wherever there is no confusion, the terms TVD, TVB, ENO or positive scheme are loosely used for schemes that are TVD, TVB, ENO or positive for (a) the fully discretized form, (b) the semidiscretized form, or (c) the frozen constant coefficient case. Note that all TVD, TVB, and ENO schemes are a subclass of positive schemes and all TVD schemes are a subclass of TVB and ENO schemes. Also when we use the terms TVD, TVB, or ENO, they mean the form has these types of properties for 1D scalar constant coefficient hyperbolic PDEs or nonlinear scalar conservative laws. It is remarked that regardless of the type of high-resolution method for 1-D, the final scheme for multidimensions is only of the positive type of scheme in the sense of [11, 12]. Strictly speaking, higher than first-order TVD-type schemes exist only for 1D scalar hyperbolic conservation laws and for 1D linear hyperbolic systems.

A careful examination of (2.4), (2.10), (2.14), or (2.15) reveals that spurious oscillations across discontinuities can be avoided if one replaces all of the three-point central differences of the fluxes (2.4b), (2.4c), (2.4d) by one of the spatially noncompact second-order high-resolution shock-capturing TVD, TVB, ENO, or positive-type schemes. Note that spatially higher than second-order high-resolution noncompact schemes can also be used but additional analysis is needed on the over all order of accuracy of the final scheme. In other words, redefine (2.4b), (2.4c), (2.4d) by

$$\mathcal{D}_x F = [\tilde{F}_{j+1/2,k,l} - \tilde{F}_{j-1/2,k,l}], \quad (3.1a)$$

$$\mathcal{D}_y G = [\tilde{G}_{j,k+1/2,l} - \tilde{G}_{j,k-1/2,l}], \quad (3.1b)$$

$$\mathcal{D}_z H = [\tilde{H}_{j,k,l+1/2} - \tilde{H}_{j,k,l-1/2}], \quad (3.1c)$$

where $\tilde{F}_{j\pm 1/2,k,l}$, $\tilde{G}_{j,k\pm 1/2,l}$, and $\tilde{H}_{j,k,l\pm 1/2}$ are the “good old” noncompact second-order numerical fluxes to be defined shortly. Most of these numerical fluxes can be viewed as a spatially three-point central differencing with a nonlinear numerical dissipation as described in Harten [44, 45], Yee and Harten [46], and Yee [47]. The majority of these numerical fluxes have a 5-point grid stencil in each spatial direction. The attractive property of these compact high-resolution shock-capturing schemes is that fourth-order accuracy can be achieved using the same grid stencil and numerical fluxes as their second-order noncompact cousins.

High-resolution time-accurate analog of (2.4a). Using (3.1), the high-resolution time-accurate analog of (2.4a) becomes

$$\begin{aligned} U_{j,k,l}^{n+1} &+ \theta \{ \lambda^x [\tilde{F}_{j+1/2,k,l}^{n+1} - \tilde{F}_{j-1/2,k,l}^{n+1}] \\ &+ \lambda^y [\tilde{G}_{j,k+1/2,l}^{n+1} - \tilde{G}_{j,k-1/2,l}^{n+1}] \\ &+ \lambda^z [\tilde{H}_{j,k,l+1/2}^{n+1} - \tilde{H}_{j,k,l-1/2}^{n+1}] \} + \mathcal{D}_{0xyz} U_{j,k,l}^{n+1} = U_{j,k,l}^n \\ &- \lambda^x [(1 - \theta)I + \mathcal{D}_{0yz}] [\tilde{F}_{j+1/2,k,l}^n - \tilde{F}_{j-1/2,k,l}^n] \\ &- \lambda^y [(1 - \theta)I + \mathcal{D}_{0xz}] [\tilde{G}_{j,k+1/2,l}^n - \tilde{G}_{j,k-1/2,l}^n] \\ &- \lambda^z [(1 - \theta)I + \mathcal{D}_{0xy}] [\tilde{H}_{j,k,l+1/2}^n - \tilde{H}_{j,k,l-1/2}^n] \\ &+ \mathcal{D}_{0xyz} U_{j,k,l}^n. \end{aligned} \quad (3.2a)$$

In symbolic notation

$$L_1 \cdot U^{n+1} = R_1 \cdot U^n. \quad (3.2b)$$

High-resolution analog of (2.14a) (Time-marching to steady-state form). For steady-state computations (see Section 2.2), one can drop the last term on the implicit and explicit sides of (3.2a). A two-parameter family analog of (2.14a) is

$$\begin{aligned} U_{j,k,l}^{n+1} &+ \frac{\theta}{1 + \omega} \{ \lambda^x (I + \mathcal{D}_{0yz}) [\tilde{F}_{j+1/2,k,l}^{n+1} - \tilde{F}_{j-1/2,k,l}^{n+1}] \\ &+ \lambda^y (I + \mathcal{D}_{0xz}) [\tilde{G}_{j,k+1/2,l}^{n+1} - \tilde{G}_{j,k-1/2,l}^{n+1}] \\ &+ \lambda^z (I + \mathcal{D}_{0xy}) [\tilde{H}_{j,k,l+1/2}^{n+1} - \tilde{H}_{j,k,l-1/2}^{n+1}] \} = U_{j,k,l}^n \\ &- \frac{1 - \theta}{1 + \omega} \{ \lambda^x (I + \mathcal{D}_{0yz}) [\tilde{F}_{j+1/2,k,l}^n - \tilde{F}_{j-1/2,k,l}^n] \\ &+ \lambda^y (I + \mathcal{D}_{0xz}) [\tilde{G}_{j,k+1/2,l}^n - \tilde{G}_{j,k-1/2,l}^n] \\ &+ \lambda^z (I + \mathcal{D}_{0xy}) [\tilde{H}_{j,k,l+1/2}^n - \tilde{H}_{j,k,l-1/2}^n] \} \\ &+ \frac{\omega}{1 + \omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}], \end{aligned} \quad (3.3a)$$

or in symbolic notation,

$$L_S \cdot U^{n+1} = R_S \cdot U^n + \frac{\omega}{1 + \omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}]. \quad (3.3b)$$

High-resolution analog of (2.14b), (2.14c), and (2.15). Similarly, one can obtain the corresponding high-resolution shock-capturing form of (2.14b), (2.14c), and (2.15) (i.e., with the appropriate numerical fluxes (3.1) instead of the three-point central differences of (2.4b)–(2.4d)).

Denote these high-resolution analogs of (2.14b), (2.14c), and (2.15) in symbolic notation respectively as

$$L_D \cdot \Delta U_{j,k,l}^{n+1} = R_D \cdot U^n + \frac{\omega}{1+\omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}], \quad (3.4)$$

$$U_{j,k,l}^{n+1} = R_o \cdot \hat{U} + \frac{\omega}{1+\omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}], \quad (3.5)$$

$$U_{j,k,l}^{n+1} = R_E \cdot U^n. \quad (3.6)$$

Here, L_D and R_D are the high-resolution analogs of the implicit and explicit operators for (2.14b), R_o is the analog of the one-leg operator for (2.14c), and R_E is the analog of the symbolic notation for the multistage Runge–Kutta method for (2.5). The vector $\hat{U}$ in (3.5) is the same as in (2.14c).

Again, for $\theta \neq 0$, $\theta \neq 1$, and $\omega \neq 0$ using iterative relaxation methods to solve the one-leg high-resolution formulation (3.5) requires fewer numerical flux evaluations and numerical flux additions than (3.3) and (3.4). Extensive numerical experimentation is needed to determine the relative convergence rate of (3.3), (3.4), and (3.5) for time-marching to the steady state.

High-resolution shock-capturing filter. For higher than two stages of Runge–Kutta or predictor–corrector time discretizations, evaluation of (3.1) at every stage is rather expensive. To avoid the added operations using (3.1) over (2.4a,b,c) one can apply (3.1) at the last stage of the Runge–Kutta method and the earlier stages using (2.4a,b,c). This is based on our successful experiences using this shock-capturing filter for spatially fourth- and sixth-order (a) noncompact central differences and (b) predictor–corrector MacCormack schemes [13]. Excellent shock-capturing properties for unsteady computations were obtained. Readers are referred to our forthcoming paper for details. An even less expensive filter step was proposed in [16].

3.1. Choices of Numerical Fluxes for the Fourth-Order Compact Schemes

Variants of the established form of the second- and third-order noncompact numerical fluxes $\tilde{F}_{j+1/2,k,l}$ that exhibit high-resolution shock-capturing capability have flooded the literature in the past six years. Most of these later noncompact numerical fluxes as well as the established ones are applicable for the proposed fourth-order compact scheme (3.1)–(3.6). Here, only a few of the established forms of the numerical fluxes are cited.

3.1.1. Harten–Yee–Roe–Davis Numerical Fluxes. For the Harten and Yee upwind TVD-type scheme and Yee–Roe–Davis symmetric TVD-type schemes, the numerical flux using the Roe’s approximate Riemann solver is of the form [46, 47]

$$\tilde{F}_{j+1/2,k,l} = \frac{1}{2} [F_{j+1,k,l} + F_{j,k,l} + R_{j+1/2} \Phi_{j+1/2}]. \quad (3.7)$$

Here $R_{j+1/2}$ is the right eigenvector matrix of $\partial F / \partial U$ using Roe’s approximate average state and $\Phi_{j+1/2}$ has several forms which are now discussed separately.

Second-order symmetric TVD scheme. The elements of the vector $\Phi_{j+1/2}$, denoted by $(\phi_{j+1/2}^l)^S$, for a general second-order symmetric TVD scheme are

$$(\phi_{j+1/2}^l)^S = -\psi(a_{j+1/2}^l) [\alpha_{j+1/2}^l - Q_{j+1/2}^l]. \quad (3.8a)$$

The value $a_{j+1/2}^l$ is the characteristic speed a^l , where $l = 1, 2, \dots, 5$, of $\partial F / \partial U$ evaluated at some symmetric average of $U_{j,k,l}$ and $U_{j+1,k,l}$. The function ψ is an entropy correction to $|a_{j+1/2}^l|$. One possible form is

$$\psi(a_{j+1/2}^l) = \begin{cases} |a_{j+1/2}^l|, & |a_{j+1/2}^l| \geq \delta_1, \\ [(a_{j+1/2}^l)^2 + \delta_1^2] / 2\delta_1, & |a_{j+1/2}^l| < \delta_1. \end{cases} \quad (3.8b)$$

α^l is the l th jump in the characteristic variable in the x -direction. For problems containing only unsteady shocks, δ_1 is usually set to zero. Note that entropy-violating phenomena occur only for steady or nearly steady shocks. For steady-state problems containing strong shock waves, a proper control of the size of δ_1 is very important, especially for hypersonic blunt-body flows. See [48] for a discussion. The ‘limiter’ function $Q_{j+1/2}^l$, expressed in terms of the jump in the characteristic variables, can be of the form

$$Q_{j+1/2}^l = \min\text{mod}(\alpha_{j-1/2}^l, \alpha_{j+1/2}^l) + \min\text{mod}(\alpha_{j+1/2}^l, \alpha_{j+3/2}^l) - \alpha_{j+1/2}^l, \quad (3.8c)$$

$$Q_{j+1/2}^l = \min\text{mod}(\alpha_{j-1/2}^l, \alpha_{j+1/2}^l, \alpha_{j+3/2}^l), \quad (3.8d)$$

$$Q_{j+1/2}^l = \min\text{mod}[2\alpha_{j-1/2}^l, 2\alpha_{j+1/2}^l, 2\alpha_{j+3/2}^l, \frac{1}{2}(\alpha_{j-1/2}^l + \alpha_{j+3/2}^l)]. \quad (3.8e)$$

The minmod function of a list of arguments is equal to the smallest number in absolute value if the list of arguments is of the same sign, or is equal to zero if any arguments are of opposite sign. See the subsection on choice of limiters for additional discussion.

Second-order upwind TVD scheme. The elements of the vector Φ_{j+1} denoted by $(\phi_{j+1/2}^l)^U$ for a second-order upwind TVD scheme, originally developed by Harten and later modified and generalized by Yee [47], are

$$(\phi_{j+1/2}^l)^U = \frac{1}{2} \psi(a_{j+1}^l) (g_{j+1}^l + g_j^l) - \psi(a_{j+1/2}^l + \gamma_{j+1/2}^l) \alpha_{j+1/2}^l, \quad (3.9a)$$

$$\gamma_{j+1/2}^l = \frac{1}{2} \psi(a_{j+1}^l) \begin{cases} (g_{j+1}^l - g_j^l) / \alpha_{j+1/2}^l, & \alpha_{j+1/2}^l \neq 0, \\ 0, & \alpha_{j+1/2}^l = 0. \end{cases} \quad (3.9b)$$

Examples of the commonly used “limiter” function g_j^l can be expressed as

$$g_j^l = \minmod(\alpha_{j-1/2}^l, \alpha_{j+1/2}^l), \quad (3.9c)$$

$$g_j^l = (\alpha_{j+1/2}^l \alpha_{j-1/2}^l + |\alpha_{j+1/2}^l \alpha_{j-1/2}^l|) / (\alpha_{j+1/2}^l + \alpha_{j-1/2}^l), \quad (3.9d)$$

$$g_j^l = \{\alpha_{j-1/2}^l [(\alpha_{j+1/2}^l)^2 + \delta_2] + \alpha_{j+1/2}^l [(\alpha_{j-1/2}^l)^2 + \delta_2]\} / [(\alpha_{j+1/2}^l)^2 + (\alpha_{j-1/2}^l)^2 + 2\delta_2], \quad (3.9e)$$

$$g_j^l = \minmod(2\alpha_{j-1/2}^l, 2\alpha_{j+1/2}^l, \frac{1}{2}(\alpha_{j+1/2}^l + \alpha_{j-1/2}^l)), \quad (3.9f)$$

$$g_j^l = S \cdot \max[0, \min(2|\alpha_{j+1/2}^l|, S \cdot \alpha_{j-1/2}^l), \min(|\alpha_{j+1/2}^l|, 2S \cdot \alpha_{j-1/2}^l)]; \quad S = \text{sgn}(\alpha_{j+1/2}^l). \quad (3.9g)$$

Here δ_2 is a small parameter to prevent division by zero and $\text{sgn}(\alpha_{j+1/2}^l) = \text{sign}(\alpha_{j+1/2}^l)$. In practical calculations $10^{-7} \leq \delta_2 \leq 10^{-5}$ is a commonly used range. For $\alpha_{j+1/2}^l + \alpha_{j-1/2}^l = 0$, g_j^l is set to zero in (3.9d).

Choice of limiter functions. Later development in limiters has flooded the literature and has created much debate. Most of the improvements are usually problem dependent. See [49–52] on the error propagation for nonlinear approximations to hyperbolic equations containing discontinuities in derivatives or discontinuous solutions. For the last six years of development in flux limiters, see articles which have appeared in the *Journal of Computational Physics* and related CFD Journals and conference proceedings. For high gradient and/or high frequency wave propagation with shock waves and aeroacoustics applications, suitable limiters, and the proper amount of limiting are essential to the overall accuracy of flow computations in addition to the comments above Section III. See Davis [6] for a possible limiter for this type of flow. The artificial compression method of Harten [10] can also be used to steepen the clipping effect due to standard TVD schemes. See Yee and Kutler [53] and Yee et al. [54] for examples. Extensive numerical experimentation is needed to determine the performance of these schemes and limiter combinations.

Shu [55, 56] showed procedures for modifying some existing TVD schemes such that the resulting schemes could be proven to be TVB and of globally higher-order accuracy in space, including extrema points. For example, by replacing the g_j^l function by g_j^M as discussed in Shu, the modified flux schemes can be made uniformly second-order accurate even at points of extrema. One of the forms suggested by Shu is

$$g_j^M = \frac{1}{2} \minmod(\alpha_{j+1/2}^l, \omega \alpha_{j-1/2}^l + M \Delta x^2 \text{sgn}(\alpha_{j+1/2}^l)) + \frac{1}{2} \minmod(\alpha_{j-1/2}^l, \omega \alpha_{j+1/2}^l + M \Delta x^2 \text{sgn}(\alpha_{j-1/2}^l)). \quad (3.10)$$

Here $1 \leq \omega \leq 3$ and $M \geq 0$. Shu suggests setting $M = 50$ for the Burgers’ equation computations. One can also use

the numerical flux of Osher and Chakravarthy [57] or Shu [43, 56] by using the appropriate flux limiter functions.

High-resolution TVD, TVB and ENO Lax–Friedrichs schemes. The corresponding high-resolution TVD Lax–Friedrichs schemes for system cases can be obtained by defining the ψ function to be $\psi(a_{j+1/2}^l) = a_{j+1/2}^{\max}$ for any of the $(\phi_{j+1/2}^l)^S$ or $(\phi_{j+1/2}^l)^U$. The value $a_{j+1/2}^{\max}$ can be $\beta(|u_{j+1/2}| + c_{j+1/2})$ with $0.5 \leq \beta \leq 1$, where u is the velocity in the x -direction and c is the sound speed. See Shu [43] for additional formulae. In addition by redefining the ψ , one can obtain a high-resolution TVB Lax–Friedrichs method by changing the limiter function to be the appropriate form as discussed above. Although using the Lax–Friedrichs numerical flux would introduce more numerical dissipation into the scheme, an entropy inequality is automatically satisfied with this numerical flux. Thus one does not have to deal with an arbitrary parameter δ_1 . In addition, at each grid point a savings of a (5×5) matrix–vector multiplication is realized in each direction.

High-Resolution ENO and positive schemes. If ENO (Harten and Osher [58]) and positive schemes other than the Lax–Friedrichs numerical flux discussed in the previous paragraph are desired, one can define the appropriate numerical flux according to the references cited earlier.

3.1.2. The MUSCL Approach

MUSCL approach using an approximate Riemann solver. The numerical flux function $\tilde{F}_{j+1/2,k,l}$ for an upwind MUSCL-type scheme as described in Yee [59,13] using the local-characteristic approach can be expressed as

$$\tilde{F}_{j+1/2,k,l} = \frac{1}{2}[F(U_{j+1/2}^R) + F(U_{j+1/2}^L) + R_{j+1/2}^\circ \Phi_{j+1/2}^l]. \quad (3.11a)$$

The elements of $\Phi_{j+1/2}^\circ$ and the vector $(\alpha^\circ)_{j+1/2}$ are given by

$$(\phi^\circ)_{j+1/2}^l = -\psi((a^\circ)_{j+1/2}^l)(\alpha^\circ)_{j+1/2}^l, \quad (3.11b)$$

$$(\alpha^\circ)_{j+1/2} = (R^\circ)_{j+1/2}^{-1}(U_{j+1/2}^R - U_{j+1/2}^L), \quad (3.11c)$$

where $\psi((a^\circ)_{j+1/2}^l)$ can be $|(\alpha^\circ)_{j+1/2}^l|$ or the same form as (3.8b). Here $(a^\circ)_{j+1/2}^l$ are the eigenvalues and $R_{j+1/2}^\circ$ is the eigenvector matrix of $\partial F / \partial U$ evaluated using a symmetric average between $U_{j+1/2}^R$ and $U_{j+1/2}^L$; i.e.,

$$(a^\circ)_{j+1/2}^l = a^l(U_{j+1/2}^R, U_{j+1/2}^L), \quad (3.11d)$$

$$R_{j+1/2}^\circ = R(U_{j+1/2}^R, U_{j+1/2}^L). \quad (3.11e)$$

However, there are options in applying the limiters for system cases. Namely, one can impose limiters on the conservative, primitive, or characteristic variables.

Various “slope” limiters can be used to eliminate un-

wanted oscillations. A popular one is the “minmod” limiter; it modifies the upwind-biased interpolation as

$$U_{j+1/2}^R = U_{j+1,k,l} - \frac{1}{4}[(1 - \bar{\eta})\widetilde{\Delta}_{j+3/2} + (1 + \bar{\eta})\widetilde{\Delta}_{j+1/2}], \quad (3.12a)$$

$$U_{j+1/2}^L = U_{j,k,l} + \frac{1}{4}[(1 - \bar{\eta})\widetilde{\Delta}_{j-1/2} + (1 + \bar{\eta})\widetilde{\Delta}_{j+1/2}], \quad (3.12b)$$

$$\widetilde{\Delta}_{j+1/2} = \text{minmod}(\Delta_{j+1/2}, \omega\Delta_{j-1/2}), \quad (3.12c)$$

$$\widetilde{\Delta}_{j+1/2} = \text{minmod}(\Delta_{j+1/2}, \omega\Delta_{j+3/2}), \quad (3.12d)$$

where

$$\Delta_{j+1/2} = U_{j+1,k,l} - U_{j,k,l} \quad (3.12e)$$

$$\text{minmod}(p, \omega q) = \text{sgn}(p) \cdot \max\{0, \min[|p|, \omega q \text{sgn}(p)]\} \quad (3.12f)$$

with $p = \Delta_{j+1/2}$ and $q = \Delta_{j-1/2}$ in Eq. (3.12c). Here the spatial order of accuracy (before the application of limiters) is determined by the value of $\bar{\eta}$,

$$\begin{aligned} \bar{\eta} &= -1, & \text{fully upwind scheme,} \\ \bar{\eta} &= 0, & \text{Fromm scheme,} \\ \bar{\eta} &= 1/3, & \text{third-order upwind-biased scheme,} \\ \bar{\eta} &= 1, & \text{three-point central-difference scheme,} \end{aligned}$$

and $1 \leq \omega \leq (3 - \bar{\eta})/(1 - \bar{\eta})$ with $\bar{\eta} \neq 1$.

One can improve the global order of accuracy (TVB) of the MUSCL scheme (3.11) by modifying $U_{j+1/2}^R$ and $U_{j+1/2}^L$ in Eq. (3.12) by

$$U_{j+1/2}^R = U_{j+1,k,l} - \frac{1}{4}[(1 - \bar{\eta})\widetilde{\Delta}_{j+3/2}^M + (1 + \bar{\eta})\widetilde{\Delta}_{j+1/2}^M], \quad (3.13a)$$

$$U_{j+1/2}^L = U_{j,k,l} + \frac{1}{4}[(1 - \bar{\eta})\widetilde{\Delta}_{j-1/2}^M + (1 + \bar{\eta})\widetilde{\Delta}_{j+1/2}^M], \quad (3.13b)$$

$$\widetilde{\Delta}_{j+1/2}^M = \text{minmod}(\Delta_{j+1/2}, \omega\Delta_{j-1/2} + M\Delta x^2 \text{sgn}(\Delta_{j+1/2})), \quad (3.13c)$$

$$\widetilde{\Delta}_{j+1/2}^M = \text{minmod}(\Delta_{j+1/2}, \omega\Delta_{j+3/2} + M\Delta x^2 \text{sgn}(\Delta_{j+1/2})), \quad (3.13d)$$

where

$$\text{minmod}(p, q) = \text{sgn}(p) \cdot \max\{0, \min[|p|, q \text{sgn}(p)]\}, \quad (3.13e)$$

with $p = \Delta_{j+1/2}$ and $q = \omega\Delta_{j-1/2} + M\Delta x^2 \text{sgn}(\Delta_{j+1/2})$ in Eq. (3.13c).

MUSCL approach using the Lax–Friedrichs numerical flux. The numerical flux function $\tilde{F}_{j+1/2,k,l}$ for a MUSCL-type approach using the Lax–Friedrichs numerical flux can be expressed as

$$\tilde{F}_{j+1/2,k,l} = \frac{1}{2}[F(U_{j+1/2}^R) + F(U_{j+1/2}^L) + \Phi_{j+1/2}^o], \quad (3.14a)$$

where $\Phi_{j+1/2}^o$ is

$$\Phi_{j+1/2}^o = -(a^o)_{j+1/2}^{\max}(U_{j+1/2}^R - U_{j+1/2}^L), \quad (3.14b)$$

and $(a^o)_{j+1/2}^{\max}$ can be

$$(a^o)_{j+1/2}^{\max} = \beta(|u_{j+1/2}^o| + c_{j+1/2}^o); 0.5 \leq \beta \leq 1. \quad (3.14c)$$

There is a tremendous savings in operation count (especially for multidimensional problems and/or nonequilibrium flows) in using the MUSCL–Lax–Friedrichs numerical flux instead of the Roe-type first-order upwind numerical flux when the limiter function is applied to the conservative or primitive variables instead of the characteristic variables. Note that one does not have a similar savings using the Lax–Friedrichs numerical flux for the non-MUSCL formulations. In problems containing contact discontinuities as well as shocks, one can use a more compressive limiter for the density and a less compressive limiter for the other variables. To compensate for the slightly more diffusive nature of these higher-order Lax–Friedrichs schemes, the artificial compression method of Harten [10] can be used. See Yee and Kutler [53] for an implementation and example.

MUSCL approach using flux–vector splittings. The numerical flux $\tilde{F}_{j+1/2,k,l}$ for either flux–vector splitting can be expressed as

$$\tilde{F}_{j+1/2,k,l} = F^+(U_{j+1/2}^L) + F^-(U_{j+1/2}^R), \quad (3.15)$$

where $F^\pm(U_{j+1/2}^{L,R})$ are evaluated using either the generalized Steger–Warming splitting, or the generalized van Leer splitting. The vectors $U_{j+1/2}^R$ and $U_{j+1/2}^L$ are the same as in equation (3.12). See Yee [13] and references cited therein.

3.2. Compact High-Resolution Schemes for Problems Containing Source Terms

When S in (2.1) is not zero and S is a function of U , x , y , and z , if one uses a pointwise evaluation of $S(U, x, y, z)$, i.e., $S(U, x, y, z) \approx S(U_{j,k,l}, j\Delta x, k\Delta y, l\Delta z)$, (2.7) becomes

$$\begin{aligned} U_t + F_x + G_y + H_z - S \\ = - \left[\frac{\Delta t}{2} U_{tt} + \frac{\Delta x^2}{3!} F_{xxx} + \frac{\Delta y^2}{3!} G_{yyy} + \frac{\Delta z^2}{3!} H_{zzz} \right] + \dots, \end{aligned} \quad (3.16)$$

and (2.8) becomes

$$F_{xxx} = S_{xx} - U_{txx} - G_{yxx} - H_{zxx} \quad (3.17a)$$

$$G_{yyy} = S_{yy} - U_{tyy} - F_{xyy} - H_{zyy} \quad (3.17b)$$

$$H_{zzz} = S_{zz} - U_{tzz} - F_{xzz} - G_{yzz} \quad (3.17c)$$

$$U_t = \frac{\partial}{\partial t} [S - F_x - G_y - H_z]. \quad (3.17d)$$

For the semidiscrete formulation for steady-state computations, one drops all the terms containing the t -derivatives. Thus the analogy for (3.2), (3.3), and (3.5) for problems containing source terms, respectively, are

$$L_1 \cdot U^{n+1} - \theta \Delta t S_{j,k,l}^{n+1} = R_1 \cdot U^n + \Delta t [(1 - \theta)I + \mathcal{D}_{0xyz}] S_{j,k,l}^n, \quad (3.18)$$

$$L_S \cdot U^{n+1} - \frac{\theta \Delta t}{1 + \omega} \mathcal{D}_{0xyz} S_{j,k,l}^{n+1} = R_S \cdot U^n + \frac{\omega}{1 + \omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}] + \frac{1 - \theta}{1 + \omega} \Delta t \mathcal{D}_{0xyz} S_{j,k,l}^n, \quad (3.19)$$

$$U_{j,k,l}^{n+1} = R_o \cdot \hat{U} + \frac{\omega}{1 + \omega} [U_{j,k,l}^n - U_{j,k,l}^{n-1}] + \frac{1 - \theta}{1 + \omega} \Delta t \mathcal{D}_{0xyz} \hat{S}_{j,k,l}. \quad (3.20)$$

The analogy for the delta formulation (3.4) and (3.6) can be obtained in a similar manner.

From the studies in [25, 27–29], pointwise evaluation might not be the optimal discretization for the source terms (in terms of stability and accuracy), depending on the method of discretizing the convection term. Readers are referred to these references for additional discussion.

3.3. TVD Property for the scalar 1-D case

For 1D, all the compact forms collapse to the standard second-order noncompact case unless $S \neq 0$ in (2.1a). For (3.2), the 1D version has two extra terms ($\frac{1}{6}\mathcal{D}_{0x}(u_j^{n+1})$ and $\frac{1}{6}\mathcal{D}_{0x}(u_j^n)$) over the standard second-order noncompact case. For the proof that (3.22) has the TVD or TVB property, see the original NASA TM (Yee [21]) for a discussion. For $\theta = 1$, the implicit method is unconditionally TVD and for $\theta = \frac{1}{2}$, the scheme is TVD if the CFL like condition is $\leq \frac{4}{3}$. The positive scheme definition for multidimensional systems can be found in Liu and Lax [12]. For the proof of whether a higher than first-order scheme in multidimensions satisfies the positivity property, see Einfeldt [11] and Liu and Lax [12].

3.4. Convection Dominating Viscous Flows

Formal extension of these high-resolution shock-capturing compact schemes to include viscous terms while main-

taining the same order of accuracy is quite involved and computationally expensive (Abarbanel [60]). For convection dominating viscous flows where the accuracy of the convection terms is more important, the easiest method for discretizing the viscous terms is the standard noncompact second- or fourth-order central differencing. Another alternative is to use the standard compact fourth-order method. Applying this to $\partial^2 V / \partial x^2$ yields

$$\frac{\partial^2 V}{\partial x^2} \approx \frac{1}{\Delta x^2} (C^{-1} D V)_j, \quad (3.21a)$$

where the C and D operators are defined by

$$(C V)_j = \frac{1}{12} V_{j+1} + \frac{5}{6} V_j + \frac{1}{12} V_{j-1}, \quad (3.21b)$$

$$(D V)_j = V_{j+1} - 2V_j + V_{j-1}. \quad (3.21c)$$

The final scheme using either the noncompact second- or fourth-order central differencing or (3.21) for the viscous terms is no longer fourth order. How this inconsistent way of discretizing the viscous terms affects the overall performance and accuracy of the convection dominating flows remain to be addressed.

3.5. Approximation to Multidimensional Schemes

The extra cross derivative terms $\frac{1}{6}(\mathcal{D}_{0y} + \mathcal{D}_{0z})\mathcal{D}_x F$, $\frac{1}{6}(\mathcal{D}_{0x} + \mathcal{D}_{0z})\mathcal{D}_y G$, and $\frac{1}{6}(\mathcal{D}_{0x} + \mathcal{D}_{0y})\mathcal{D}_z H$ appearing in all of the above fourth-order compact schemes using (2.4) or (3.1) for the $\mathcal{D}_x F$, $\mathcal{D}_y G$, and $\mathcal{D}_z H$ can be viewed as approximations to genuinely multidimensional schemes in the sense that multidimensional flux differences are involved. These forms can be interpreted as poor man's multidimensional shock-capturing schemes for structured grids without the complicated formulation as in Roe [61] and related work. In particular, these cross derivative terms involve four extra vector additions for 2D and 8 for 3D in each spatial direction over their second-order noncompact cousins. Since one computes the entire flux field before summing the flux differences, no added flux evaluations are needed. For example, the F flux differencing for 2D now involves $F_{j\pm 1/2, k\pm 1}$ and $F_{j\pm 1/2, k}$ for 2D, and $F_{j\pm 1/2, k\pm 1, l}$, $F_{j\pm 1/2, k, l\pm 1}$, and $F_{j\pm 1/2, k, l}$ for 3D. The partial involvement of the multidimensional nature of the fluxes are apparent. For the TVD type of schemes, the grid molecule of the fluxes are 5×3 point in 2D and $5 \times 3 \times 3$ in 3D as opposed to a five-point 1D line for the second-order noncompact case. Consequently, these terms would produce less distortion in spherical type shocks and are more accurate in vortex type flows than schemes based purely on 1D extensions. Of course, the degree of distortion also depends on the grid, the form of the numerical flux, and the flux limiters as well.

3.6. Spatially Sixth-Order Compact Schemes

To obtain a spatially sixth-order compact scheme, three additional terms involving F_{xxxxx} , G_{yyyyy} , and H_{zzzzz} need to be retained in (2.7). They have the form

$$- \left[\frac{\Delta x^4}{5!} F_{xxxxx} + \frac{\Delta y^4}{5!} G_{yyyyy} + \frac{\Delta z^4}{5!} H_{zzzzz} \right] \quad (3.22)$$

In other words we have to subtract (3.22) from the fourth-order schemes to achieve the sixth-order formulation. A crucial step to retain a narrow grid stencil for the sixth-order case is to approximate, e.g.,

$$(F_{xxxxx})_{j,k,l} \approx \frac{1}{\Delta x^2} [(F_{xxx})_{j+1,k,l} - 2(F_{xxx})_{j,k,l} + (F_{xxx})_{j-1,k,l}]. \quad (3.23)$$

Making use of the identity (2.8) for each of the $(j \pm 1, k, l)$ indices for F_{xxx} in (3.23), we have

$$\begin{aligned} (F_{xxxxx})_{j,k,l} \approx & -\frac{1}{\Delta x^4} \left\{ \left[\frac{\partial}{\partial t} \mathcal{D}_{0x}(U_{j+1,k,l}) \right. \right. \\ & + \mathcal{D}_{0x} \left(\frac{G_{j+1,k+1/2,l} - G_{j+1,k-1/2,l}}{\Delta y} \right. \\ & \left. \left. + \frac{H_{j+1,k,l+1/2} - H_{j+1,k,l-1/2}}{\Delta z} \right) \right] \\ & - 2 \left[\frac{\partial}{\partial t} \mathcal{D}_{0x}(U_{j,k,l}) + \mathcal{D}_{0x} \left(\frac{G_{j,k+1/2,l} - G_{j,k-1/2,l}}{\Delta y} \right. \right. \\ & \left. \left. + \frac{H_{j,k,l+1/2} - H_{j,k,l-1/2}}{\Delta z} \right) \right] + \left[\frac{\partial}{\partial t} \mathcal{D}_{0x}(U_{j-1,k,l}) \right. \\ & + \mathcal{D}_{0x} \left(\frac{G_{j-1,k+1/2,l} - G_{j-1,k-1/2,l}}{\Delta y} \right. \\ & \left. \left. + \frac{H_{j-1,k,l+1/2} - H_{j-1,k,l-1/2}}{\Delta z} \right) \right] \left. \right\}, \quad (3.24) \end{aligned}$$

where $\mathcal{D}_{0x}$ is the same as (2.4i). Similarly, the G_{yyyyy} and H_{zzzzz} can be approximated in the same manner. By examining the final sixth-order scheme (by subtracting (3.22) in (3.2)–(3.6)), one readily realizes that the width of the grid stencil for each spatial direction remains the same as the second-order noncompact scheme. The added terms involves an increase in the width of the grid stencil, e.g., in the y and z directions rather than the x direction for the F flux.

In other words, the flux differences for F now involve

$$\begin{aligned} & (j \pm \tfrac{1}{2}, k \pm 2, l), \quad (j \pm \tfrac{1}{2}, k \pm 1, l), \\ & (j \pm \tfrac{1}{2}, k, l), (j \pm \tfrac{1}{2}, k, l \pm 2), \\ & (j \pm \tfrac{1}{2}, k, l \pm 1). \end{aligned} \quad (3.25)$$

Consequently, instead of requiring an extra four vector additions for 2D and eight for 3D in each spatial direction over their second-order noncompact cousins for the fourth-order compact case, the number of extra vector additions for the sixth-order case is doubled. The extra vector additions are 8 for 2D and 16 for 3D in each spatial direction. For example, the F flux differencing for 2D now involves $F_{j \pm 1/2, k+2}$, $F_{j \pm 1/2, k-2}$, $F_{j \pm 1/2, k+1}$ and $F_{j \pm 1/2, k-1}$. The beauty of the sixth-order scheme is the **extreme compact nature of the stencil** and the **full involvement of the multidimensional nature** of the fluxes. For the TVD type of schemes, the grid molecule of the fluxes is the full 5×5 point square in 2D and $5 \times 5 \times 5$ point cubic in 3D. Note that the grid molecule of their second-order noncompact cousins is a five-point line.

Extension of the Abarbanel and Kumar compact scheme to sixth-order. Using the above formula, one can obtain a sixth-order variant of the Abarbanel and Kumar scheme by replacing (3.1) with (2.4b), (2.4c), (2.4d). However, the grid molecule now becomes 3×5 in 2D and $3 \times 5 \times 5$ in 3D. The compact nature is less pronounced than the high-resolution compact case since a grid molecule of 3×3 in 2D and $3 \times 3 \times 3$ in 3D cannot be maintained. In addition, the multidimensional nature of this form is somewhat inconsistent. The flux differences put more weight on the nondominating directions (e.g., the y and z directions for the F flux), instead of the dominating direction (e.g., the x direction for the F flux).

IV. COMPACT HIGH-RESOLUTION SHOCK-CAPTURING SCHEMES BASED ON TOTAL VARIATION DIMINISHING IN THE MEAN (TVDM)

Cockburn and Shu [9] proposed an explicit compact shock-capturing scheme based on the splitting of a Lax–Friedrichs flux and the idea of a total variation diminishing in the mean (TVDM). Here, we extend their idea to a family of explicit and implicit schemes with numerical fluxes similar to Section III, but using the TVDM idea. That is, the flux limiters are performed on a mean value of U involving a symmetric linear combination of adjacent grid points. However, even for scalar hyperbolic conservation laws, their TVDM idea does not completely suppress spurious oscillations across discontinuities due to the limiting of the local mean step. See their original paper for illustrations. The present straightforward extension of their

TVDM idea suffers a similar shortcoming. By applying part of their idea and performing flux limiters not on the local mean value of U but on U itself, a tremendous improvement in the shock resolution is realized. Another alternative in achieving the desired shock resolution is to evaluate the entire numerical flux function on the local mean value of U . The reason for presenting the schemes in 3D is to contrast these schemes with the ones proposed in Section III. Although the operation count for both families of methods are very close for problems that are lower than 3D, for 3D the TVDM version requires a larger operation count than the Abarbanel and Kumar extension. One advantage of the TVDM version is that a spatially and temporally fourth-order compact form for both time-accurate and time-marching approaches can be readily obtained as opposed to the inability to extend the Abarbanel and Kumar modification in a similar manner for time-accurate computations.

Assume the F_x , G_y , and H_z in (2.1) are approximated by some compact operator at $(j \Delta x, k \Delta y, l \Delta z)$,

$$F_x \approx \frac{1}{\Delta x} (A_x^{-1} B_x F)_{j,k,l}, \quad (4.1a)$$

$$G_y \approx \frac{1}{\Delta y} (A_y^{-1} B_y G)_{j,k,l}, \quad (4.1b)$$

$$H_z \approx \frac{1}{\Delta z} (A_z^{-1} B_z H)_{j,k,l}, \quad (4.1c)$$

where for a fourth-order approximation,

$$(A_x F)_{j,k,l} = \frac{1}{6} (F_{j+1,k,l} + 4F_{j,k,l} + F_{j-1,k,l}), \quad (4.2a)$$

$$(A_y G)_{j,k,l} = \frac{1}{6} (G_{j,k,l+1} + 4G_{j,k,l} + G_{j,k,l-1}), \quad (4.2b)$$

$$(A_z H)_{j,k,l} = \frac{1}{6} (H_{j,k,l+1} + 4H_{j,k,l} + H_{j,k,l-1}), \quad (4.2c)$$

$$(B_x F)_{j,k,l} = \frac{1}{2} (F_{j+1,k,l} - F_{j-1,k,l}), \quad (4.2d)$$

$$(B_y G)_{j,k,l} = \frac{1}{2} (G_{j,k,l+1} - G_{j,k,l-1}), \quad (4.2e)$$

$$(B_z H)_{j,k,l} = \frac{1}{2} (H_{j,k,l+1} - H_{j,k,l-1}). \quad (4.2f)$$

Similarly, one can define the corresponding third-order and sixth-order compact operators. Since one does not gain in operation count for third-order compact schemes over the noncompact cousins these forms are not discussed here. In Section 4.2, an approximate sixth-order compact scheme will be discussed.

4.1. Two-Parameter Families of Explicit and Implicit Compact Schemes

A one-parameter family of explicit and implicit compact schemes suitable for both time-accurate and time-marching approaches for (2.1) with $S = 0$ can be written

$$\begin{aligned} U_{j,k,l}^{n+1} + \theta [\lambda^x (A_x^{-1} B_x F)_{j,k,l}^{n+1} + \lambda^y (A_y^{-1} B_y G)_{j,k,l}^{n+1} \\ + \lambda^z (A_z^{-1} B_z H)_{j,k,l}^{n+1}] = U_{j,k,l}^n - (1 - \theta) [\lambda^x (A_x^{-1} B_x F)_{j,k,l}^n \\ + \lambda^y (A_y^{-1} B_y G)_{j,k,l}^n + \lambda^z (A_z^{-1} B_z H)_{j,k,l}^n]. \end{aligned} \quad (4.3)$$

Let

$$\bar{U}_{j,k,l} = (A_z A_y A_x U)_{j,k,l}. \quad (4.4)$$

Since A_x , A_y , and A_z commute, we can multiply the semi-discretized form of (4.3) by $A_x A_y A_z$ and (4.3) becomes

$$\begin{aligned} \bar{U}_{j,k,l}^{n+1} + \theta [\lambda^x (A_z A_y B_x F)_{j,k,l}^{n+1} + \lambda_y (A_z A_x B_y G)_{j,k,l}^{n+1} \\ + \lambda^z (A_x A_y B_z H)_{j,k,l}^{n+1}] = \bar{U}_{j,k,l}^n - (1 - \theta) [\lambda^x (A_z A_y B_x F)_{j,k,l}^n \\ + \lambda^y (A_z A_x B_y G)_{j,k,l}^n + \lambda^z (A_x A_y B_z H)_{j,k,l}^n]. \end{aligned} \quad (4.5a)$$

A two-parameter family of explicit and implicit counterparts of (4.5a) takes the form

$$\begin{aligned} \bar{U}_{j,k,l}^{n+1} + \frac{\theta}{1 + \omega} [\lambda^x (A_z A_y B_x F)_{j,k,l}^{n+1} + \lambda^y (A_z A_x B_y G)_{j,k,l}^{n+1} \\ + \lambda^z (A_x A_y B_z H)_{j,k,l}^{n+1}] = \bar{U}_{j,k,l}^n - \frac{1 - \theta}{1 + \omega} [\lambda^x (A_z A_y B_x F)_{j,k,l}^n \\ + \lambda^y (A_z A_x B_y G)_{j,k,l}^n + \lambda^z (A_x A_y B_z H)_{j,k,l}^n] \\ + \frac{\omega}{1 + \omega} [\bar{U}_{j,k,l}^n - \bar{U}_{j,k,l}^{n-1}]. \end{aligned} \quad (4.5b)$$

The one-leg formulation of Dahlquist for this case has the form

$$\begin{aligned} \bar{U}_{j,k,l}^{n+1} = \bar{U}_{j,k,l}^n - \lambda^x (A_z A_y B_x F)_{j,k,l}^{\wedge} - \lambda^y (A_z A_x B_y G)_{j,k,l}^{\wedge} \\ - \lambda^z (A_x A_y B_z H)_{j,k,l}^{\wedge} + \frac{\omega}{1 + \omega} [\bar{U}_{j,k,l}^n - \bar{U}_{j,k,l}^{n-1}]. \end{aligned} \quad (4.5c)$$

The symbol $(\wedge)$ here means the flux evaluations on the right-hand side of (4.5c) are evaluated using one of three ways: (1) evaluated at $\hat{U} = (1 - \theta)/(1 + \omega) U^n + \theta/(1 + \omega) U^{n+1}$, (2) evaluated partly at $\hat{U}$ and partly at $\bar{U} = (1 - \theta)/(1 + \omega) \bar{U}^n + \theta/(1 + \omega) \bar{U}^{n+1}$, and (3) evaluated at $\bar{U}$. More details on the various options will be discussed shortly. The advantage of (4.5c) over (4.5b), where iterative relaxation methods are used to solve the nonlinear algebraic equations as discussed in Sections II and III, carry over to the present formulation, especially for the 3D case. Again, higher than second-order implicit counterparts of (4.5b), (4.5c) can also be obtained in a similar manner but the resulting scheme involves more than three time levels.

For (4.5) (or (4.4)) to have a high-resolution shock-

capturing property, instead of using (4.2), the following is proposed:

$$(B_x F)_{j,k,l} = F_{j+1/2,k,l}^* - F_{j-1/2,k,l}^* \quad (4.6a)$$

$$(B_y G)_{j,k,l} = G_{j,k+1/2,l}^* - G_{j,k-1/2,l}^* \quad (4.6b)$$

$$(B_z H)_{j,k,l} = H_{j,k,l+1/2}^* - H_{j,k,l-1/2}^*. \quad (4.6c)$$

Without loss of generality, it is assumed that U means $\hat{U}$ for (4.5c) for the following three options of evaluating (4.6). In particular, when we say that the flux is evaluated at $\bar{U} = (A_z A_y A_x U)_{j,k,l}$, we actually mean that the flux is evaluated at $(A_z A_y A_x \hat{U})_{j,k,l}$ for (4.5c).

Option I. To achieve fourth-order spatial differencing, the first option is to evaluate $F_{j+1/2,k,l}^*$, $G_{j,k+1/2,l}^*$, and $H_{j,k,l+1/2}^*$ in exactly the same form and arguments as the $\bar{F}_{j+1/2,k,l}$, $\bar{G}_{j,k+1/2,l}$, and $\bar{H}_{j,k,l+1/2}$ in (3.7)–(3.15). This is the author's first proposed compact form to replace Cockburn and Shu's compact form. The terms in the round brackets on both sides of (4.5) are, e.g.,

$$\begin{aligned} (A_z A_y B_x F)_{j,k,l} &= \frac{1}{6} A_z [(F_{j+1/2,k+1,l}^* + 4F_{j+1/2,k,l}^* + F_{j+1/2,k-1,l}^*) \\ &\quad - (F_{j-1/2,k+1,l}^* + 4F_{j-1/2,k,l}^* + F_{j-1/2,k-1,l}^*)] \\ &= \text{etc.} \end{aligned} \quad (4.7)$$

For option I, $F_{j\pm 1/2,k\pm 1,l}^* = \bar{F}_{j\pm 1/2,k\pm 1,l}$ and $F_{j\pm 1/2,k,l}^* = \bar{F}_{j\pm 1/2,k,l}$ as in (3.7)–(3.15).

Expanding out the right-hand side of (4.7), one gets 18 terms of the numerical flux evaluations in 3D (in each direction) as opposed to six terms in 2D (in each direction) and two terms in 1D for each of the operators like (4.7) in Eq. (4.5). Comparing the operation count with the Abarbanel and Kumar extension, the TVDM version requires a lot more vector additions for the 3D case. In other words, the vector additions for the Abarbanel and Kumar extension increase linearly from 2D to 3D but not for the TVDM version. However, the variants of the fourth-order Runge–Kutta method of Cockburn and Shu are readily obtained for both time-accurate and time-marching approaches as opposed to the inability to extend the Abarbanel and Kumar extensions in a similar manner for a spatially and temporally fourth-order scheme for time-accurate computations.

The multidimensional nature of these schemes and the molecule of the grid stencil are similar as discussed in Section 3.5. This explicit scheme will be discussed in the next subsection. The viscous analog of (4.5) using the fourth-order form (3.21) is straightforward. However, the viscous part is rather expensive to compute. The discussion above applies to options II and III as well.

Option II. The second option is the straightforward

extension of Cockburn and Shu's idea. In this case, we define $F_{j+1/2,k,l}^*$, $G_{j,k+1/2,l}^*$, and $H_{j,k,l+1/2}^*$ to have the same form as (3.7)–(3.15) except e.g., all the $R_{j+1/2}$ and $\Phi_{j+1/2}$ are evaluated at $\bar{U}_{j-1,k,l}$, $\bar{U}_{j,k,l}$, $\bar{U}_{j+1,k,l}$, and $\bar{U}_{j+2,k,l}$. That is, e.g.,

$$F_{j+1/2,k,l}^* = \frac{1}{2} [F_{j+1,k,l} + F_{j,k,l} + \bar{R}_{j+1/2} \bar{\Phi}_{j+1/2}], \quad (4.8)$$

where $\bar{R}_{j+1/2}$ and $\bar{\Phi}_{j+1/2}$ are the same as in Section III but are evaluated at $\bar{U}$. For the corresponding MUSCL and flux vector splittings of (3.1), all the limiting is applied to $\bar{U}$.

Preliminary numerical experiments performed by Dr. George Huang of NASA Ames on the 1D scalar Burgers equation revealed that the straightforward extension of Cockburn and Shu's idea to the numerical fluxes proposed in Section III suffers a shortcoming similar to that of their original numerical flux. This TVDM idea does not completely suppress spurious oscillations across discontinuities. However, numerical experiments on option I indicate that spurious oscillations are minimized and a tremendous improvement in the shock resolution is realized.

Option III. The third option is to evaluate all of the terms in the round brackets on the implicit and explicit operators in (4.5) at $\bar{U}$. That is, e.g.,

$$F_{j+1/2,k,l}^* = \frac{1}{2} [\bar{F}_{j+1,k,l} + \bar{F}_{j,k,l} + \bar{R}_{j+1/2} \bar{\Phi}_{j+1/2}], \quad (4.9)$$

where $\bar{F}_{j+1,k,l}$, $\bar{F}_{j,k,l}$, $\bar{R}_{j+1/2}$, and $\bar{\Phi}_{j+1/2}$ are the same as in Section III but are evaluated at $\bar{U}$. For the corresponding MUSCL and flux-vector splitting of (3.1), all the dependent variables and limiting are applied to $\bar{U}$. Although the third option alters the original compact property of the scheme, preliminary numerical experiments show that shock resolution is similar or slightly better than option I and far better than option II. In addition, the standard matrix inversion associated with the standard compact scheme is not required for option III. In fact, the operation count for option III is comparable to the high-resolution case discussed in section III for 2D, but requires more operations for 3D computations. Note that Option III collapses to the non-compact case for 1D unless $S \neq 0$ in (2.1a). Although the exact spatial order of accuracy using option III needs further investigation, one apparent advantage of option III over their standard noncompact cousins is that this scheme can be viewed as an approximation to genuinely multidimensional schemes as discussed in Sections II and III.

Similar to Sections II and III, one can obtain the corresponding ADI delta form for (4.5). For steady-state computations, one can use the same simplified first-order spatial differencing for the implicit operator (implicit left-hand side) as discussed previously.

Temporally higher-order explicit TVDM compact schemes. Unlike the explicit higher-order compact schemes discussed in Section III, the schemes discussed here can retain fourth-order spatial and time accuracy for time-accurate and time-marching computations. The explicit scheme is the same as (2.15) except the three options in evaluating (4.6) should be applied to the proper arguments of each stage of the Runge–Kutta method for high-resolution shock-capturing capability. The R° counterpart of (2.15c) is

$$R^\circ = -\frac{1}{\Delta x} (A_y A_z B_x F)_{j,k,l}^n - \frac{1}{\Delta y} (A_x A_z B_y G)_{j,k,l}^n - \frac{1}{\Delta z} (A_x A_y B_z H)_{j,k,l}^n. \quad (4.10)$$

Alternatively, to save CPU, one can apply (A.6) at the last stage of the Runge–Kutta method and (4.2d,e,f) for the earlier stages of the Runge–Kutta procedure. To suppress the oscillations across discontinuities due to the TVDM step, one can apply the filter step on $U^{n+1/2}$ where $U^{n+1/2}$ is the solution of $U^{n+1/2} = A_z^{-1} A_y^{-1} A_x^{-1} U^{n+1}$ using the Runge–Kutta method. In this case, one can avoid the three options in applying the flux limiters.

Viscous flows. Formal extension of the TVDM-type compact schemes to include simple viscous terms is straightforward using the fourth-order compact operator such as (3.21). However, the grid stencil for the inclusion of viscous terms is rather expensive to compute due to the multiplication factor of the discretized viscous terms by the $A_x A_y A_z$ operator.

TVDM Property of (4.5) for 1D scalar case. In 1D with $\bar{u}_j = (A_x u)_j$, (4.5) becomes

$$\bar{u}_j^{n+1} + \lambda \theta (B_x f)_j^{n+1} = \bar{u}_j^n - \lambda (1 - \theta) (B_x f)_j^n. \quad (4.11)$$

Cockburn and Shu define the total variation of the mean $\bar{u}$ by

$$TV(\bar{u}^n) = \sum_{j=-\infty}^{\infty} |\bar{u}_{j+1}^n - \bar{u}_j^n|. \quad (4.12)$$

The explicit scheme that Cockburn and Shu considered is for $\theta = 0$ using the Lax–Friedrichs flux splitting. They showed that their explicit scheme satisfies the TVDM sufficient condition, i.e.,

$$TV(\bar{u}^{n+1}) \leq TV(\bar{u}^n), \quad (4.13)$$

under the CFL condition of $\frac{1}{2}$.

Using the same argument as in Section 3.3 of [21] one

can readily obtain either the positive or the TVDM property for (4.11) for the three options of evaluating $(B_x f)_j$.

4.2. A Spatially Sixth-Order Extension

The standard sixth-order compact approximation takes the form

$$(A_x F)_{j,k,l} = \frac{1}{6} [F_{j+1,k,l} + 3F_{j,k,l} + F_{j-1,k,l}] \quad (4.14a)$$

$$(B_x F)_{j,k,l} = \frac{1}{60} [F_{j+2,k,l} - F_{j-2,k,l}] + \frac{28}{60} [F_{j+1,k,l} - F_{j-1,k,l}] \\ = (B_x^1 F)_{j,k,l} + (B_x^2 F)_{j,k,l} \quad (4.14b)$$

with

$$(B_x^1 F)_{j,k,l} = \frac{1}{60} [F_{j+2,k,l} - F_{j-2,k,l}] \quad (4.14c)$$

$$(B_x^2 F)_{j,k,l} = \frac{28}{60} [F_{j+1,k,l} - F_{j-1,k,l}]. \quad (4.14d)$$

An approximation to modify (4.14) to have high-resolution shock-capturing property is to keep (4.14c) but replace (4.14d) by

$$(B_x^2 F)_{j,k,l} = \frac{28}{60} [F_{j+1/2,k,l}^\star - F_{j-1/2,k,l}^\star] \quad (4.15)$$

with the rest of the formulation as discussed above. By using (4.15), the sixth-order grid stencil is the same as the fourth-order high-resolution compact counterparts. The multidimensional nature of this scheme using the $\bar{U}$ formulation is as discussed previously. Alternatively one can use (4.14d) instead of (4.15) but add a high-resolution filter as the final step to obtain the solution for the next time level.

V. CONCLUDING REMARKS

Two families of explicit and implicit compact high-resolution shock-capturing methods for the multidimensional compressible Euler equations have been formulated. Some of these schemes can be spatially fourth- and sixth-order accurate away from discontinuities. The attractive property of these compact high-resolution shock-capturing schemes is that fourth- or sixth-order accuracy can be achieved using the same grid stencil width (5–7 points in each spatial direction) and numerical fluxes as their second-order noncompact cousins. In contrast, typical grid stencils for noncompact fourth-order high-resolution shock-capturing schemes require 9–11 points in each spatial direction.

Many variations of these two families of schemes are proposed. The majority of the modified Abarbanel and Kumar schemes are best suited for time-marching to the steady state. Although they can be used for time-accurate computations, the time accuracy can be at most second order in order. Two modifications to the TVDM idea proposed by Cockburn and Shu to improve shock resolution

are discussed. They can be used for both time-marching and time-accurate computations. These modifications to the scheme of Cockburn and Shu result in far better shock resolution than their original form. In 2D, the operation count for both families is comparable, whereas the 3D TVDM version is more expensive to compute at each step than the Abarbanel and Kumar extension. However, a spatially and temporally fourth-order compact variant of the Cockburn and Shu scheme is readily obtained for both time-accurate and time-marching approaches as opposed to the inability to extend the Abarbanel and Kumar modification in a similar manner for time-accurate computations.

The one-leg formulation of these two families of implicit compact schemes is also proposed. If iterative relaxation methods are used, the one-leg forms (for both families) are less expensive to compute than their non-one-leg cousins. High-resolution shock-capturing properties of these families of compact forms can also be achieved via a variant of the higher-order Lax Friedrichs numerical flux. Comparable operations count to their classical shock-capturing counterparts can be achieved without the use of Riemann solvers for coupled nonlinear systems. Thus this makes high-order high-resolution compact shock-capturing schemes a viable and efficient numerical method for 3D combustion and chemically and thermally nonequilibrium flow computations.

Preliminary numerical experiments (performed by Dr. George Huang of NASA Ames) with both families of compact schemes for the 1D scalar Burgers equation and a 2D shock reflection problem indicate the desired shock-capturing property. The time differencing used for the numerical experiments for both problems is the implicit Euler method. The Abarbanel and Kumar extension gives a better shock resolution than the TVDM version. However, the current TVDM version exhibits better shock resolution than the numerical flux used by Cockburn and Shu in their original paper. In order to assess the accuracy and shock resolution of these schemes, extensive numerical tests for a variety of representative model problems and higher than 1D Euler equations have to be performed. For high gradient, and/or wave propagation and high frequency types of flow fields, selection of a limiter with less clipping at extrema points is the key. One possibility is the limiter suggested by Davis [6]. Another is the artificial compression method of Harten [10]. The use of limiters for this type of flow containing no shock wave can act as a nonlinear method of supplying numerical dissipation. Details of the study with limiters other than the ones discussed in Section III are the subject of current research.

Without extensive numerical experiments in hand, all we can comment on is the relative advantages and disadvantages of these two families of schemes based on operations count (vector additions and tridiagonal matrix inver-

sion due to the compact formula), the requirement of a special numerical boundary treatment, applicability to and accuracy for time-accurate calculations, and ease of implementation to include source terms. From the discussion in previous sections, one can conclude that for all but the fourth-order time-accurate capability issue, the Abarbanel and Kumar extension appears to be more efficient than the TVDM version.

The majority of these implicit schemes are especially suited for time-marching approaches to steady-state numerical solutions, since higher-order spatial accuracy can be achieved with minimal effort and the steady states are independent of the time step. The proper choice of time discretizations for the proposed two families of schemes for wave propagation, and computational aeroacoustics type of applications has not been addressed. Thus, the time discretizations discussed in this paper might not be optimized for the particular types of flows in the sense of wave resolution and phase error discussed in Tam and Webb, Lele, Ma, & Fu, Davis, and the 1995 Workshop on Aeroacoustics. This topic is ongoing research. Future study will include practical application of these families of methods to a variety of flow physics.

ACKNOWLEDGMENTS

The author thanks Saul Abarbanel for his valuable discussions during the course of this research and George Huang for performing the preliminary numerical study. Special thanks to Saul Abarbanel, Eli Turkel, George Huang, Terry Holst, and Peter Goorjian for their critical review of the manuscript.

REFERENCES

1. M. Carpenter, D. Gottlieb, and S. Abarbanel, *J. Comput. Phys.* **108**, 272 (1993).
2. S. Lele, *J. Comput. Phys.* **103**, 16 (1992).
3. Y.-W. Ma and D. Fu, *Proceedings 6th International Symposium on Computational Fluids, Lake Tahoe, CA, Sept. 4-8, 1995*.
4. S. S. Davis, A space-time discretization procedure for wave propagation problems, NASA TM-102215, Nov. 1989 (unpublished).
5. N. A. Adams and K. Shariff, A high-resolution hybrid compact-ENO scheme for shock-turbulence interaction problems, CTR Manuscript 155, NASA Ames Research Center and Stanford University, 1995 (unpublished).
6. S. F. Davis, Shock capturing with Padé methods, in *Proceedings, 2nd Mississippi State Conference on Differential Equations and Computational Simulations, April 7-8, 1995, Miss. State, Miss.*
7. N. D. Sandham and H. C. Yee, A Numerical Study of a Class of TVD Schemes for Compressible Mixing Layers, NASA TM-102194, May 1989.
8. S. Abarbanel and A. Kumar, *J. Scientific Computing* **3**, 275 (1988).
9. B. Cockburn and S.-W. Shu, *SIAM J. Numer. Anal.* **31**, 607 (1994).
10. A. Harten, *Math. Comput.* **32**, 363 (1978).
11. B. Einfeldt, "On Positive Shock-Capturing Schemes," College of Aeronautics, COA8810, August 1988, Cranfield Institute Technology, Bedford, England.

12. X.-D. Liu and P. D. Lax, "Positive Schemes for Solving Multi-dimensional Hyperbolic Systems of Conservation Laws," *CFD Rev.* to appear.
13. H. C. Yee, "A Class of High-Resolution Explicit and Implicit Shock-Capturing Methods," VKI Lecture Series 1989-04 March 6-10, 1989, also NASA TM-101088, Feb. 1989.
14. M. Ciment and H. Leventhal, *Math. Comp.* **29**, 985 (1975).
15. R. S. Hirsh, *J. Comput. Phys.* **19**, 109 (1975).
16. B. Gustafsson and O. Olsson, *J. Comput. Phys.* **117**, 300 (1995).
17. W. R. Briley and H. McDonald, *J. Comput. Phys.* **24**, 372 (1977).
18. R. M. Beam and R. F. Warming, *AIAA J.* **16**, 293 (1978).
19. C. K. W. Tam and J. C. Webb, *J. Comput. Phys.* **10**, 262 (1993).
20. Workshop on Benchmark Problems in Computational Aeroacoustic (1995), NASA Conference Publication 3300, edited by Hardin, J. C., Ristorcelli, J. R. and Tam, C. K. W.
21. H. C. Yee, "Explicit and Implicit Compact High-Resolution Shock-Capturing Methods for Multidimensional Euler Equations I: Formulation," NASA TM-110364, August 1995.
22. J. Anderson, *Hypersonic and High Temperature Gas Dynamics* (McGraw Hill, New York, 1989).
23. C. Park, *Nonequilibrium Hypersonic Aerothermodynamics* (Wiley, New York, 1990).
24. H. C. Yee and J. Shinn, *AIAA J.* **27**, 299 (1989).
25. R. J. LeVeque and H. C. Yee, *J. Comput. Phys.* **86**, 187 (1990).
26. H. C. Yee, P. K. Sweby, and D. F. Griffiths, *J. Comput. Phys.* **97**, 249 (1991).
27. A. Lafon and H. C. Yee, *Intern. J. of CFD* **6**, 1 (1996).
28. A. Lafon and H. C. Yee, *Intern. J. of CFD* **6**, 89 (1996).
29. D. F. Griffiths, A. M. Stuart, and H. C. Yee, *SIAM J. of Numer. Anal.* **29**, 1244 (1992).
30. H. C. Yee and P. K. Sweby, *Intern. J. Bifurcation & Chaos*, **4**, 1579 (1994).
31. H. C. Yee and P. K. Sweby, *Intern. J. of CFD* **4**, 219 (1995).
32. H. C. Yee and P. K. Sweby, "Nonlinear Dynamics & Numerical Uncertainties in CFD," NASA TM-110398, April 1996.
33. H. C. Yee, *Computers and Mathematics with Applications*, **12A**, 413 (1986).
34. S. L. Steger and R. F. Warming, *J. Comput. Phys.* **40**, 263 (1981).
35. B. van Leer, "Flux-vector splitting for the Euler Equations," ICASE Report 82-30; Sept., 1982.
36. C. W. Gear, *Numerical Initial Value Problems in Ordinary Differential Equations*, Prentice-Hall, Englewood Cliffs (1971).
37. J. D. Lambert, *Computational Methods in Ordinary Differential Equations* (Wiley, New York, 1973).
38. Y. Saad, "Preconditioning Krylov Subspace Methods for CFD Applications," Proceedings of the International Workshop on Solution Techniques for Large-Scale CFD Problems, Habashi, W.G. Editor, Montreal, Canada, Sept. 26-28, 1994.
39. E. Turkel, *Applied Numerical Mathematics*, **12**, 257 (1993).
40. G. Dahlquist, "some Properties of Linear Multistep and One-Leg Methods for Ordinary Differential Equations," Conference Proceedings, 1979 SIGNUM Meeting on Numerical ODE's, Champaign, Ill (1979).
41. R. M. Beam and R. F. Warming, "An Implicit Factored Scheme for the Compressible Navier-Stokes Equations II: The Numerical ODE Connection," AIAA-79-1446 (1979).
42. M. Carpenter and C. A. Kennedy, "Fourth-Order 2N Storage Runge-Kutta Schemes," NASA TM-109112, June 1994.
43. S.-W. Shu, *J. Comput. Phys.* **83**, 32 (1989).
44. A. Harten, *J. Comp. Phys.* **49**, 375 (1983).
45. A. Harten, *SIAM J. Num. Anal.* **21**, 1 (1984).
46. H. C. Yee and A. Harten, *AIAA J.* **25**, 266 (1987).
47. H. C. Yee, "On Symmetric and Upwind TVD Schemes," *Proceedings of the 6th GAMM-Conference on Numerical Methods in Fluid Mechanics*, Sept. 1985, Gottingen, Germany.
48. H. C. Yee, G. H. Klopfer, and J.-L. Montagne, *J. Comput. Phys.* **88**, 31 (1990).
49. R. Donat, *SIAM J. Numer. Anal.* **31**, 655 (1994).
50. B. Engquist and B. Sjogreen, "High Order Shock Capturing Methods," *CFD Reviews*, Hafez & Oshima, Eds., John Wiley, New York, pp. 210-233 (1995).
51. B. Engquist and B. Sjogreen, "Numerical convergence rate in the presence of shocks," in preparation.
52. S. Jin and J.-G. Liu, "The effects of numerical viscosities, I: the slowly moving shocks," *J. Comp. Phys.* to appear (1996).
53. H. C. Yee and P. Kutler, "Application of Second-Order-Accurate Total Variation Diminishing (TVD) Schemes to the Euler Equations in General Geometries," NASA TM 85845, 1983.
54. H. C. Yee, R. F. Warming, and A. Harten, *J. Comput. Phys.* **57**, 327 (1985).
55. S.-W. Shu, *Math. Comp.* **49**, 105 (1987).
56. S.-W. Shu, *SIAM J. Sci. Stat. Comput.* **9**, 1073 (1988).
57. S. Osher and S. Chakravarthy, "Very High Order Accurate TVD Schemes," *The IMA Volumes in Mathematics and its Applications*, Vol. 2, Springer-Verlag, pp. 229-274 (1986).
58. A. Harten and S. Osher, *SIAM J. Num. Anal.* **24**, 279 (1987).
59. H. C. Yee, "On the Implementation of a Class of Upwind Schemes for System of Hyperbolic Conservation Laws," NASA TM-86839, Sept. 1985.
60. S. Abarbanel, private communication, 1994 (unpublished).
61. P. L. Roe, "Multidimensional Upwinding," VKI Lecture Series 1994-05 (1994).